

Viscous corrections from nonlinear transport

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Outline

- I. The problem of dissipative (δf) corrections
- II. A couple δf models
- III. Test them against full kinetic theory
- IV. Conclusions and future steps

Hydrodynamics

conservation laws:

$$\partial_\mu T^{\mu\nu}(x) = 0 \quad , \quad \partial_\mu N_B^\mu(x) = 0$$

additional EoM for dissipative fluids:

$$T^{\mu\nu}(x) = T_{ideal}^{\mu\nu}(x) + \delta T^{\mu\nu}(x)$$

$$N^\mu(x) = N_{ideal}^\mu(x) + \delta N^\mu(x)$$

$$\delta \dot{T}^{\mu\nu} = A^{\mu\nu}(\{T^{\alpha\beta}, N^\gamma\}) \quad , \quad \delta \dot{N}^\mu = B^\mu(\{T^{\alpha\beta}, N^\gamma\})$$

(e.g. Israel-Stewart '79)

utilizes equation of state ($p(e, n_B)$, $T(e, n_B)$), transport coeffs (η , ζ , κ_B), relaxation times (τ_η , τ_ζ , τ_κ)

some issues: - initial conditions needed \leftrightarrow thermalization

- how to “turn” hydro off at late times
- very small systems - quantum effects? DM, Wang, Greene,
- is it really hydro? He et al, arXiv:1502.05572

arXiv:1404.4119

Hydro \rightarrow particles

hydro gives N^μ & $T^{\mu\nu}$, but experiments measure particles

$$N^\mu(x) \equiv \sum_i \int \frac{d^3 p}{E} p^\mu f_i(p, x)$$

$$T^{\mu\nu}(x) \equiv \sum_i \int \frac{d^3 p}{E} p^\mu p^\nu f_i(p, x)$$

- in local equilibrium (ideal hydro) - “one to one”

$$T_{LR}^{\mu\nu}(x) = \text{diag}(e, p, p, p) \quad \Leftrightarrow \quad f_{eq,i}(x, p) = \frac{g_i}{(2\pi)^3} \frac{1}{e^{(p^\mu u_\mu - \mu_i)/T} + a}$$

- near local equilibrium (viscous hydro) - “few to many”

$$\begin{aligned} T^{\mu\nu}(x) &= T_{ideal}^{\mu\nu}(x) + \delta T^{\mu\nu}(x) \\ N^\mu(x) &= N_{ideal(x)}^\mu + \delta N^\mu(x) \end{aligned} \quad \Leftarrow \quad f_i(x, p) = f_{eq,i}(x, p) + \delta f_i(x, p)$$

\Rightarrow question of δf (even for single-species systems!)

δf models, for shear

$$\delta T^{\mu\nu} = \pi^{\mu\nu} \quad (\pi^{\mu\nu} u_\nu = 0, u_\nu \pi^{\mu\nu} = 0, \pi^\mu_{\mu} = 0)$$

purely spatial (in LR), symmetric, traceless

Navier-Stokes: $\pi^{\mu\nu} = \eta \underbrace{[\nabla^\mu u^\nu + \nabla^\nu u^\mu - \frac{2}{3} \Delta^{\mu\nu} (\partial \cdot u)]}_{2\sigma^{\mu\nu}}$

matter for:

- hadron distributions (fluid \rightarrow hadron gas conversion)
- E&M rates from QGP
- bound states in plasma ...

Grad ansatz

From “14-moment” expansion in kinetic theory

$$\delta f^{Grad}(x, \vec{p}) = \frac{1}{2T(x)^2[e(x) + p(x)]} p^\mu p^\nu \pi_{\mu\nu}(x) f_{eq}(x, \vec{p})$$

Popular for hydro because for multicomponent system the same form

$$\delta f_i = \frac{1}{2T^2(e + p)} p^\mu p^\nu \pi_{\mu\nu} f_{eq,i}$$

only needs knowledge of the full $T^{\mu\nu}$ and automatically yields $\sum_i T_i^{\mu\nu} = T^{\mu\nu}$.
Also used by Israel & Stewart (IS) to derive causal viscous hydrodynamics.

Can generalize to any power - “IS with p^α ”:

$$\delta f = \frac{C(\alpha)}{2T^2(e + p)} \left(\frac{p \cdot u}{T} \right)^{\alpha-2} p^\mu p^\nu \pi_{\mu\nu} f_{eq}$$

Weakness: negative f at sufficiently high momenta ($\pi^{\mu\nu}$ not pos definite)

Covariant transport

(on-shell) phase-space density $f(x, \vec{p}) \equiv \frac{dN(\vec{x}, \vec{p}, t)}{d^3x d^3p}$

transport equation:

$$p^\mu \partial_\mu f_i(x, p) = C_{2 \rightarrow 2}^i[\{f_j\}](x, p) + C_{2 \leftrightarrow 3}^i[\{f_j\}](x, p) + \dots$$

with, e.g.,

$$C_{2 \rightarrow 2}^i = \frac{1}{2} \sum_{jkl} \int_{234} (f_3^k f_4^l - f_1^i f_2^j) W_{12 \rightarrow 34}^{ij \rightarrow kl} \left(\int_j \equiv \int \frac{d^3 p_j}{2E_j}, \quad f_a^k \equiv f^k(x, p_a) \right)$$

thermalizes (in box), fully causal and stable

near hydro limit transport coeffs & relaxation times:

$$\eta \approx 1.2T/\sigma, \quad \tau_\pi \approx 1.2\lambda_{tr}$$

Linear response (for transport)

late-time, near-equilibrium behavior **universal**, and can be studied systematically de Groot, et al ('70s)... Arnold, Moore, Yaffe, JHEP 0011... Denicol et al PRD85 ('12)...

operationally: linearize in $\delta f = f - f_{eq}$, and put $\partial_t \rightarrow 0$

$$p \cdot \nabla f_{eq} = C[f_{eq}, \delta f]$$

integral eqn. relates δf to gradients in the system (one way to derive transport coeffs)

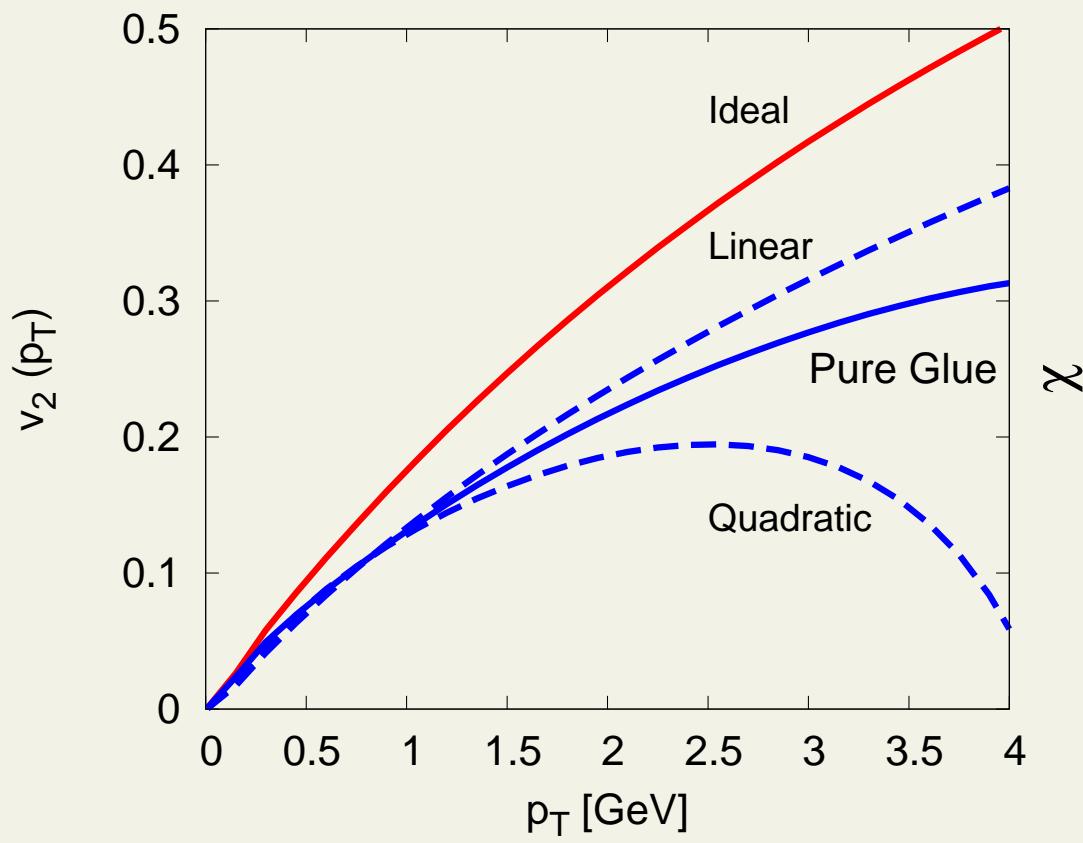
For shear, solution is of the form

$$\delta f(x, \vec{p}) = \chi \left(\frac{p \cdot u}{T} \right) \hat{p}_\mu \hat{p}_\nu \frac{\sigma^{\mu\nu}}{T} f_{eq}$$

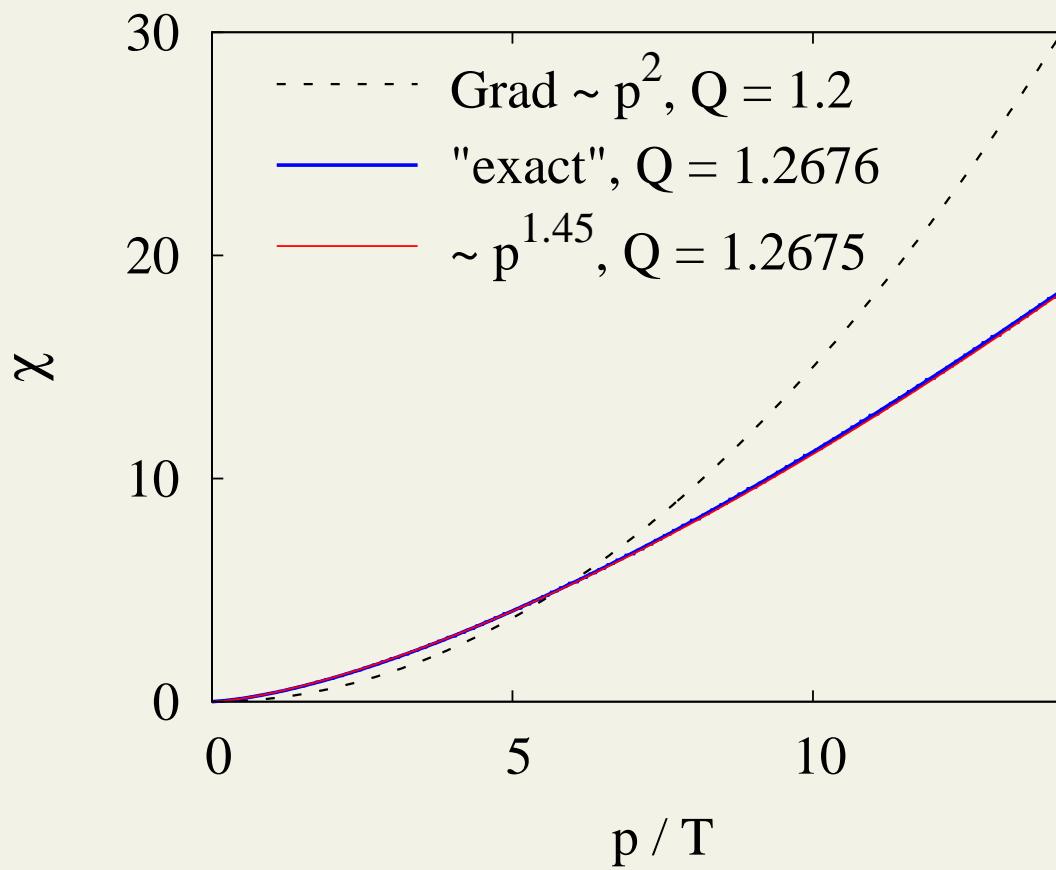
\Rightarrow nontrivial momentum dependence, but negativity problem remains

theory preference for $\chi \sim p^{1.5}$

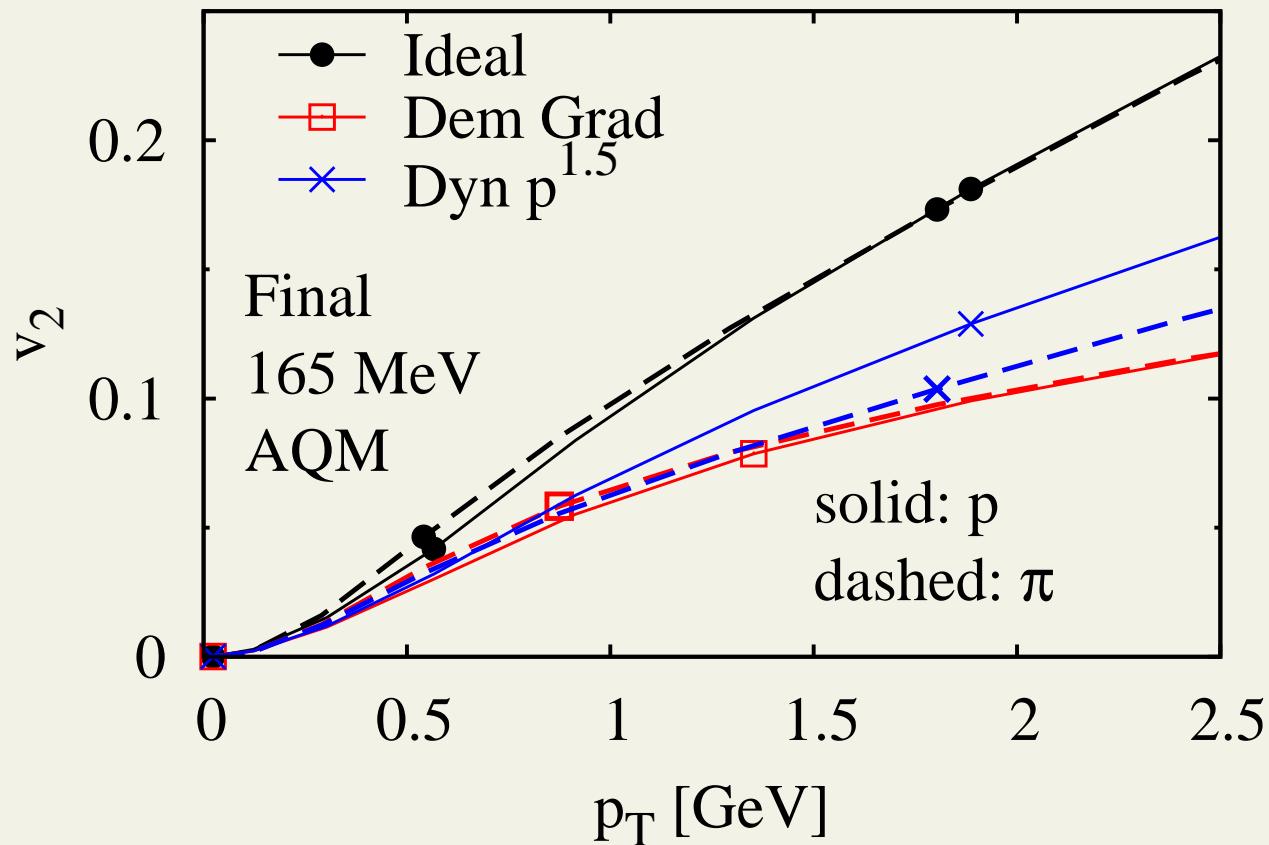
massless quark-gluon gas, forward-peaked cross sections Dusling, Moore, Teaney, PRC ('09)



massless gas, isotropic $\sigma = const$ DM, JPG38 ('12)



Au+Au @ RHIC, $b=7$ fm - conversion to hadron gas with ≈ 50 species
DM & Wolff, arXiv:1407.6413



pion-proton flow splitting due to different δf_i (additive quark model rates)

SR ansatz

Strickland & Romatschke, PRD 71 ('05):

$$f(p_T, p_z) = N e^{-\sqrt{E^2 + p_z^2}/\Lambda} = N \exp \left[-\frac{p_T}{\Lambda} \sqrt{\text{ch}^2 \xi + \textcolor{red}{a} \text{sh}^2 \xi} \right] \quad (\xi \equiv \eta - y)$$

- N, Λ, a **fixed by** N^0, T^{00}, T^{zz}
- **matches free streaming solution in 0+1D** [$a = (\tau/\tau_0)^2$]

more generally Tinti & Florkowski, PRC89 ('14)

$$f = N \exp \left[-\frac{1}{\Lambda} \sqrt{p^\mu \Xi_{\mu\nu} p^\nu} \right]$$

- **always positive, also: linear for small momenta**

Relaxation time approx (RTA)

Instead of Boltzmann, try

$$p \cdot \partial f(x, \vec{p}) = (p \cdot u) \frac{f_{eq}(x, \vec{p}) - f(x, \vec{p})}{\tau_{REL}}$$

Conserved particle number, energy & momentum, if $f_{eq}(f)$ chosen well.
 τ_{REL} must be matched to some dynamical aspect, e.g., the viscosity.

In late-time near-equilibrium regime ($\partial_t \rightarrow 0$): $p \cdot \nabla f_{eq} = -\tau_{REL}(p \cdot u)\delta f$

so with shear: $\delta f = \frac{\tau_{REL}}{2(p \cdot u)T} p_\mu p_\nu \sigma^{\mu\nu} f_{eq} = \frac{\tau_{REL}}{2} \frac{T}{(p \cdot u)} \frac{p_\mu p_\nu}{T^2} \frac{\pi^{\mu\nu}}{\eta} f_{eq}$

and from $\int \frac{d^3 p}{E} p^\mu p^\nu \delta f = \pi^{\mu\nu} \Rightarrow \tau_{REL} = \frac{5\eta}{4nT}$

Notice that $\delta f/f_{eq} \sim p^1$ (linear) in this case.

GOAL: test these models against full, nonlinear kinetic theory.

- i) obtain transport solutions with isotropic $2 \rightarrow 2$ interactions (MPC/Grid transport code)
- ii) from f , determine $T^{\mu\nu}$
- iii) study how well δf models reconstruct f from the $T^{\mu\nu}$ alone

MPC/Grid

similar to BAMPS - not a cascade

- $2 \rightarrow 2$ and $3 \leftrightarrow 2$ with test particles on a spatial grid

pair/triplet collisions with probability

$$P_{2 \rightarrow X} = \frac{\sigma_{2 \rightarrow X} v_{rel} \Delta t}{V_{cell}} , \quad P_{3 \rightarrow Y} = \frac{K_{3 \rightarrow Y} \Delta t}{V_{cell}^2}$$

5 numerical knobs: cell sizes ($d_x, d_y, d_z/d_\eta$), timestep Δt , subdivision ℓ

still action at distance → violates locality, causality, covariance

⇒ but more flexible than earlier MPC/Cascade

- we also have a version for parallel computers (MPI)

massless system, 0+1D Bjorken expansion (transversely uniform)

$$\Rightarrow f(p_T, \xi \equiv \eta - y, \tau)$$

$$u_{BJ}^\mu = (\text{ch}\eta, 0, 0, \text{sh}\eta), \quad (p \cdot u) = p_T \text{ch}\xi$$

$$T_{ideal, LR}^{\mu\nu} = p(\tau) \text{diag}(3, 1, 1, 1), \quad \pi_{LR}^{\mu\nu} = \pi_L(\tau) \text{diag}(0, -\frac{1}{2}, -\frac{1}{2}, 1)$$

dynamics governed by: $K(\tau) \equiv \frac{\tau_{exp}}{\tau_{sc}} = \frac{(\partial \cdot u)}{\lambda_{tr, MFP}} = \frac{2}{3} \tau n \sigma_{TOT} = \frac{2}{3} \tau_0 n_0 \sigma_{TOT}$

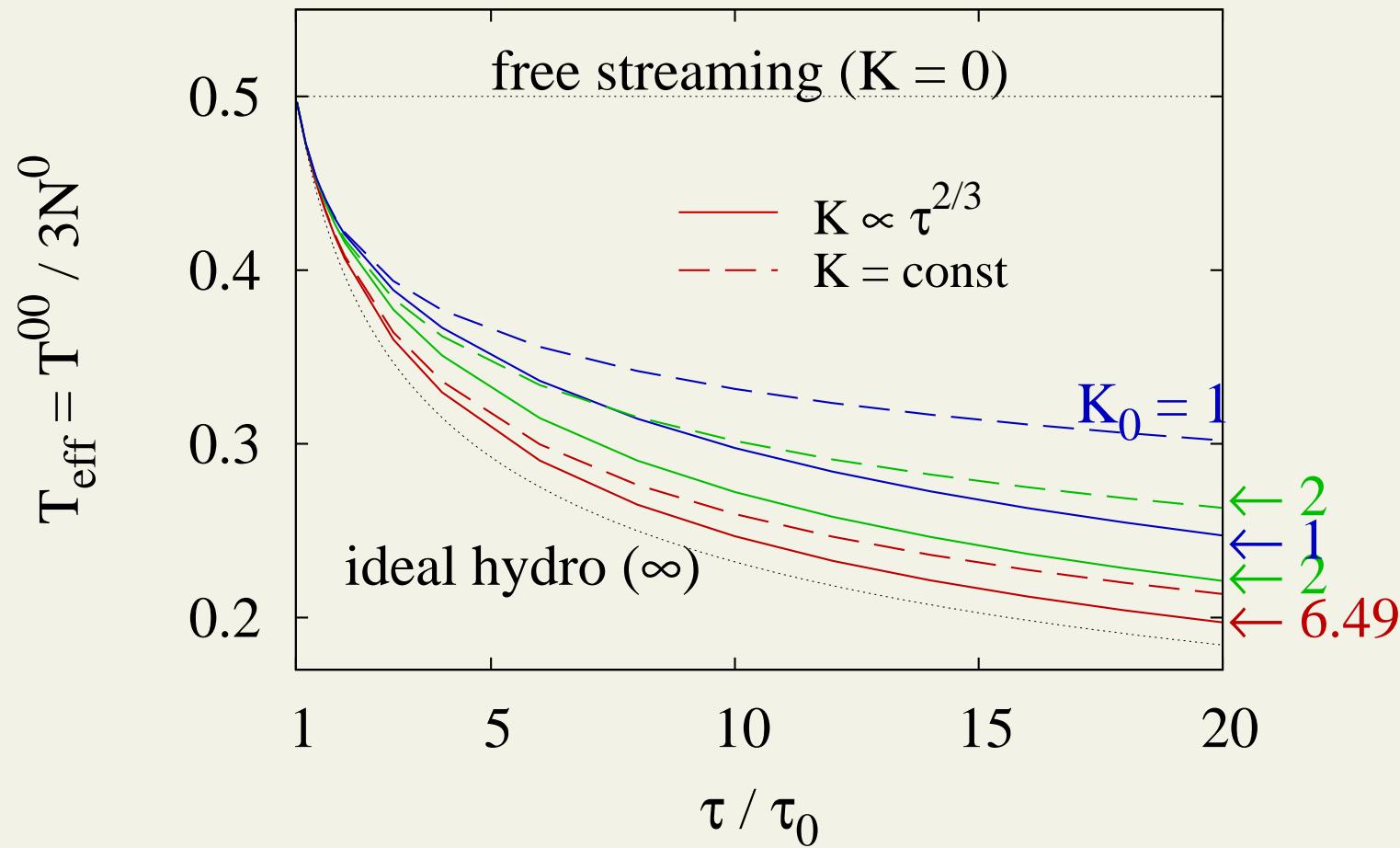
for $\eta/s \approx const$, $\sigma_{TOT} \sim \tau^{2/3} \Rightarrow K(\tau) \propto \tau^{2/3}$ DM & Huovinen, PRC79 ('09)

for $\sigma = const$, $K(\tau) = const$

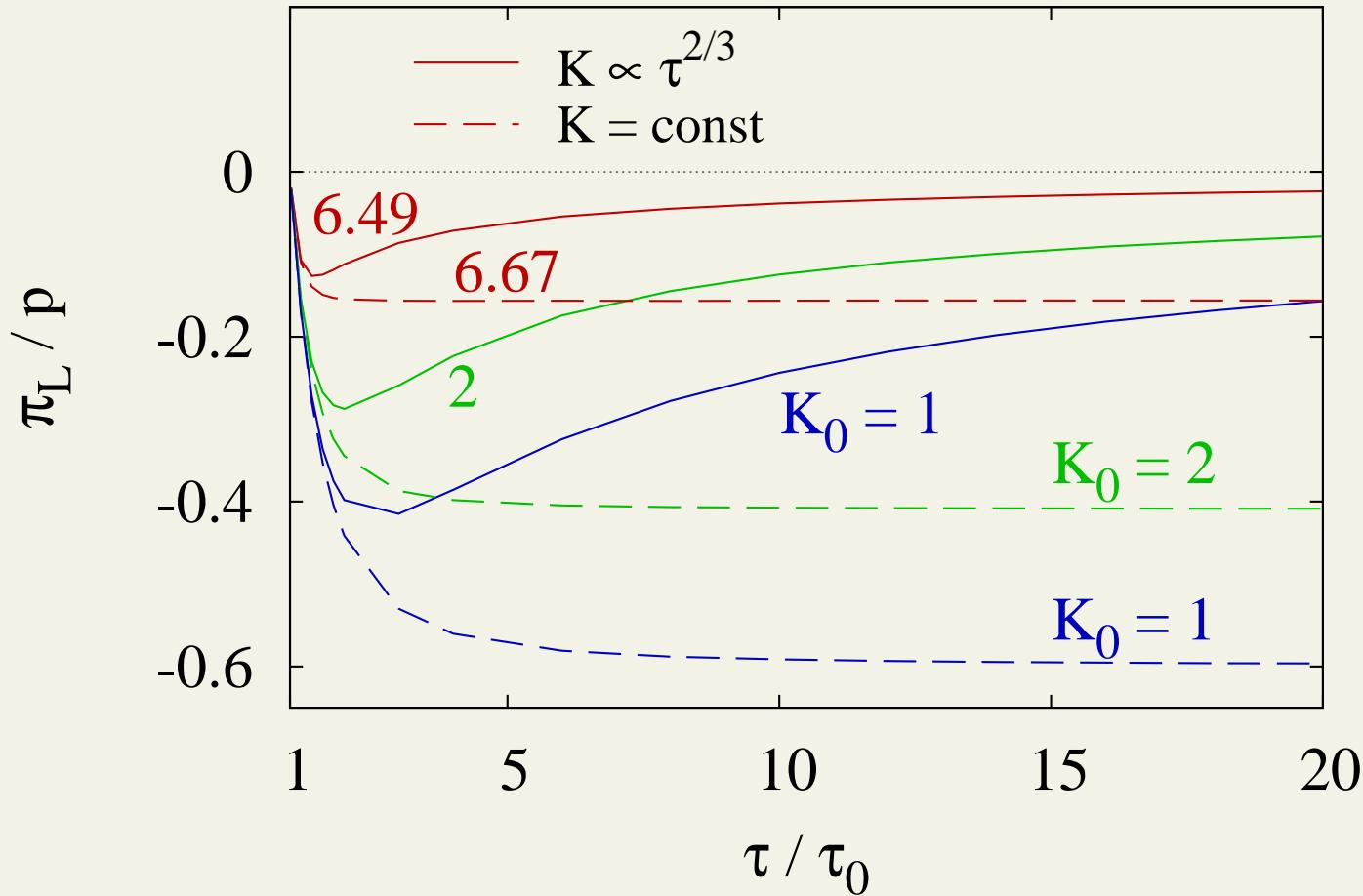
with $\eta = 1.26757.. \frac{T}{\sigma_{TOT}}$, we have $K_0 \approx 0.2 T_0 \tau_0 \frac{s}{\eta}(\tau_0)$ (used $s = 4n$)

and typically $\tau_0 T_0 \sim 1$, so $\eta/s = 1/(4\pi)$ corresponds to $K_0 \sim 2$

T_{eff} vs τ - cooling due to $p dV$ work Gyulassy, Pang, Zhang, NPA626 ('97)



viscous pressure correction vs τ - just like DM & Huovinen, PRC79 ('09)



First look at $f(p_T, \xi)$ with SR and Grad(IS) \rightarrow plot $\frac{f_{rec}}{f_{trans}}$

Generic features illustrated for $\eta/s \sim 1/(4\pi)$

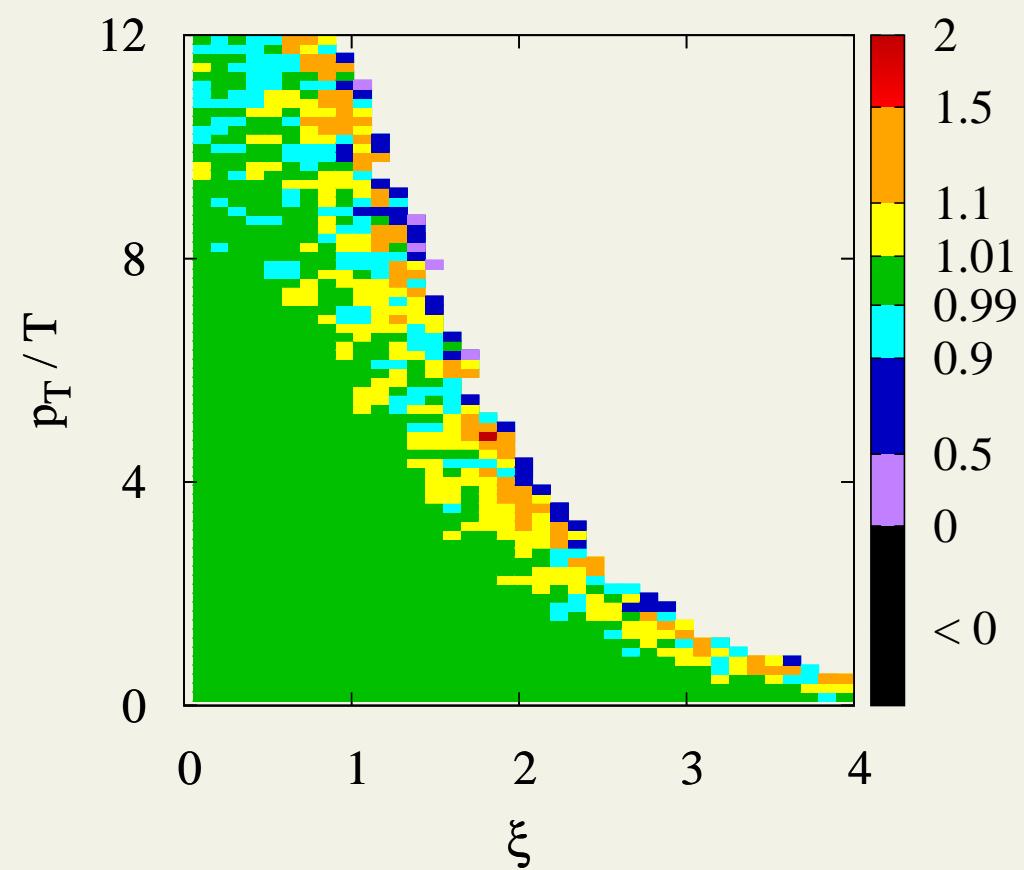
$$[K_0 = 2, K(\tau) \propto \tau^{2/3}]$$

Color coding:

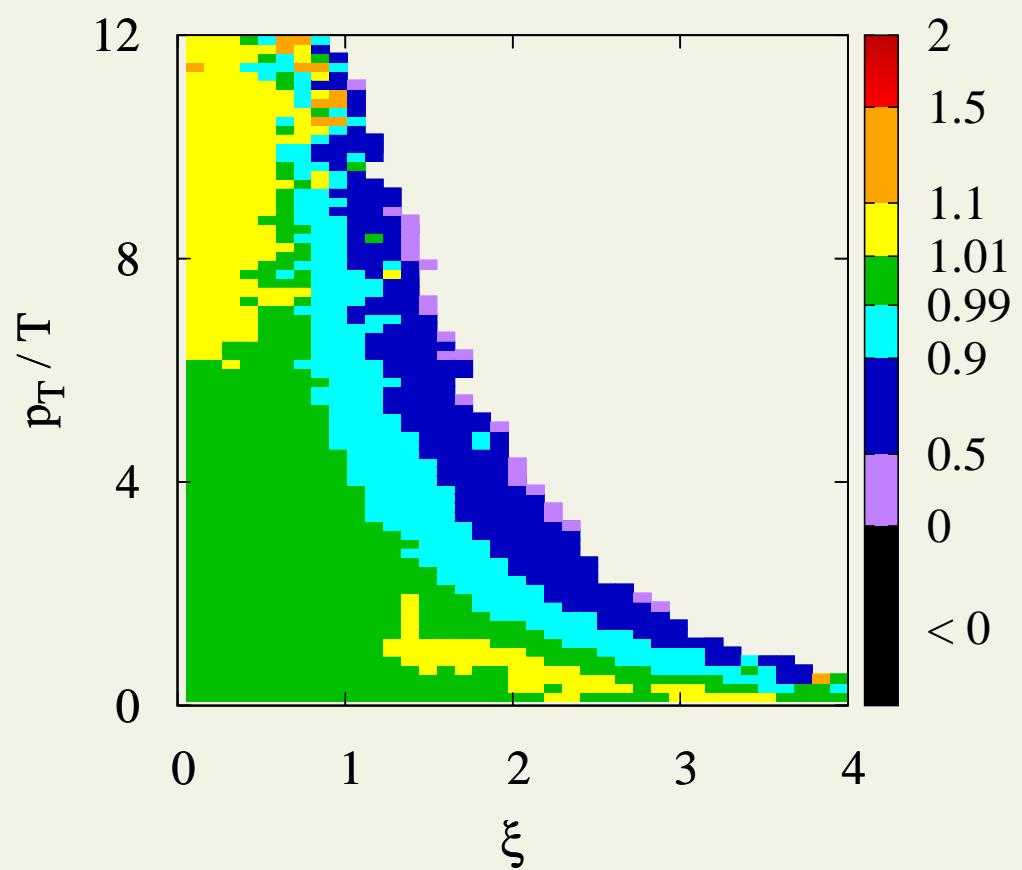
| |
|-----------|
| $+100\%$ |
| $+50\%$ |
| $+10\%$ |
| $\pm 1\%$ |
| -10% |
| -50% |
| -100% |
| < 0 |

$$\frac{\tau}{\tau_0} = 1.02, \quad K = 2 \left(\frac{\tau}{\tau_0} \right)^{2/3} \quad \left(\frac{\tau_{REL}}{\tau_{exp}} = 0.52, \quad \frac{\pi_L}{p} = -0.02 \right)$$

SR ansatz

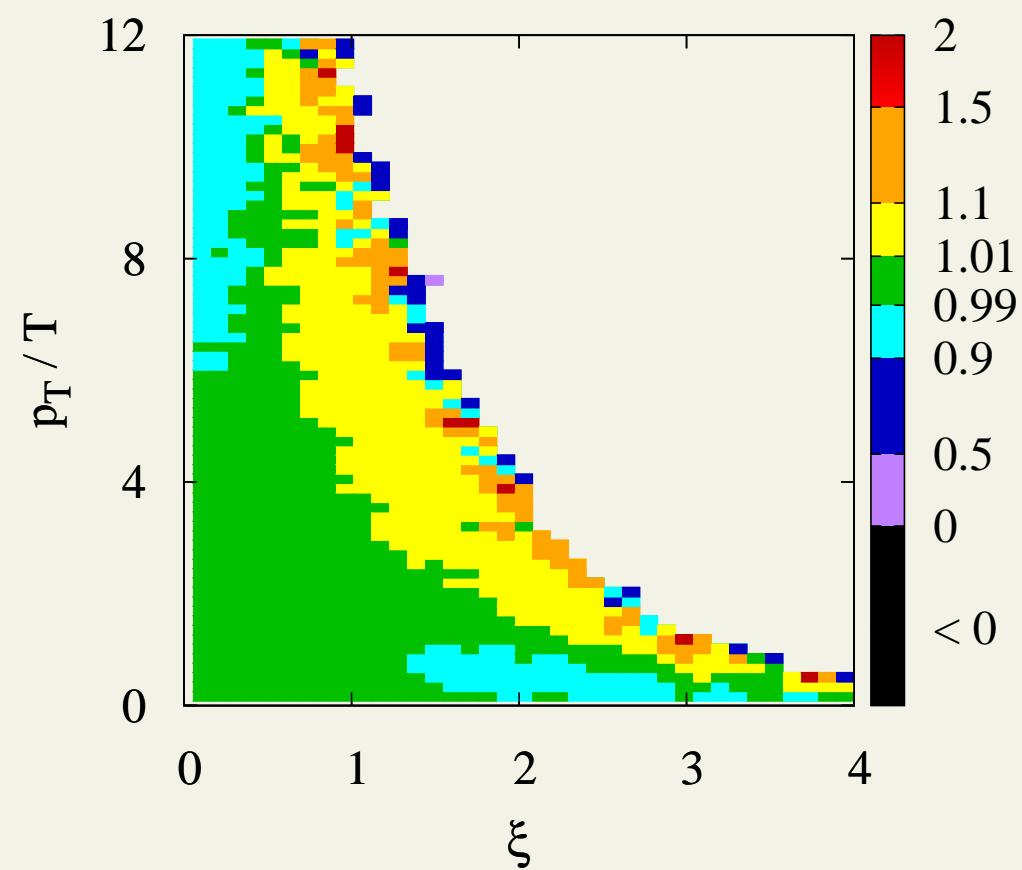


Grad (IS)

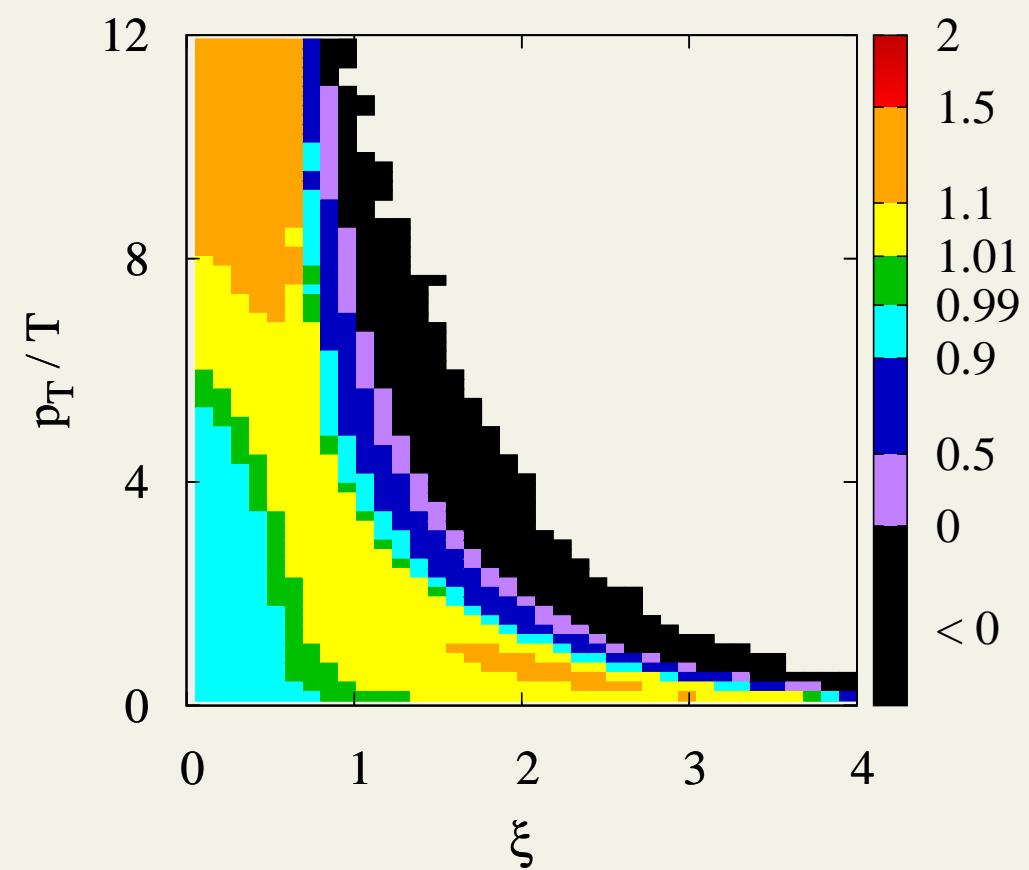


$$\frac{\tau}{\tau_0} = 1.2, \quad K = 2 \left(\frac{\tau}{\tau_0} \right)^{2/3} \quad \left(\frac{\tau_{REL}}{\tau_{exp}} = 0.47, \quad \frac{\pi_L}{p} = -0.15 \right)$$

SR ansatz

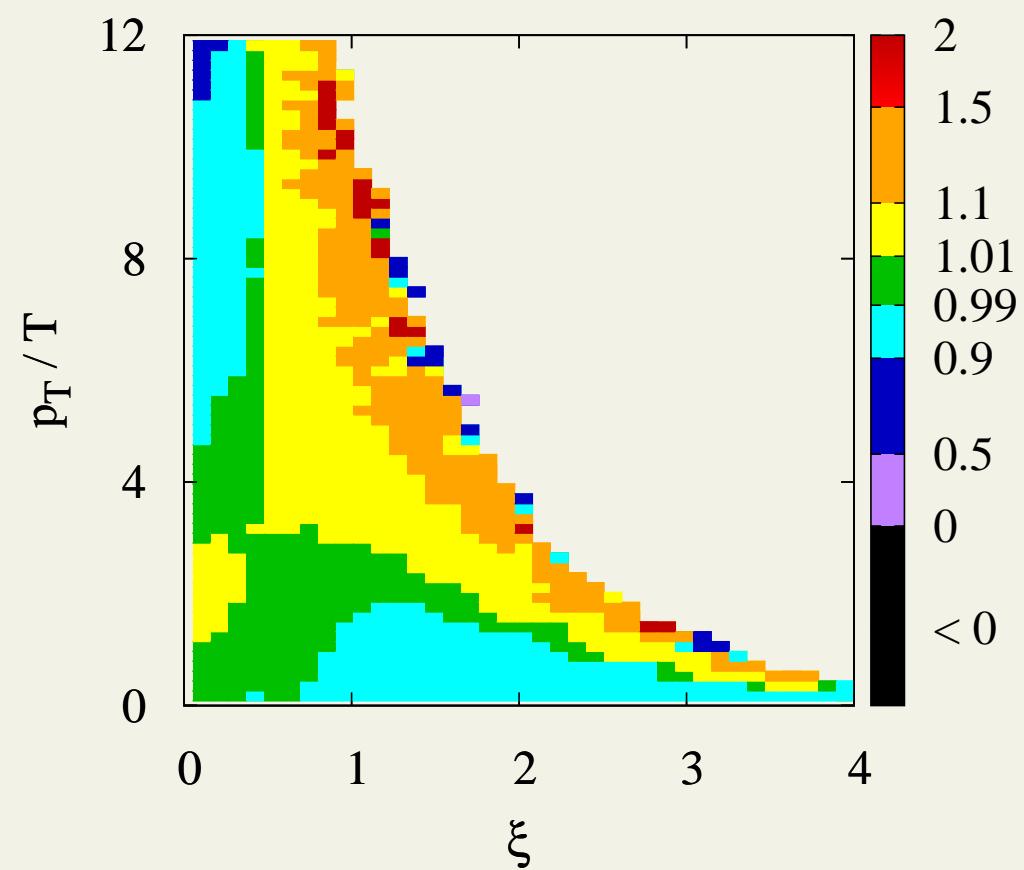


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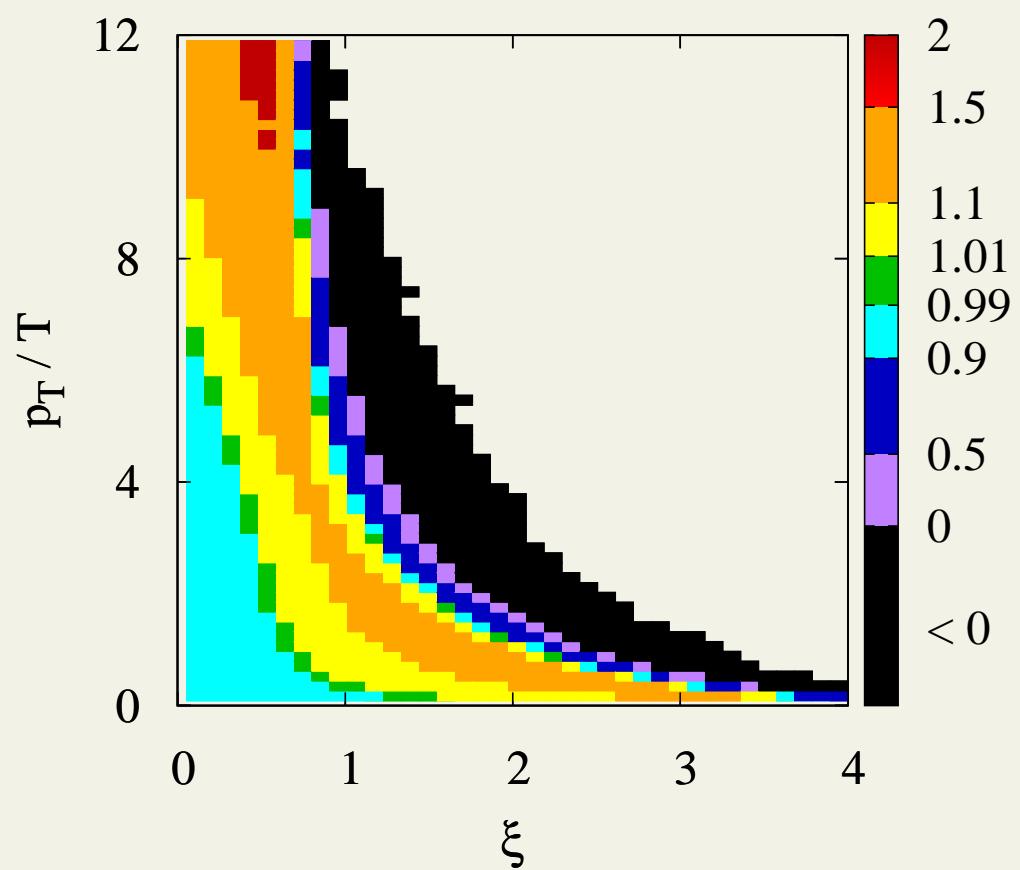


$$\frac{\tau}{\tau_0} = 1.4, \quad K = 2 \left(\frac{\tau}{\tau_0} \right)^{2/3} \quad \left(\frac{\tau_{REL}}{\tau_{exp}} = 0.42, \quad \frac{\pi_L}{p} = -0.23 \right)$$

SR ansatz



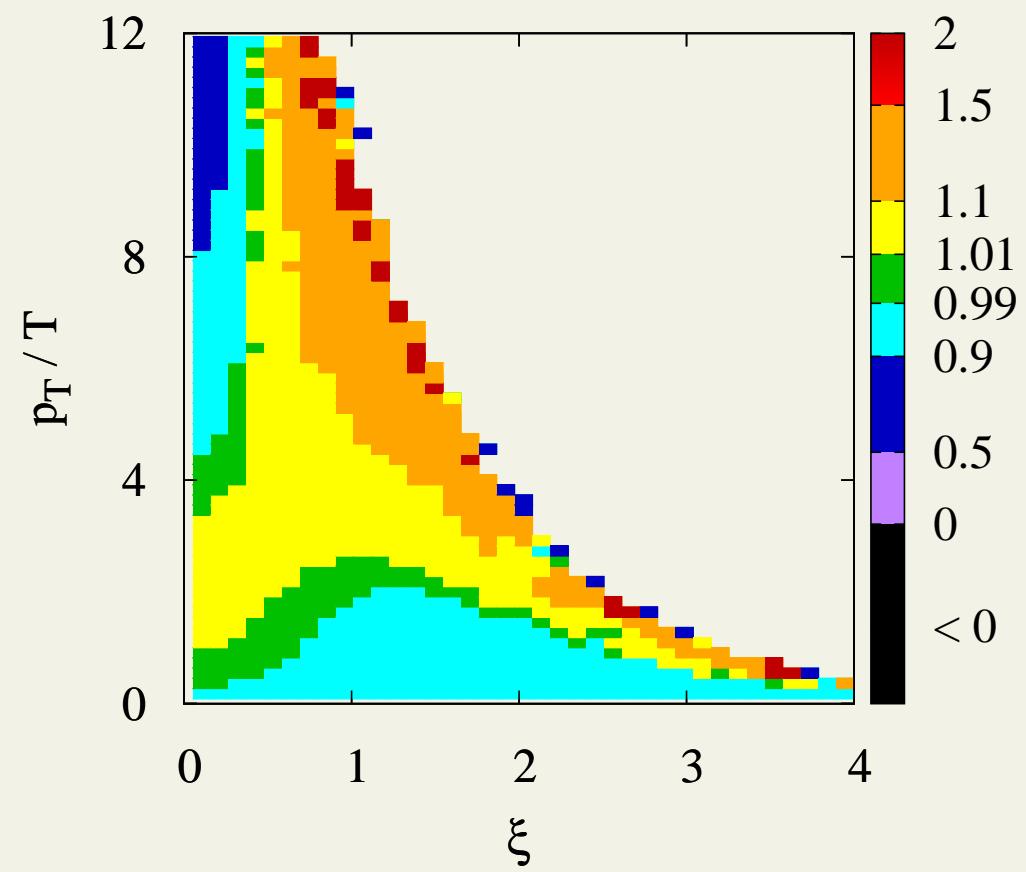
Grad (IS)



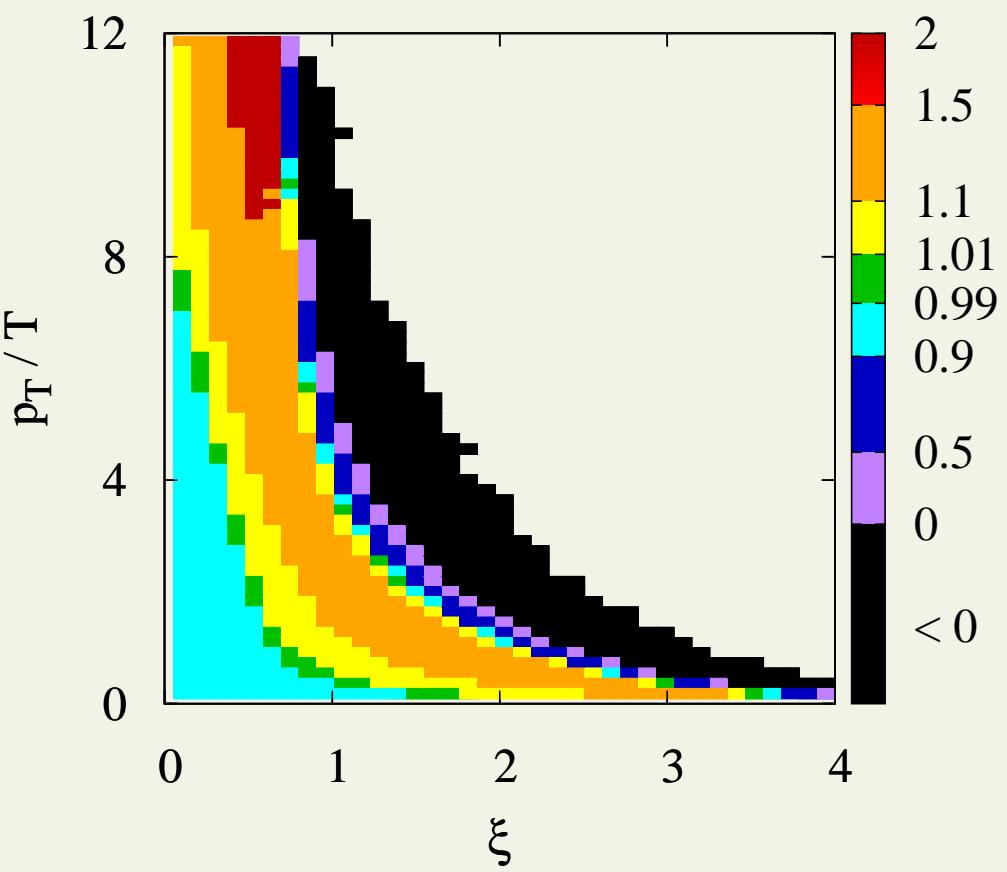
$$\frac{\tau}{\tau_0} = 1.6, \quad K = 2 \left(\frac{\tau}{\tau_0} \right)^{2/3}$$

$$\left(\frac{\tau_{REL}}{\tau_{exp}} = 0.38, \quad \frac{\pi_L}{p} = -0.27 \right)$$

SR ansatz



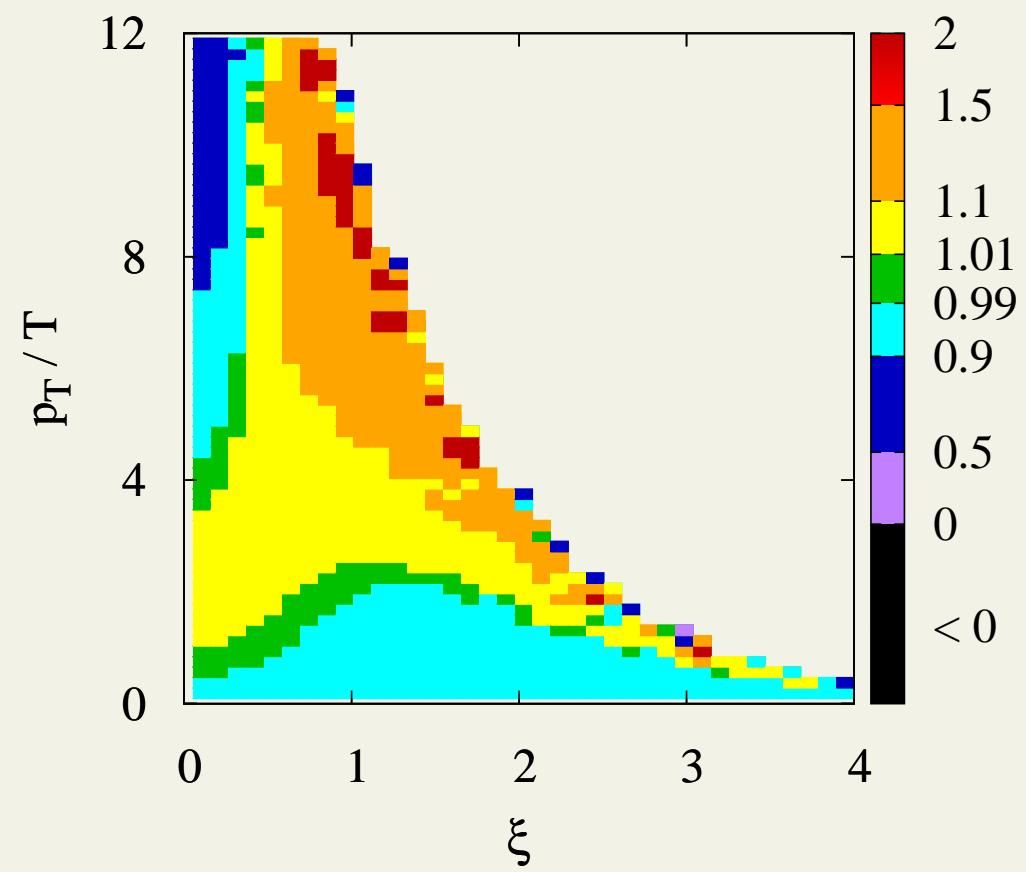
Grad (IS)



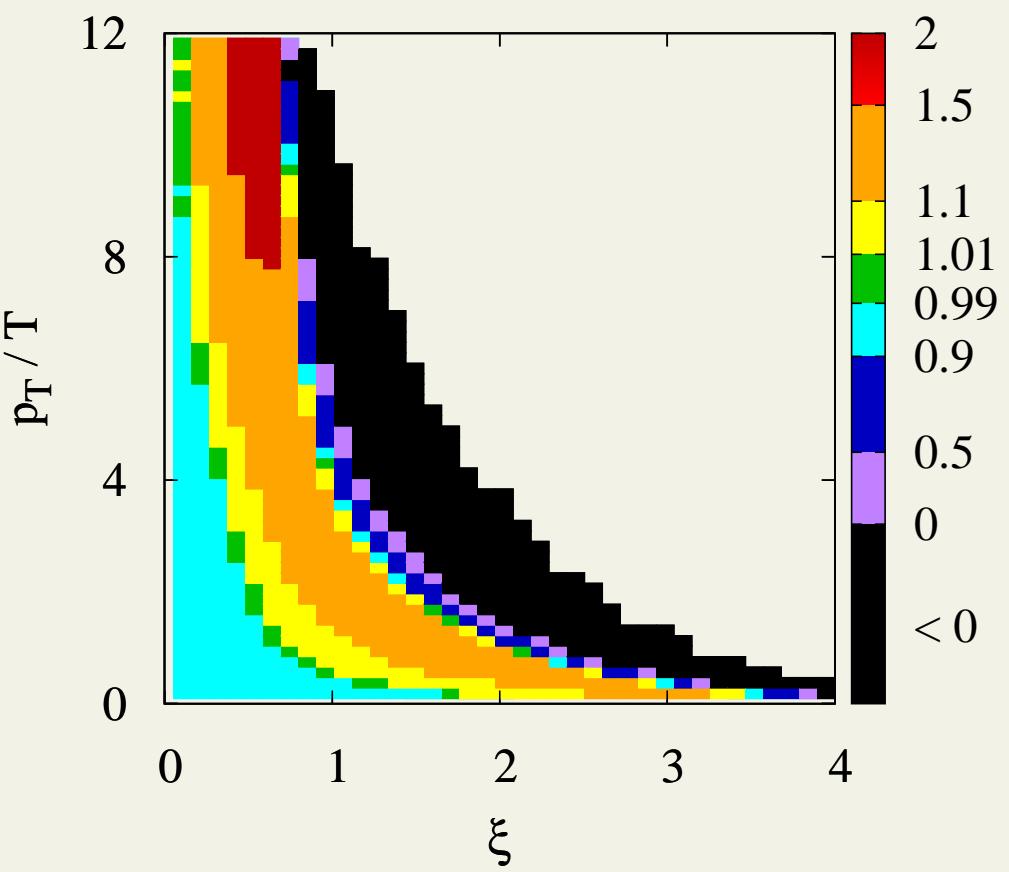
$$\frac{\tau}{\tau_0} = 1.8, \quad K = 2 \left(\frac{\tau}{\tau_0} \right)^{2/3}$$

$$\left(\frac{\tau_{REL}}{\tau_{exp}} = 0.36, \quad \frac{\pi_L}{p} = -0.28 \right)$$

SR ansatz

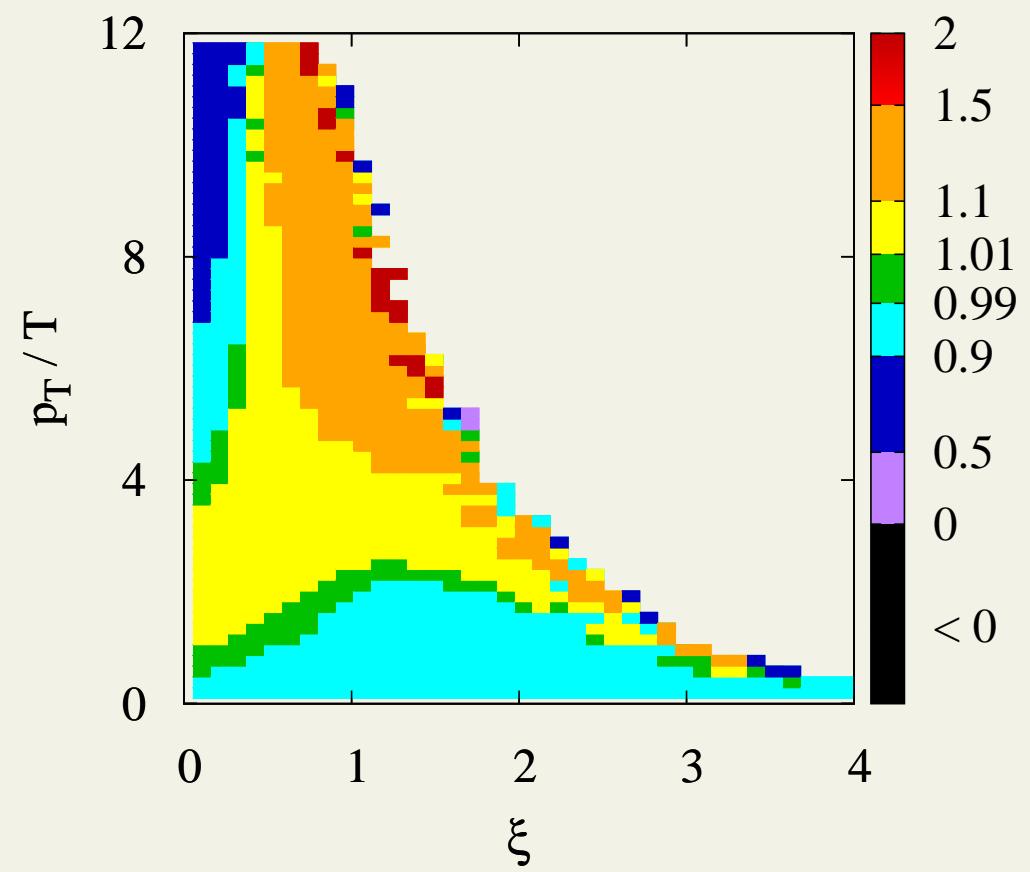


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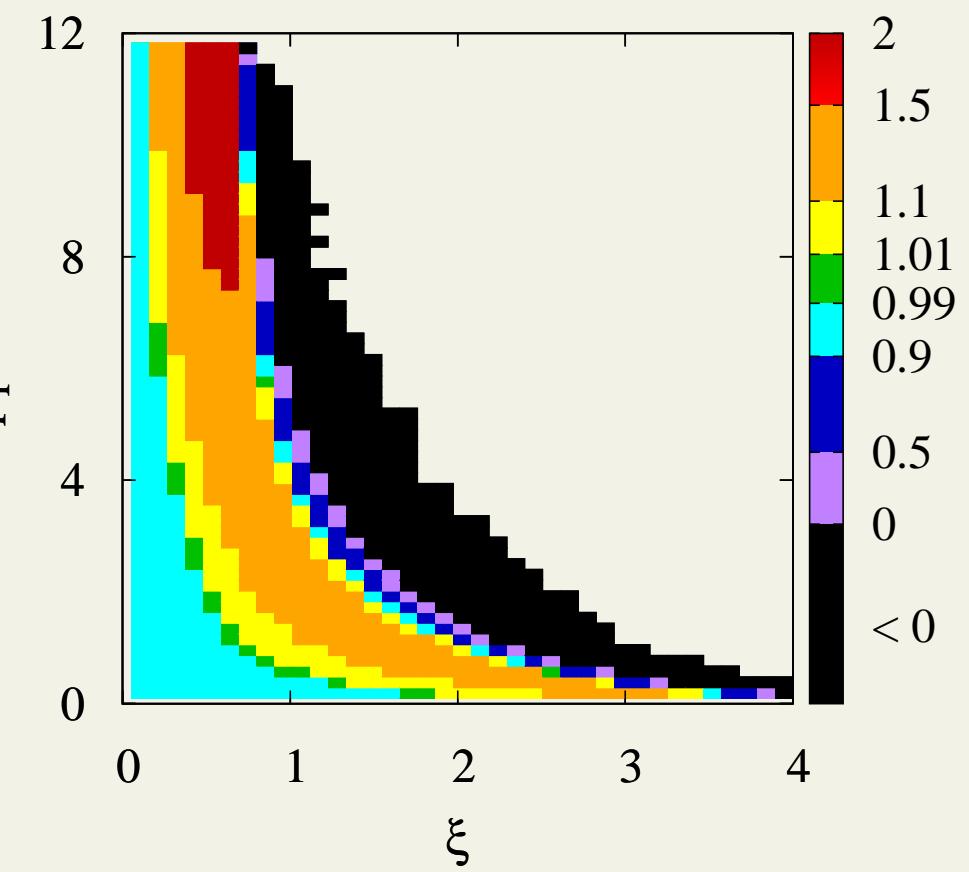


$$\frac{\tau}{\tau_0} = 2, \quad K = 2 \left(\frac{\tau}{\tau_0} \right)^{2/3} \quad \left(\frac{\tau_{REL}}{\tau_{exp}} = 0.33, \quad \frac{\pi_L}{p} = -0.29 \right)$$

SR ansatz

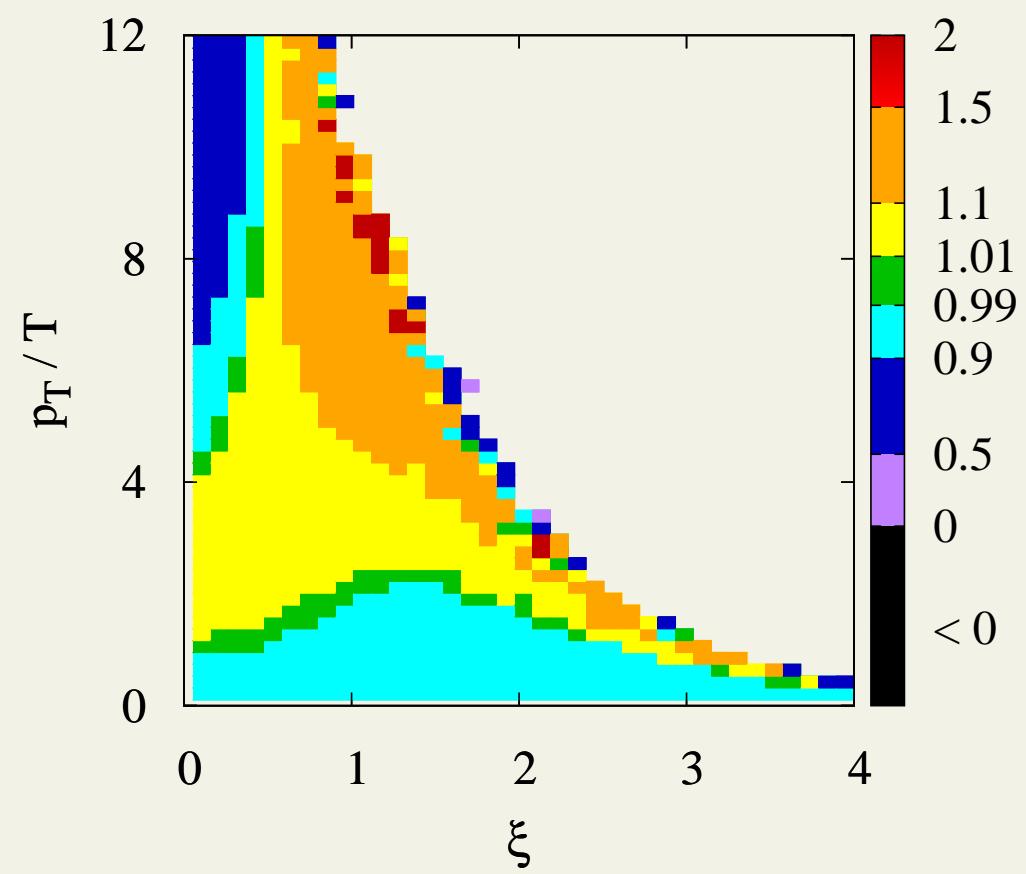


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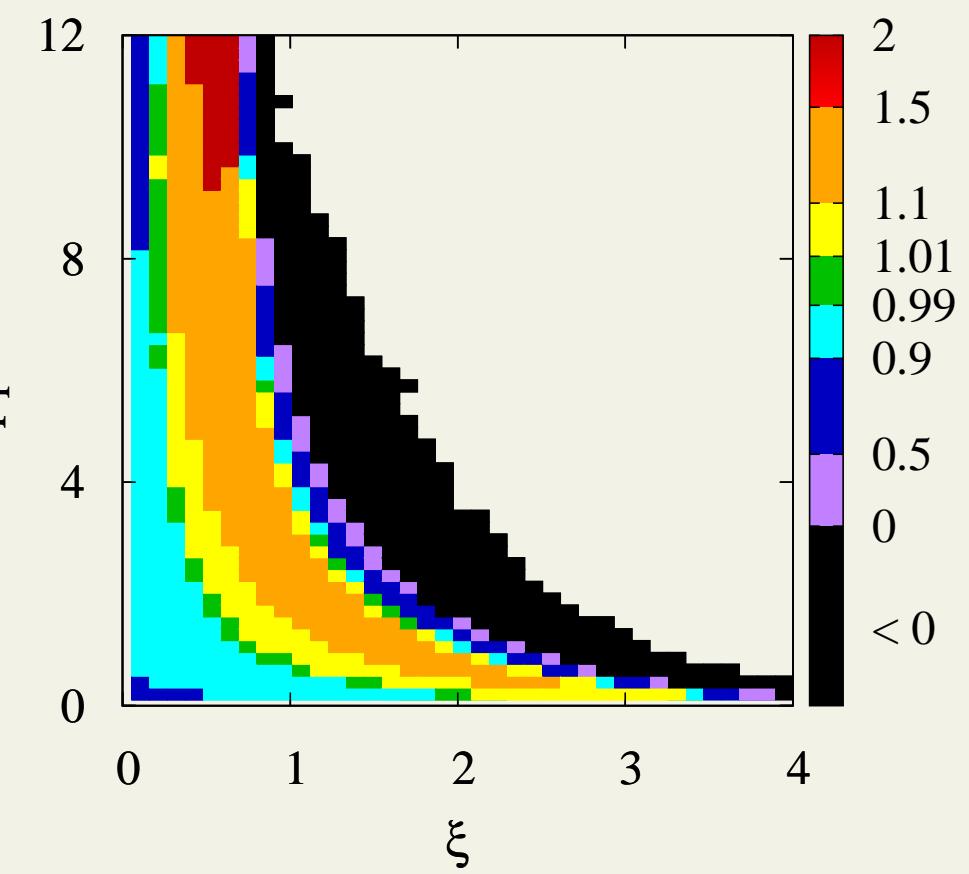


$$\frac{\tau}{\tau_0} = 3, \quad K = 2 \left(\frac{\tau}{\tau_0} \right)^{2/3} \quad \left(\frac{\tau_{REL}}{\tau_{exp}} = 0.25, \quad \frac{\pi_L}{p} = -0.26 \right)$$

SR ansatz

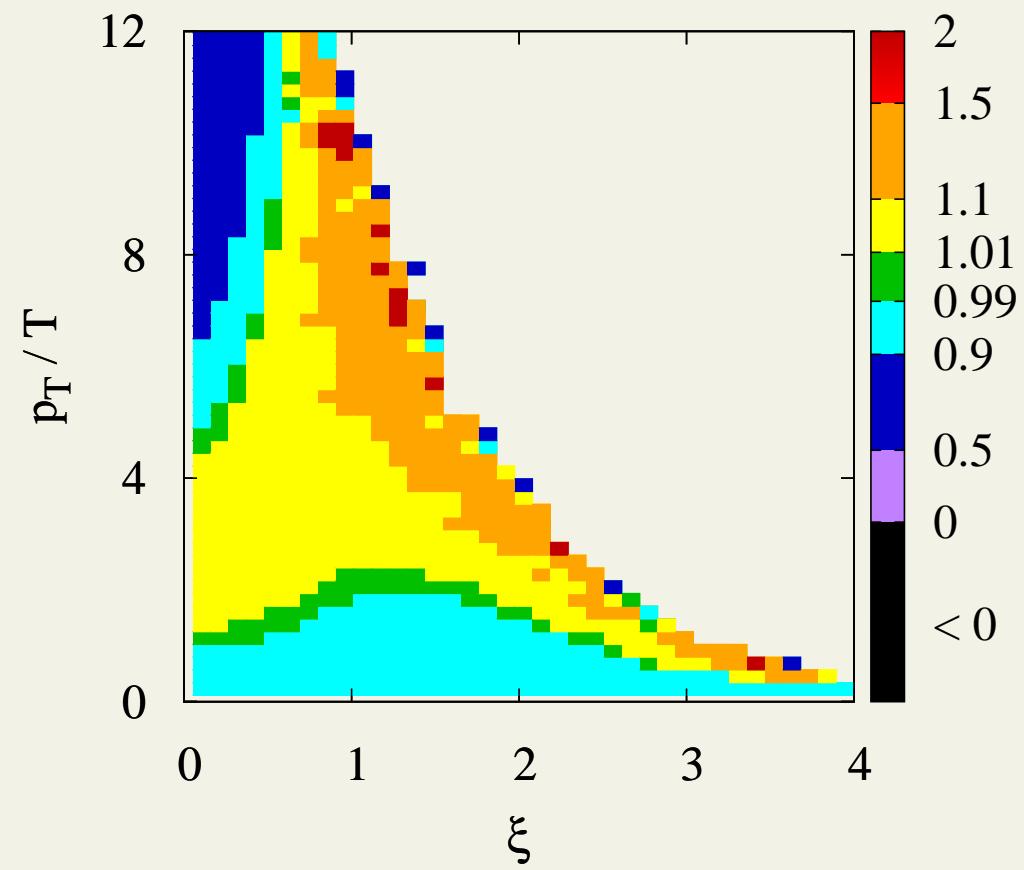


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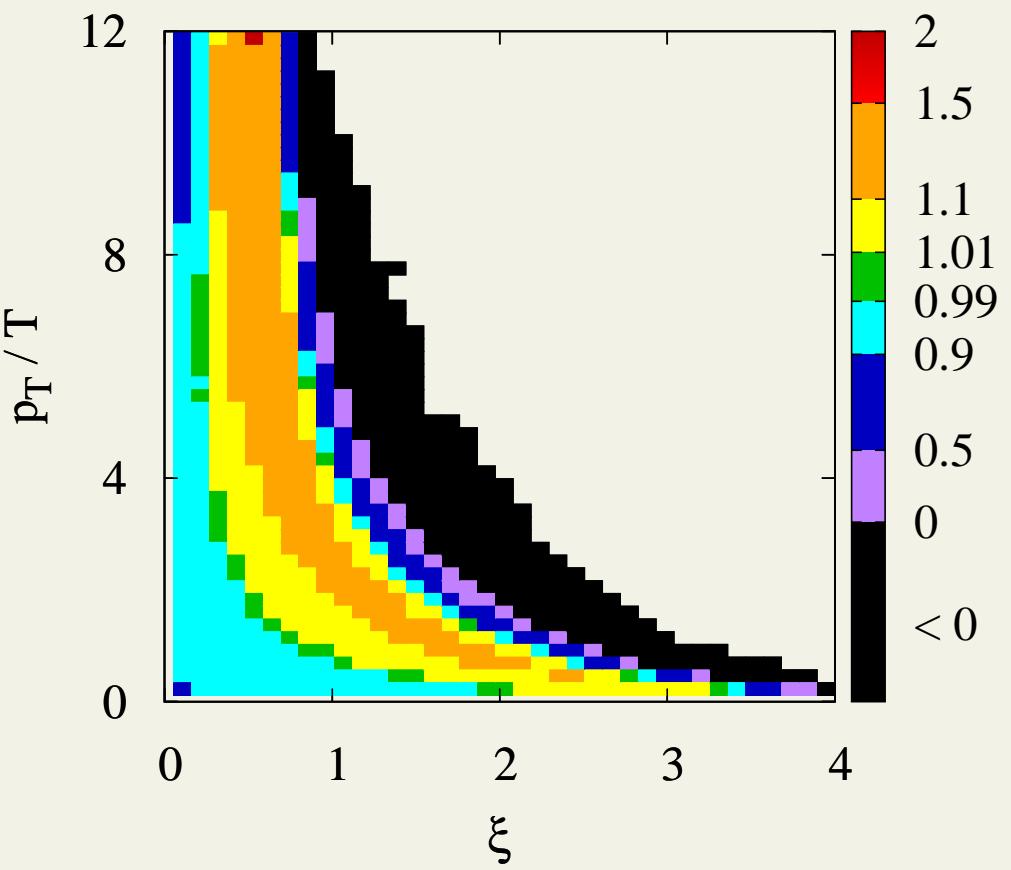


$$\frac{\tau}{\tau_0} = 4, \quad K = 2 \left(\frac{\tau}{\tau_0} \right)^{2/3} \quad \left(\frac{\tau_{REL}}{\tau_{exp}} = 0.21, \quad \frac{\pi_L}{p} = -0.22 \right)$$

SR ansatz

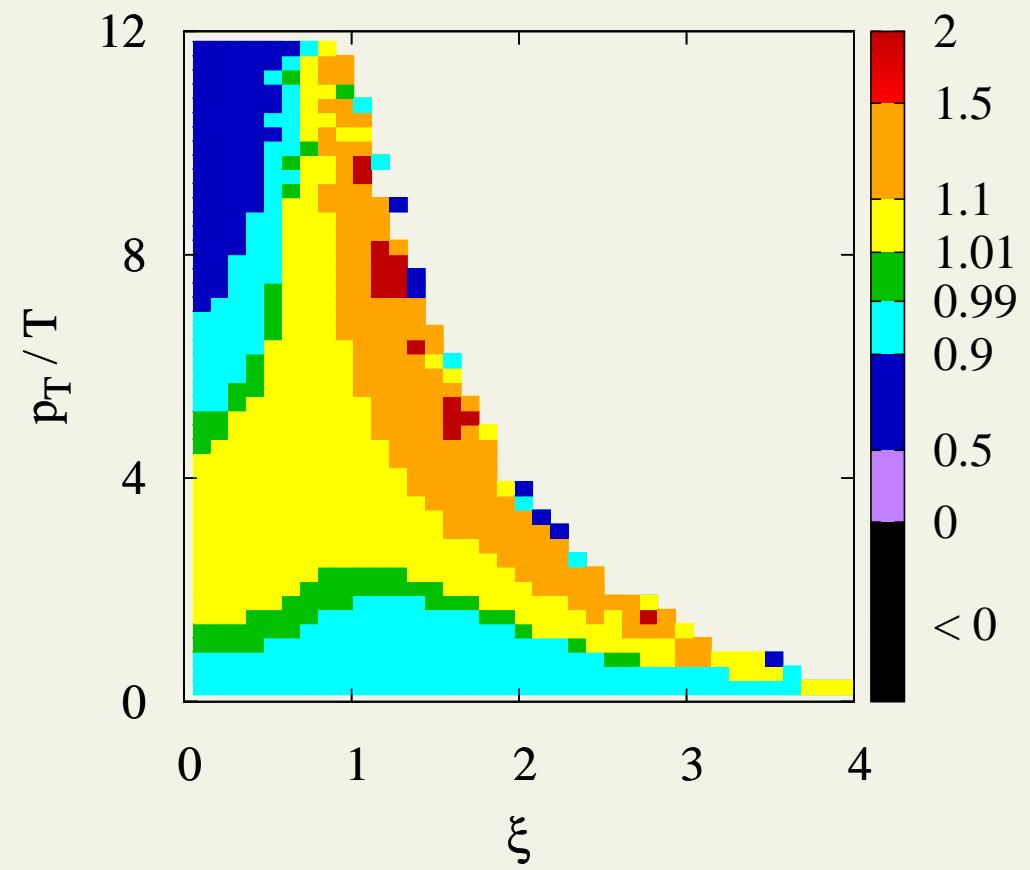


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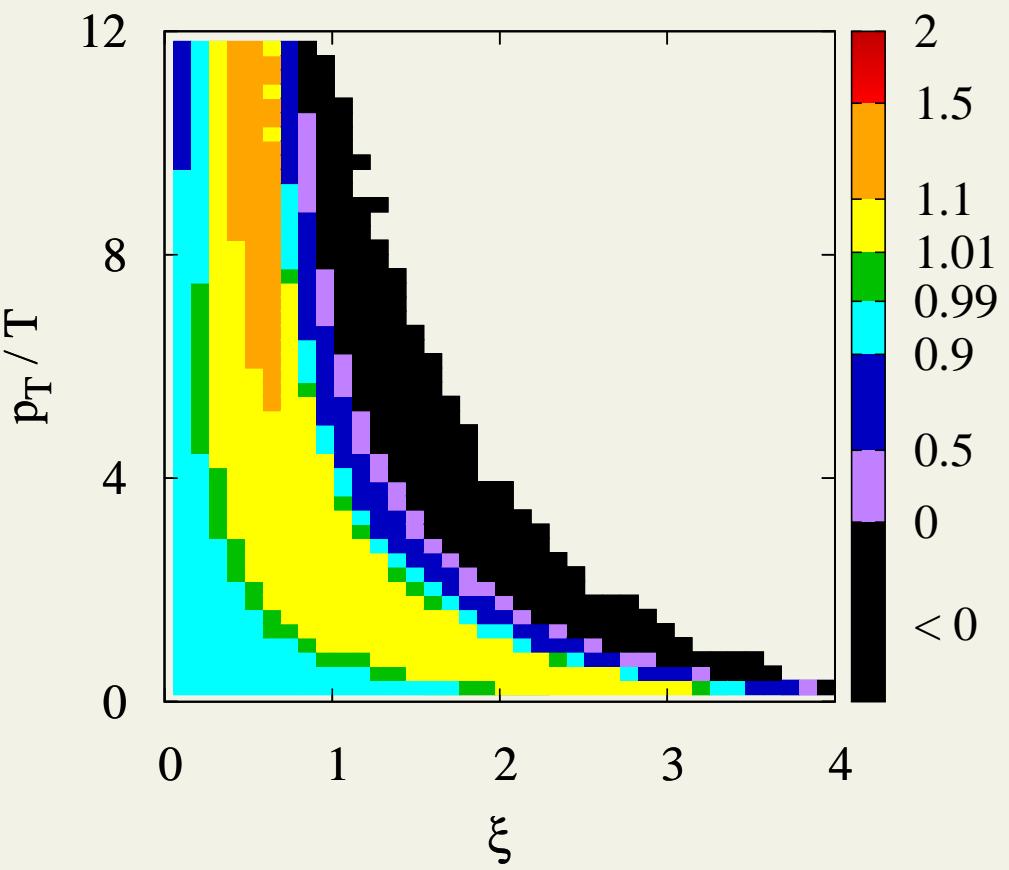


$$\frac{\tau}{\tau_0} = 6, \quad K = 2 \left(\frac{\tau}{\tau_0} \right)^{2/3} \quad \left(\frac{\tau_{REL}}{\tau_{exp}} = 0.16, \quad \frac{\pi_L}{p} = -0.17 \right)$$

SR ansatz

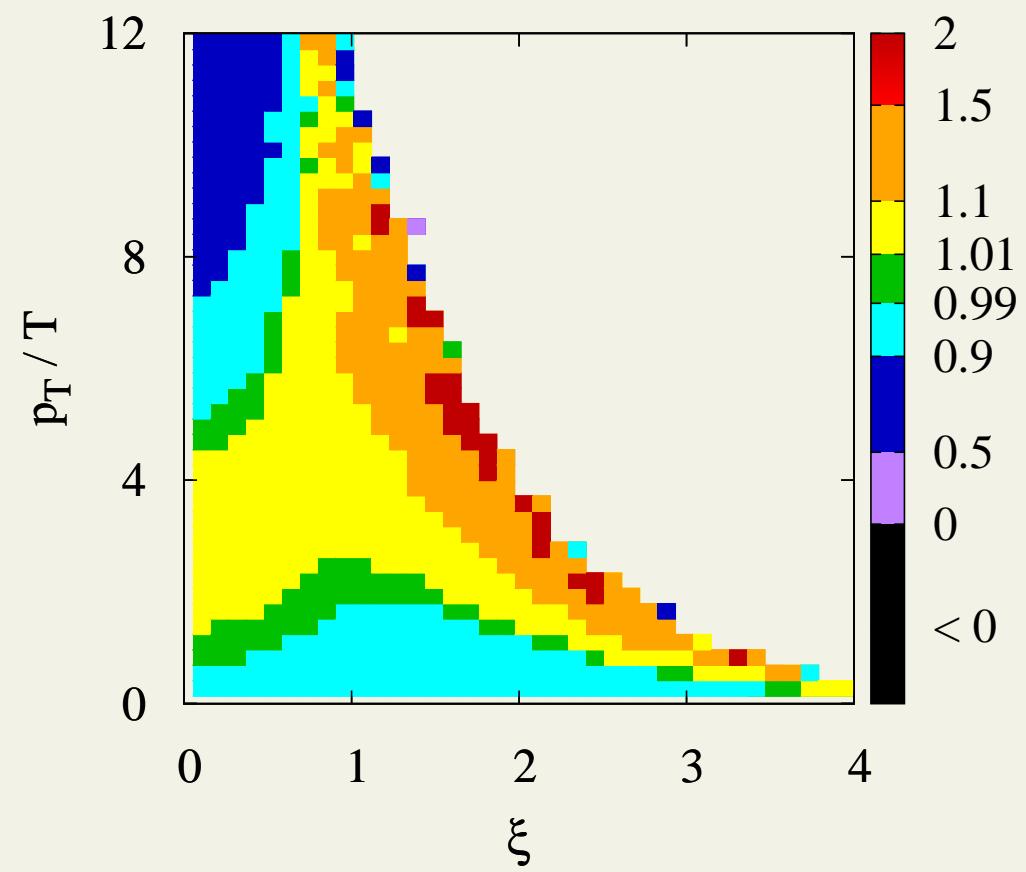


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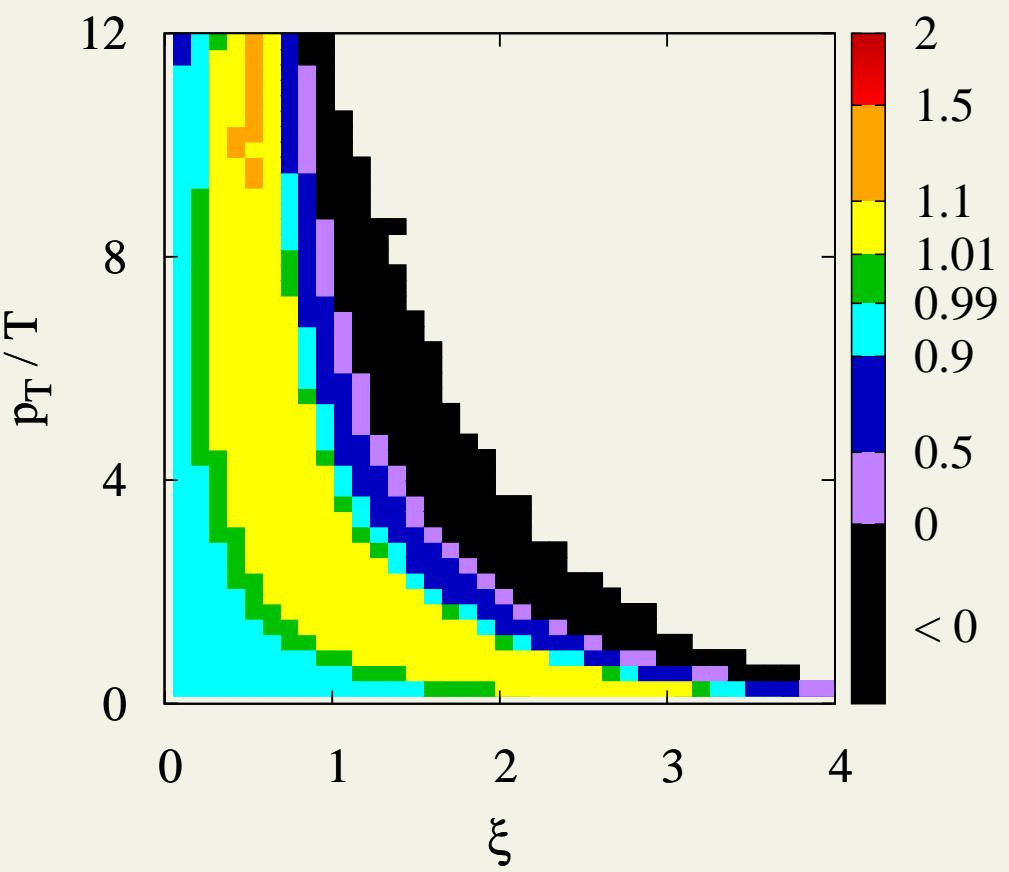


$$\frac{\tau}{\tau_0} = 8, \quad K = 2 \left(\frac{\tau}{\tau_0} \right)^{2/3} \quad \left(\frac{\tau_{REL}}{\tau_{exp}} = 0.13, \quad \frac{\pi_L}{p} = -0.14 \right)$$

SR ansatz

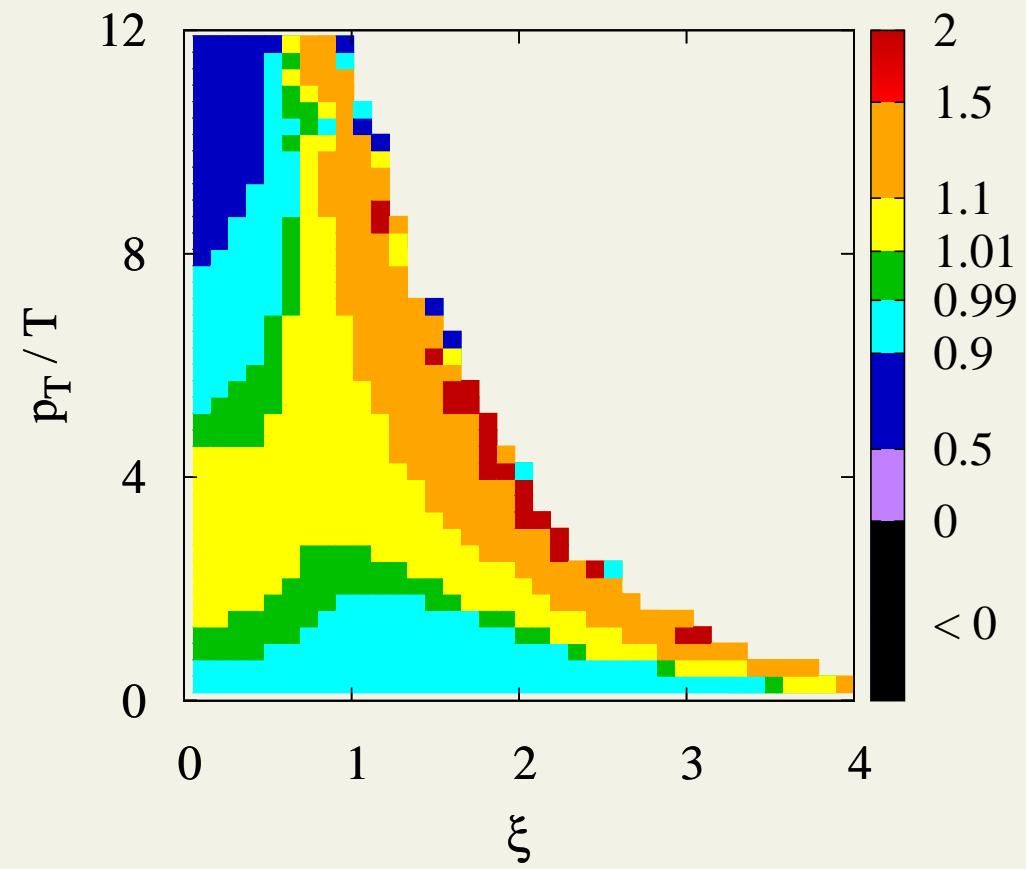


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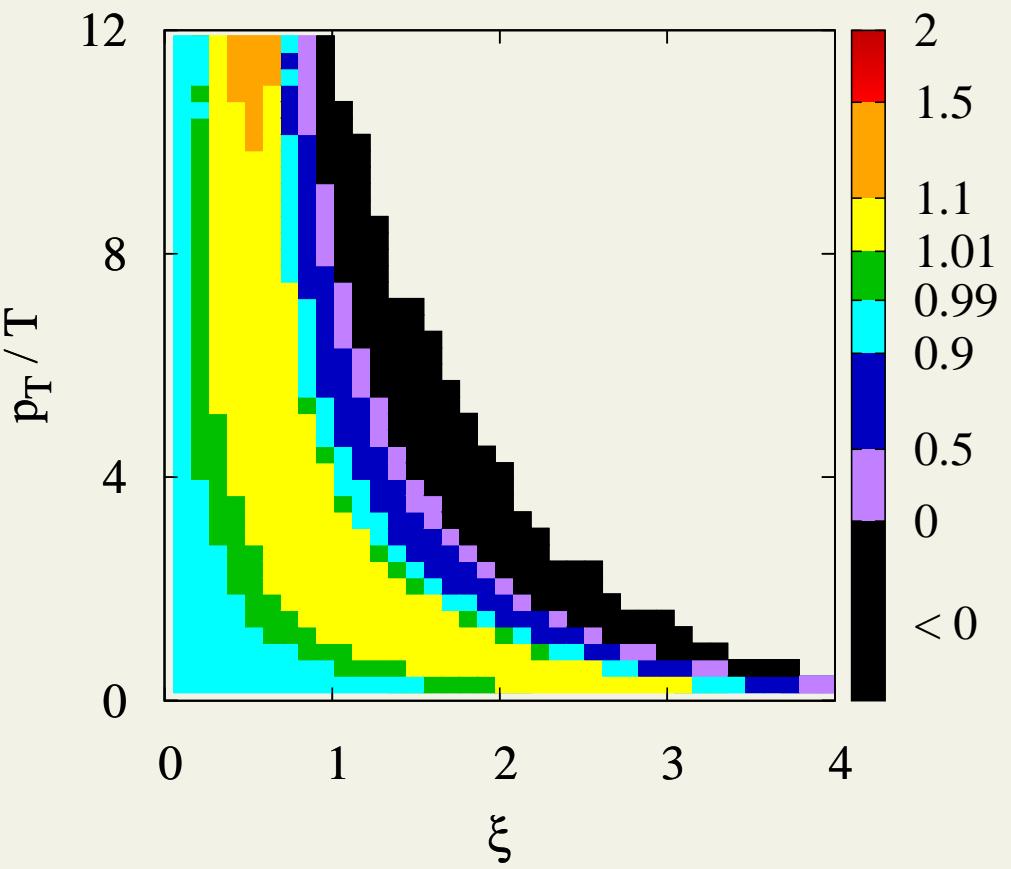


$$\frac{\tau}{\tau_0} = 10, \quad K = 2 \left(\frac{\tau}{\tau_0} \right)^{2/3} \quad \left(\frac{\tau_{REL}}{\tau_{exp}} = 0.11, \quad \frac{\pi_L}{p} = -0.12 \right)$$

SR ansatz

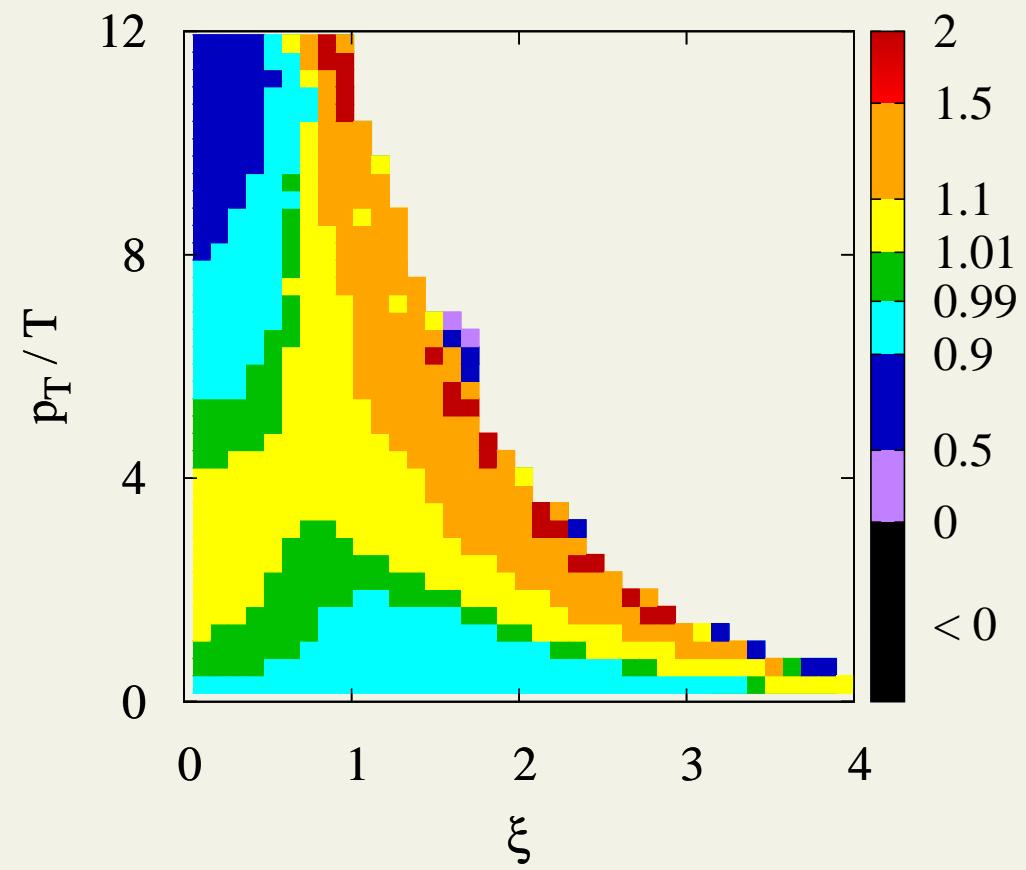


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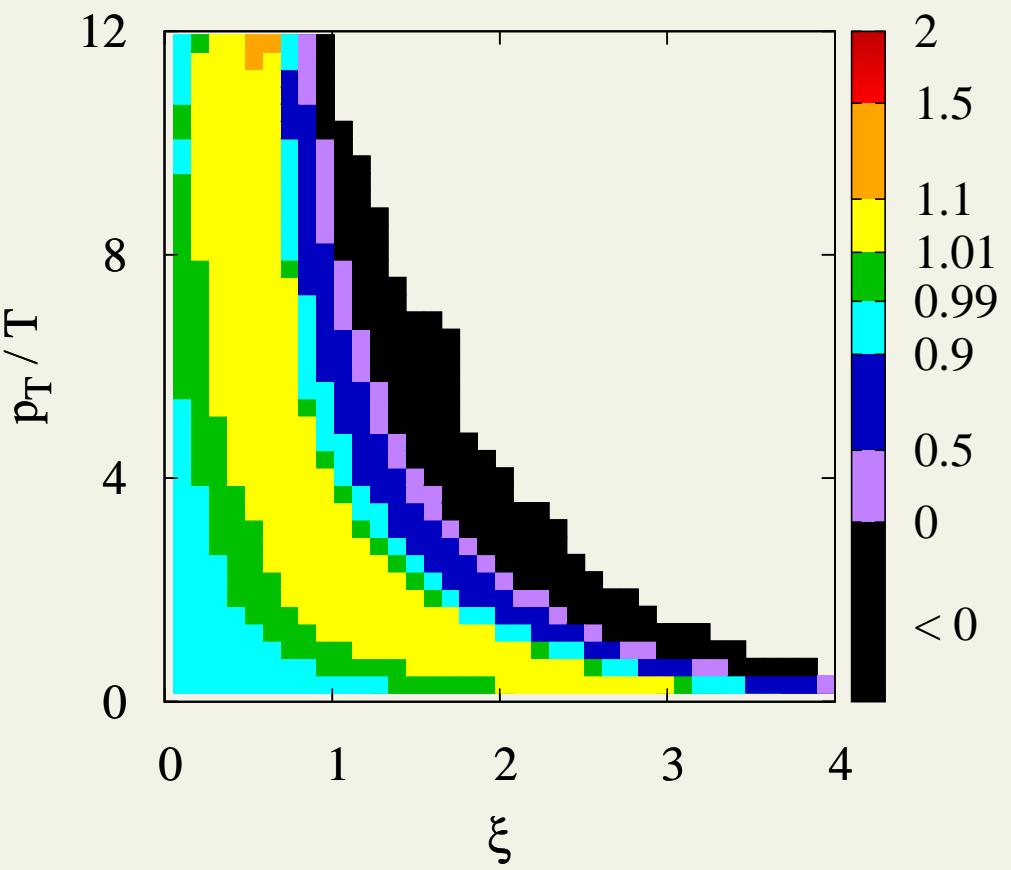


$$\frac{\tau}{\tau_0} = 12, \quad K = 2 \left(\frac{\tau}{\tau_0} \right)^{2/3} \quad \left(\frac{\tau_{REL}}{\tau_{exp}} = 0.10, \quad \frac{\pi_L}{p} = -0.11 \right)$$

SR ansatz

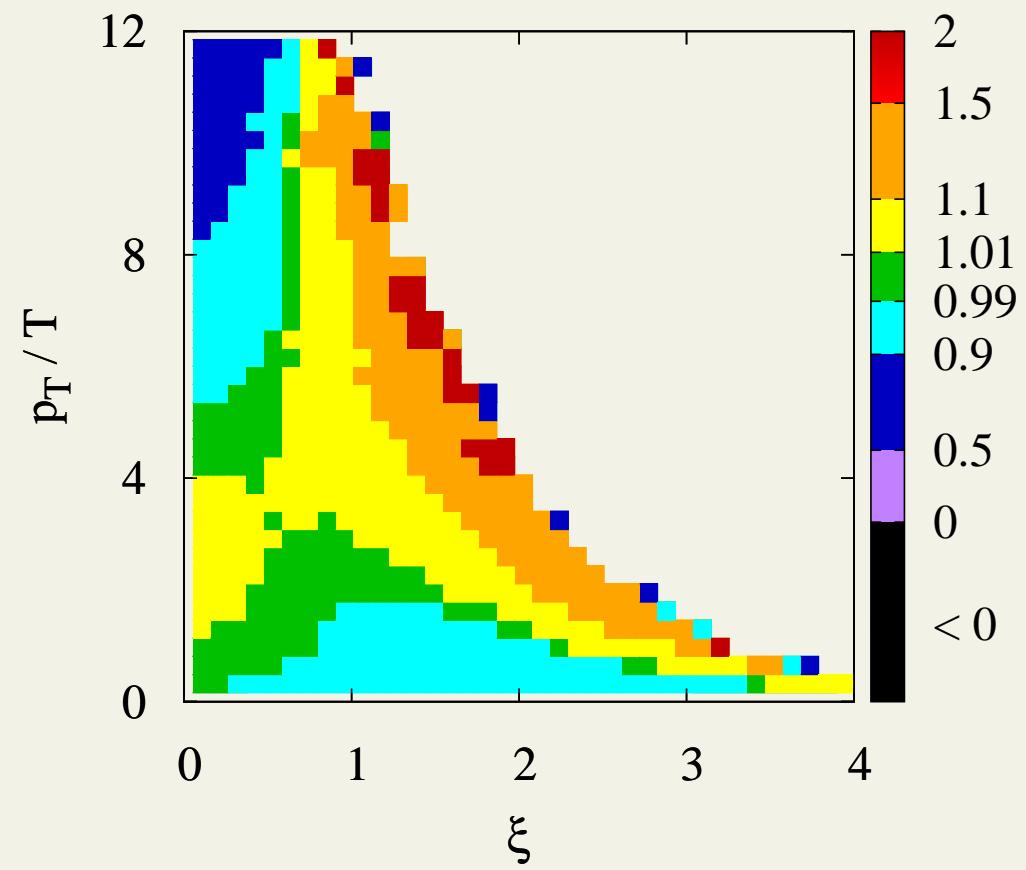


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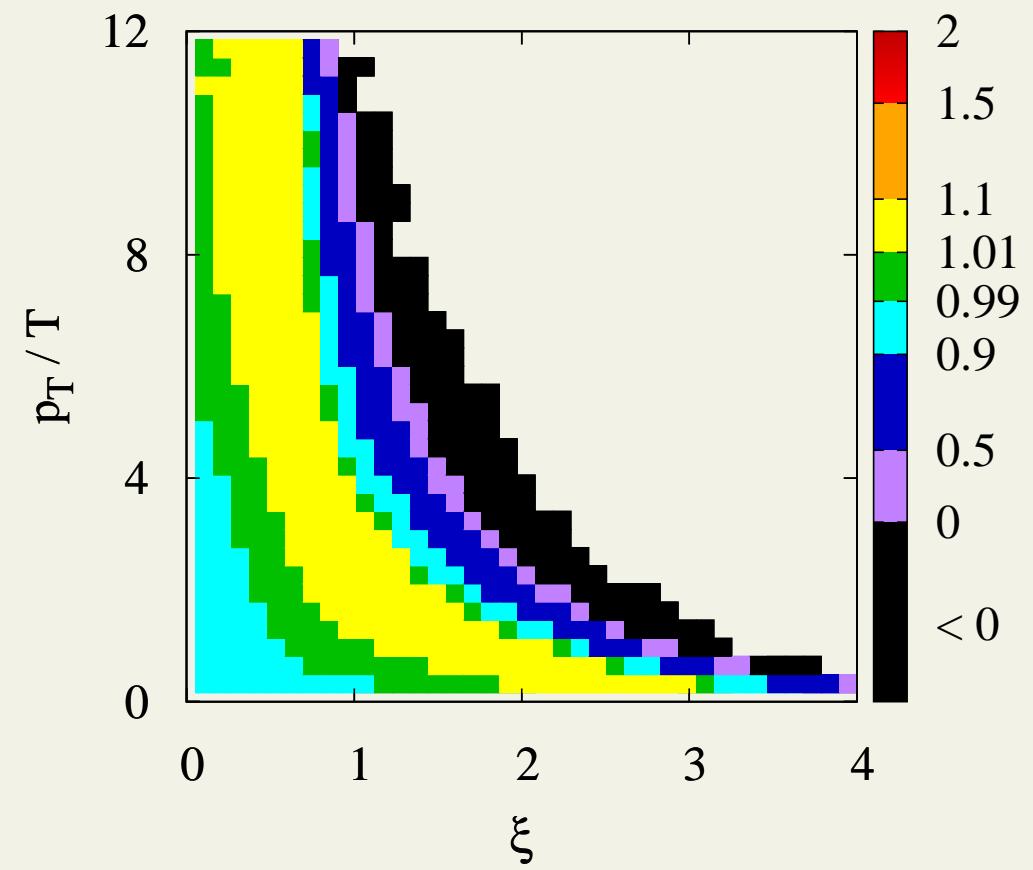


$$\frac{\tau}{\tau_0} = 14, \quad K = 2 \left(\frac{\tau}{\tau_0} \right)^{2/3} \quad \left(\frac{\tau_{REL}}{\tau_{exp}} = 0.09, \quad \frac{\pi_L}{p} = -0.10 \right)$$

SR ansatz

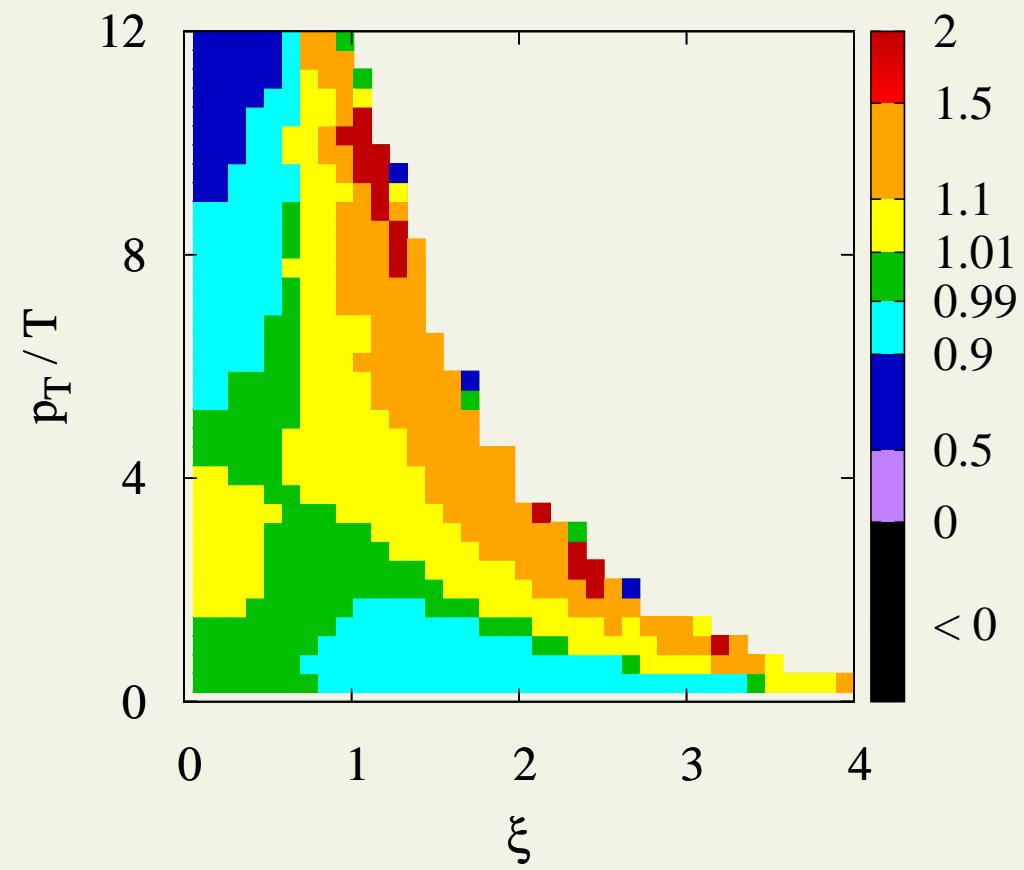


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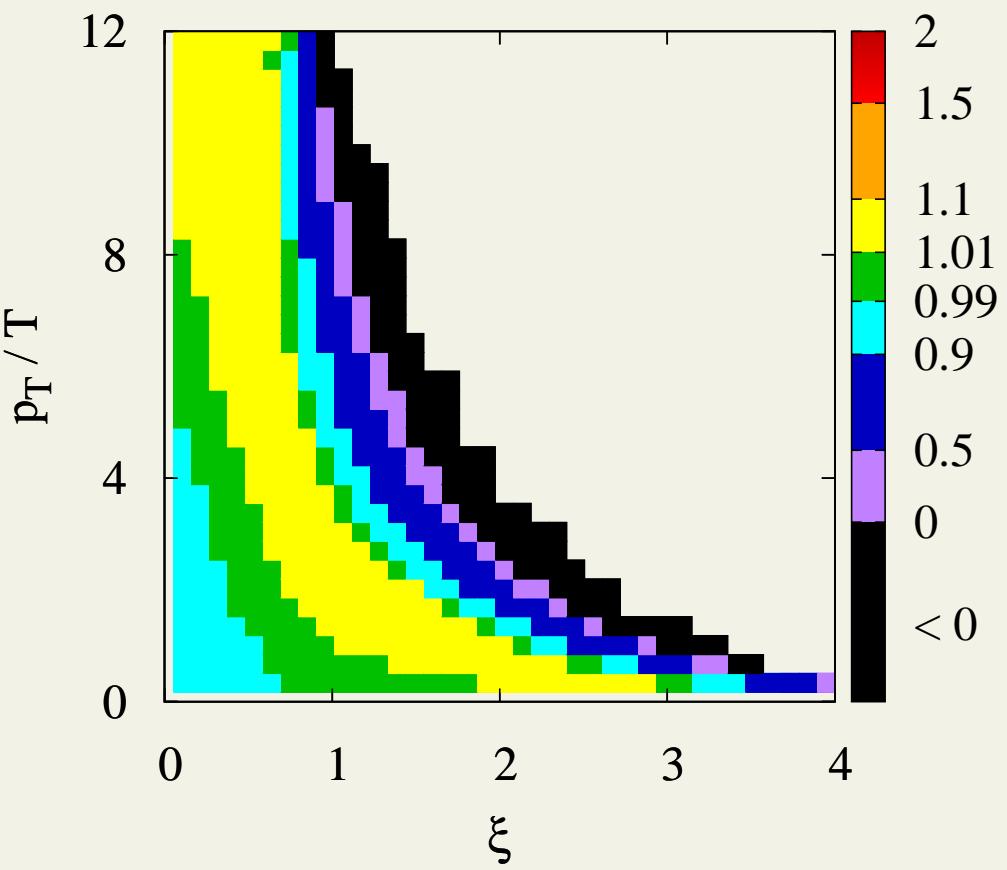


$$\frac{\tau}{\tau_0} = 16, \quad K = 2 \left(\frac{\tau}{\tau_0} \right)^{2/3} \quad \left(\frac{\tau_{REL}}{\tau_{exp}} = 0.08, \quad \frac{\pi_L}{p} = -0.09 \right)$$

SR ansatz

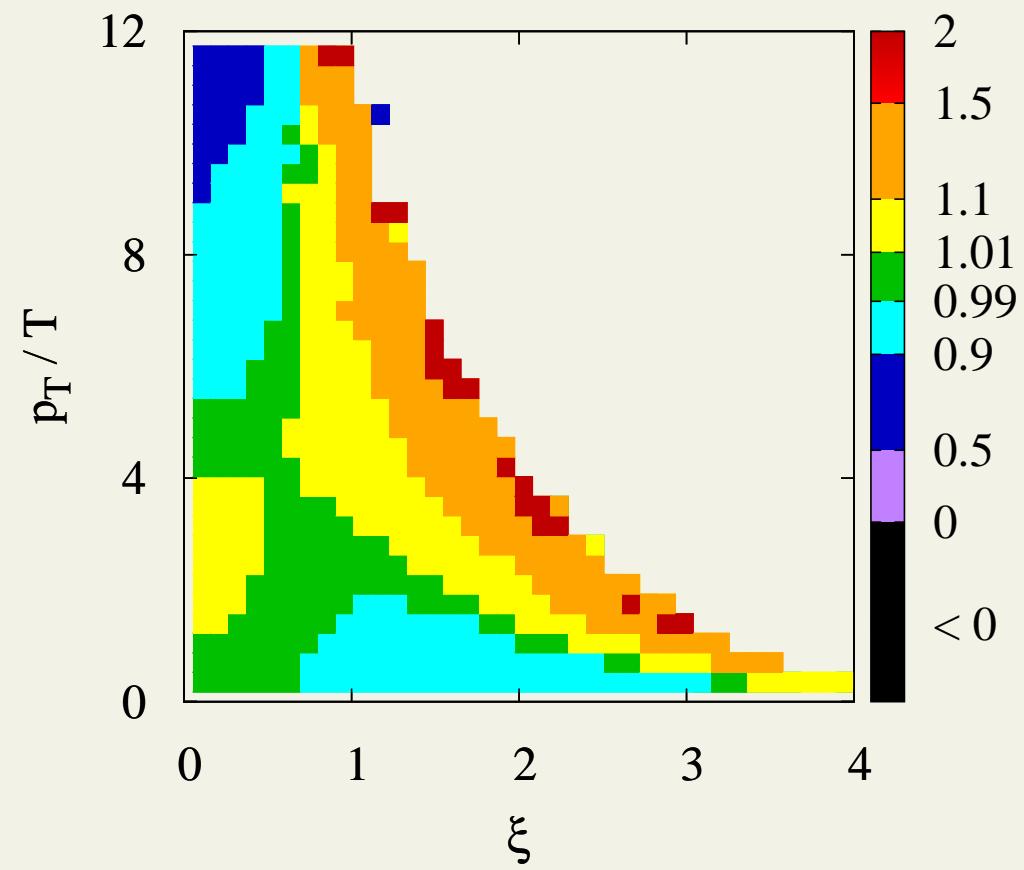


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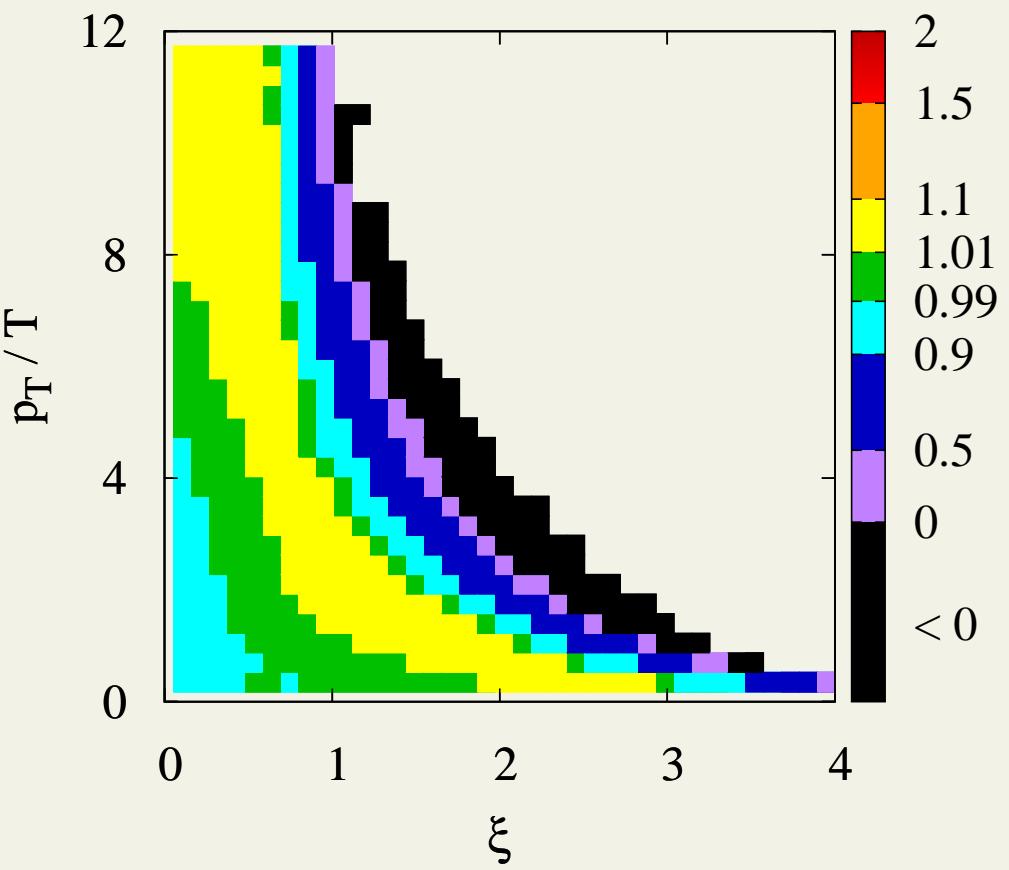


$$\frac{\tau}{\tau_0} = 18, \quad K = 2 \left(\frac{\tau}{\tau_0} \right)^{2/3} \quad \left(\frac{\tau_{REL}}{\tau_{exp}} = 0.08, \quad \frac{\pi_L}{p} = -0.08 \right)$$

SR ansatz

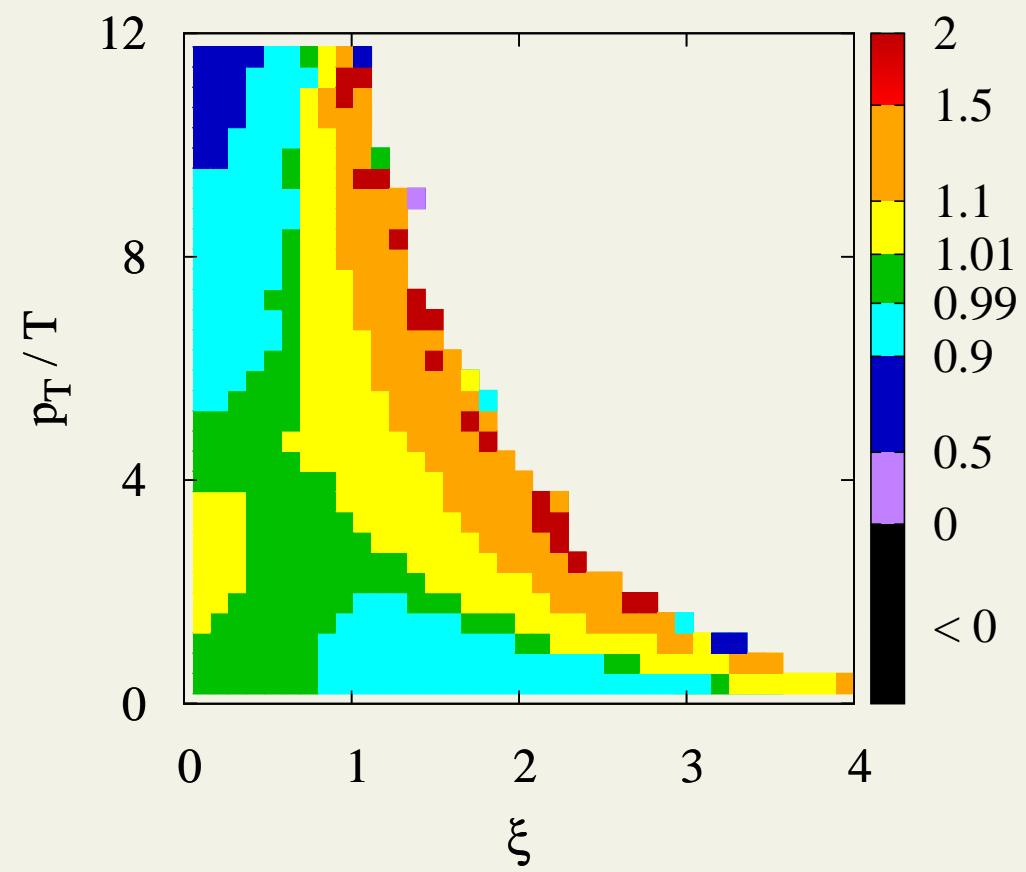


Grad (IS)

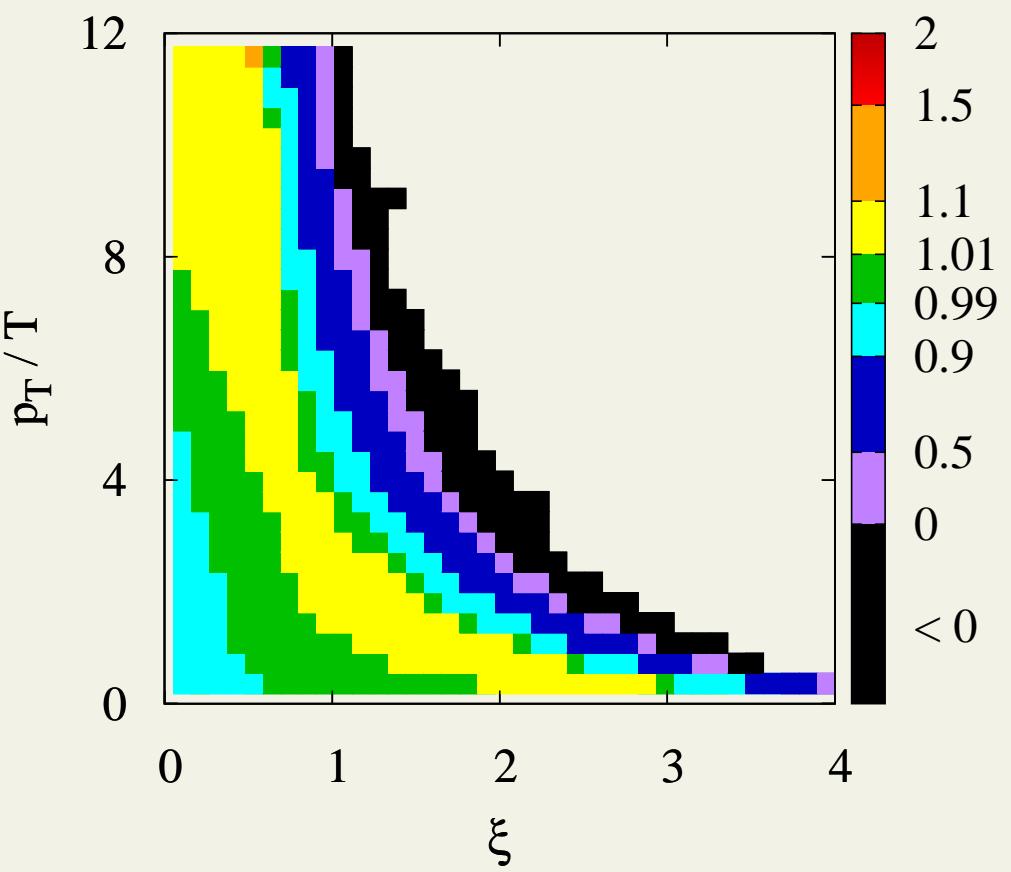


$$\frac{\tau}{\tau_0} = 20, \quad K = 2 \left(\frac{\tau}{\tau_0} \right)^{2/3} \quad \left(\frac{\tau_{REL}}{\tau_{exp}} = 0.07, \quad \frac{\pi_L}{p} = -0.08 \right)$$

SR ansatz



Grad (IS)



\Rightarrow

At early times or high ξ , SR looks better

At high pT and small ξ , Grad looks better.

Now compare four models:

a) SR, b) IS/Grad, c) IS with $p^{1.5}$, d) IS with p^1 (RTA)

study viscosity dependence $\frac{\eta}{s} \sim 0.03 - 0.2$ [$K_0 = 1, 2, 6.49$]

$$\frac{\eta}{s} \sim 0.2 \quad [K_0 = 1]$$

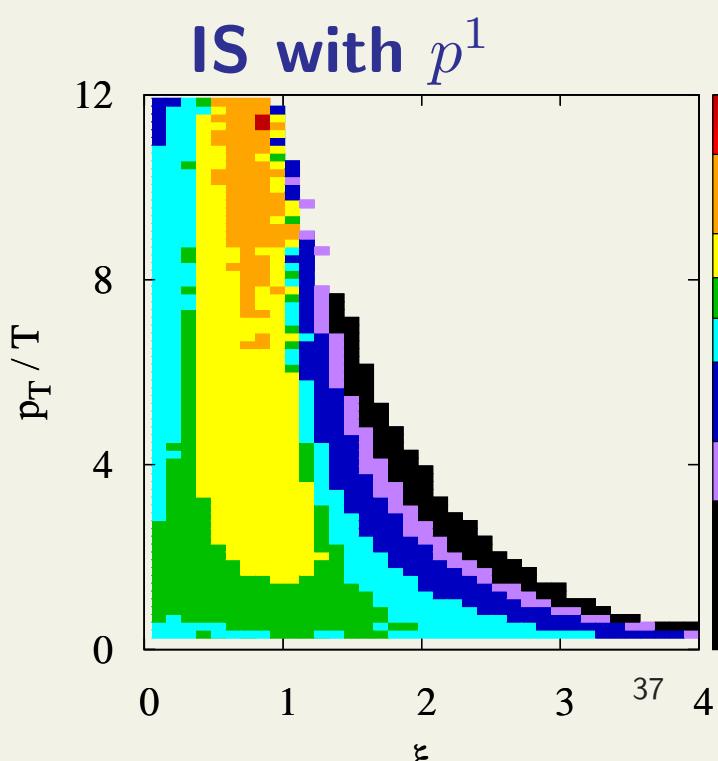
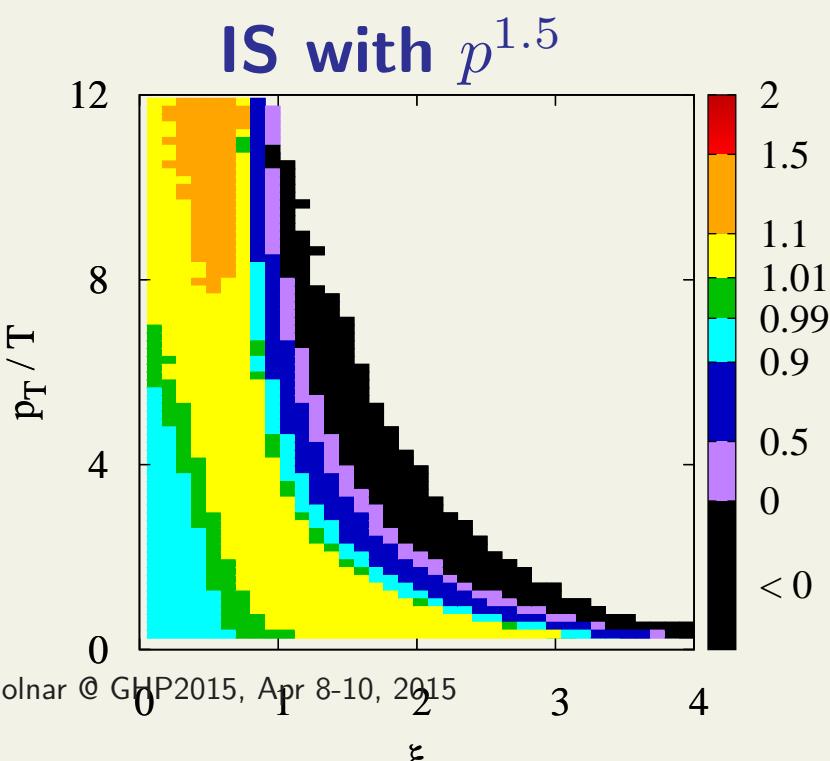
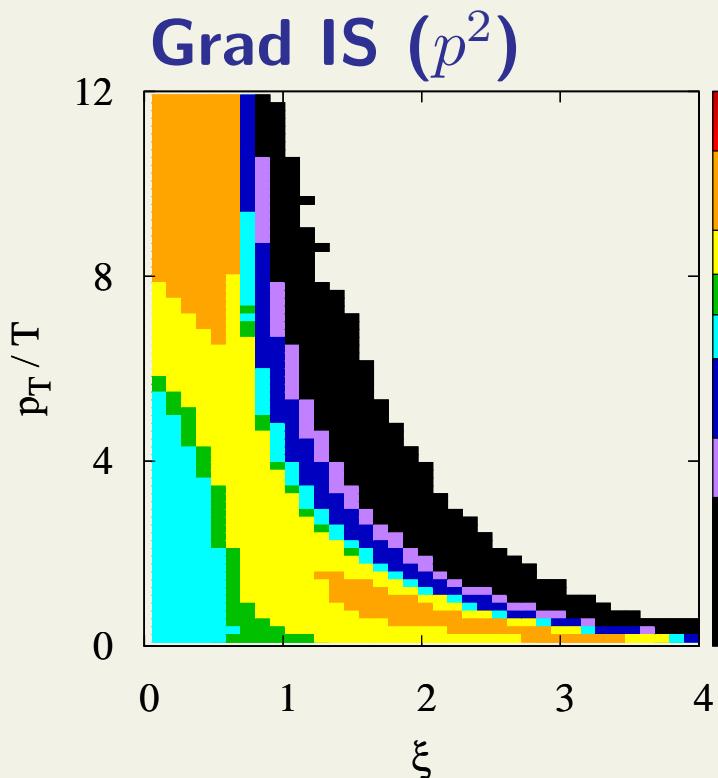
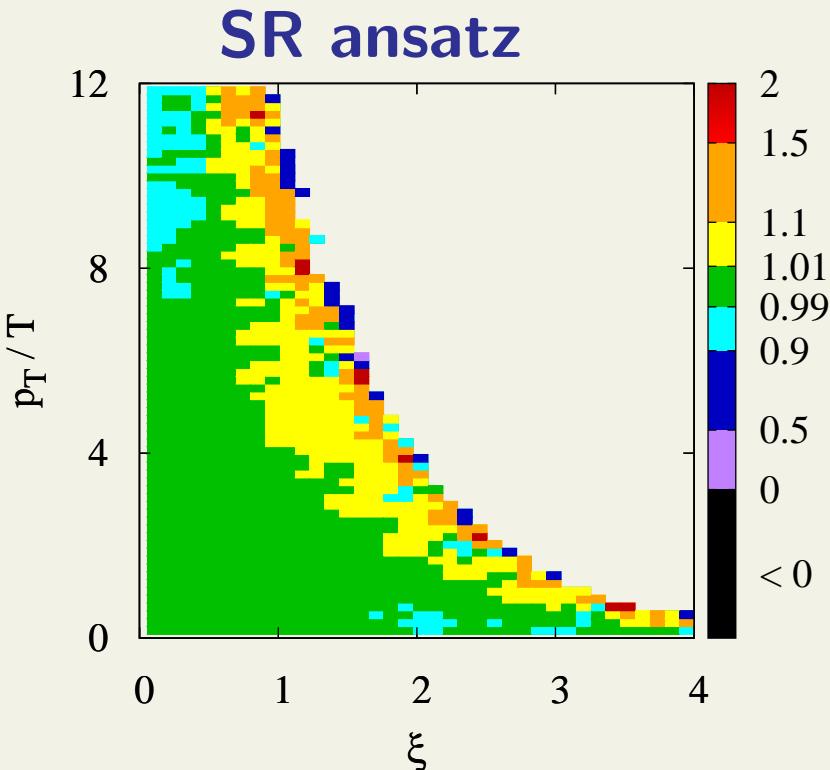
$$\frac{\tau}{\tau_0} = 1.2$$

$$K = 1 \left(\frac{\tau}{\tau_0} \right)^{2/3}$$

$$\left(\frac{\tau_{REL}}{\tau_{exp}} = 0.93, \right.$$

$$\left. \frac{\pi_L}{p} = -0.17 \right)$$

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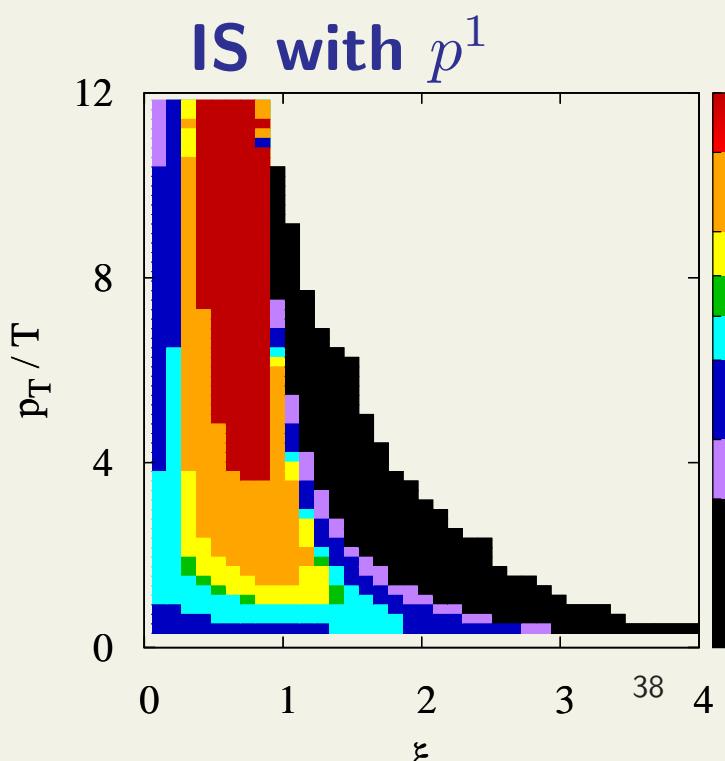
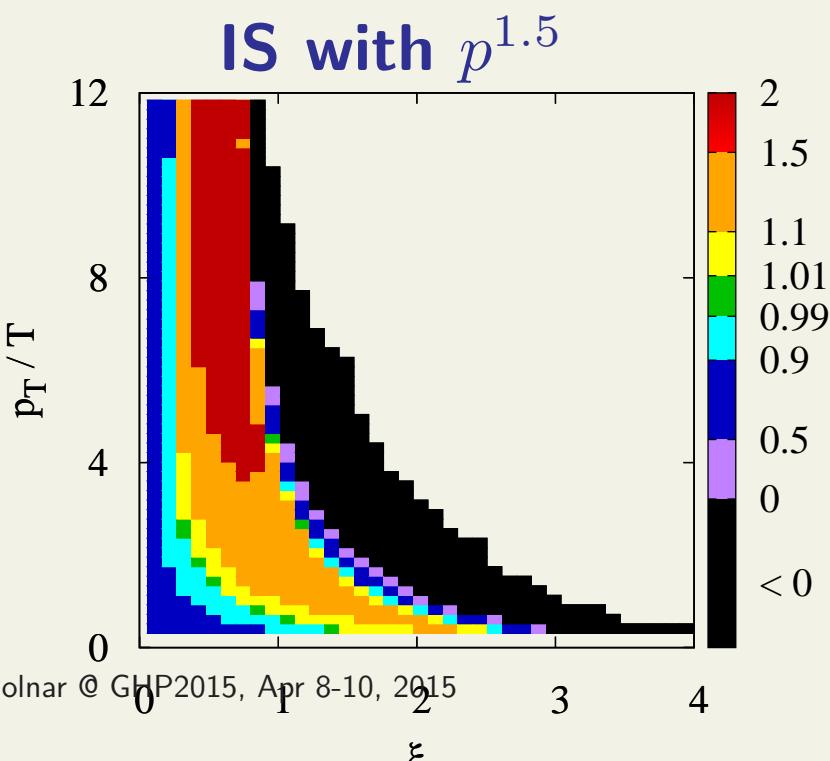
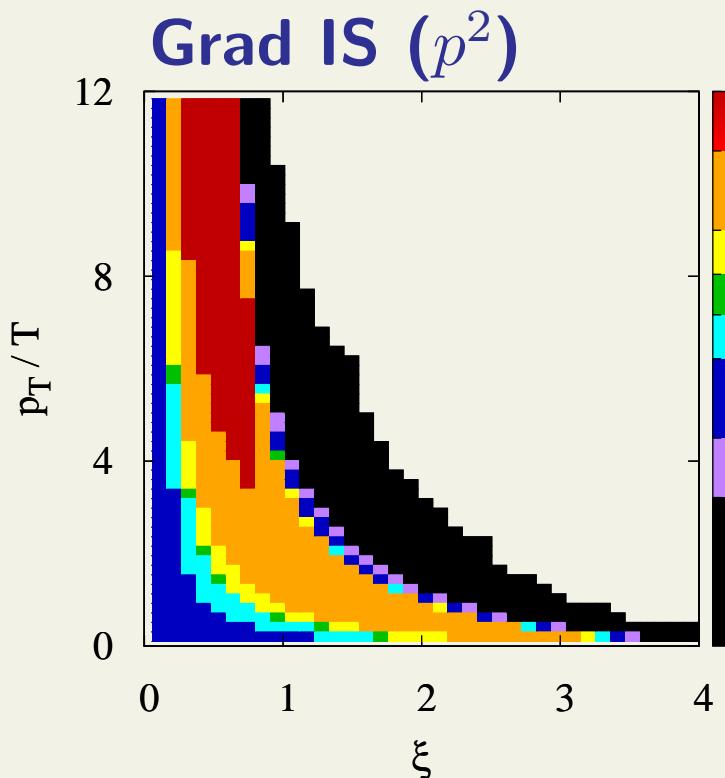
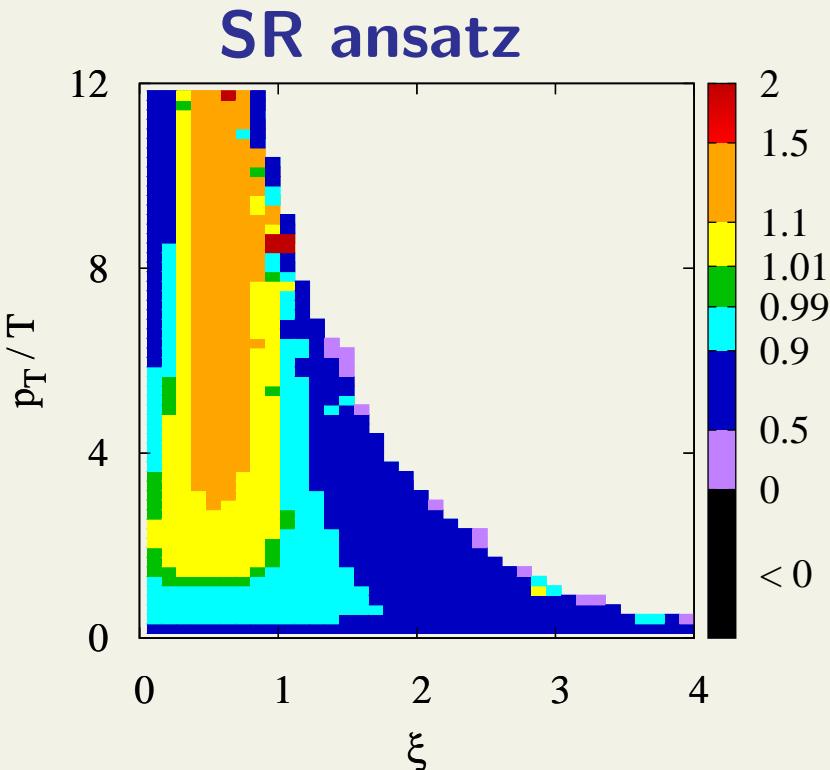
$$\frac{\tau}{\tau_0} = 3$$

$$K = 1 \left(\frac{\tau}{\tau_0} \right)^{2/3}$$

$$\left(\frac{\tau_{REL}}{\tau_{exp}} = 0.51, \right.$$

$$\left. \frac{\pi_L}{p} = -0.41 \right)$$

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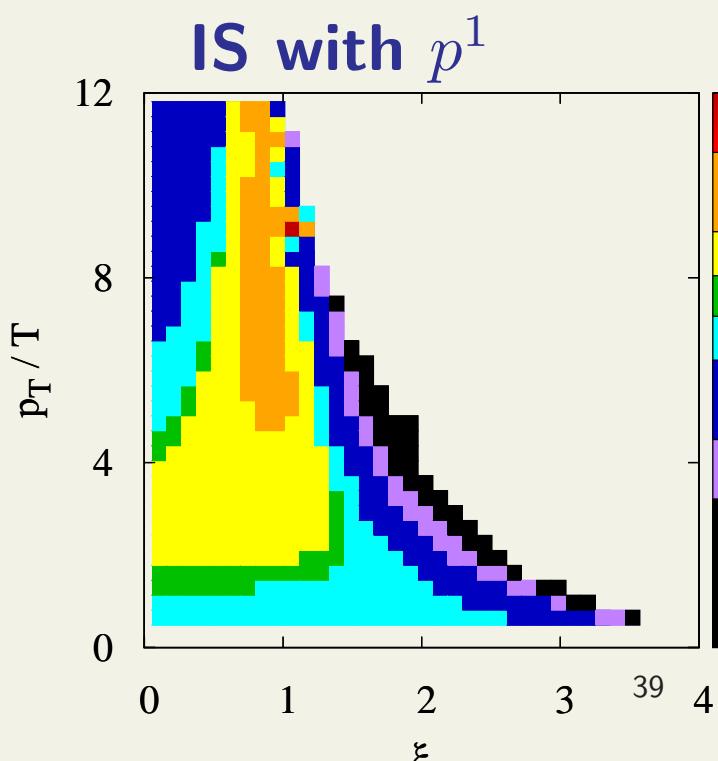
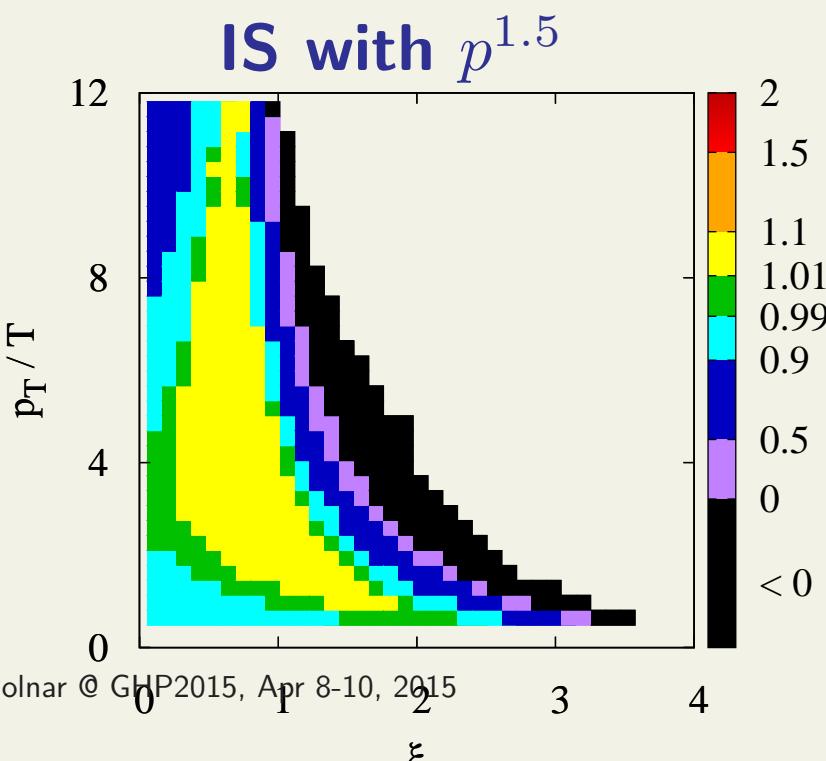
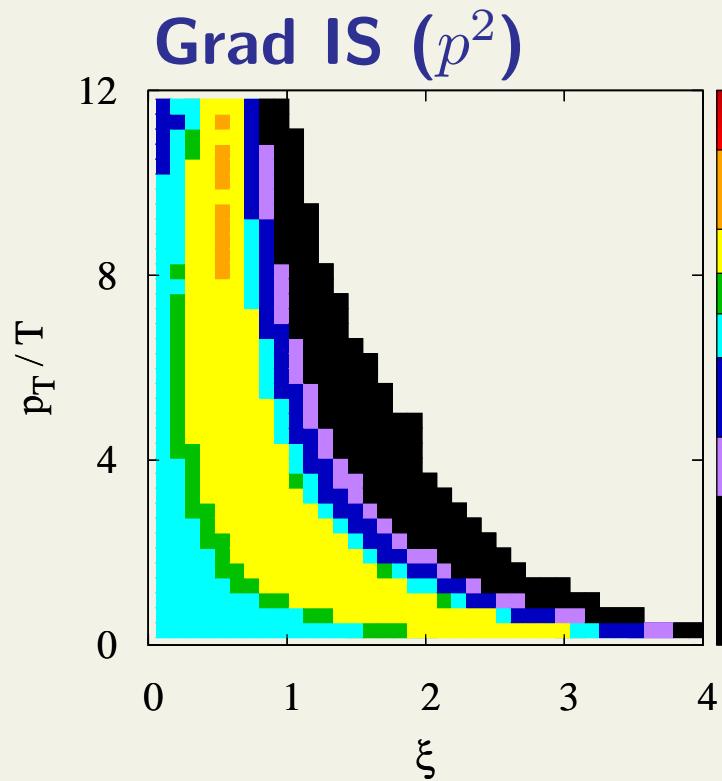
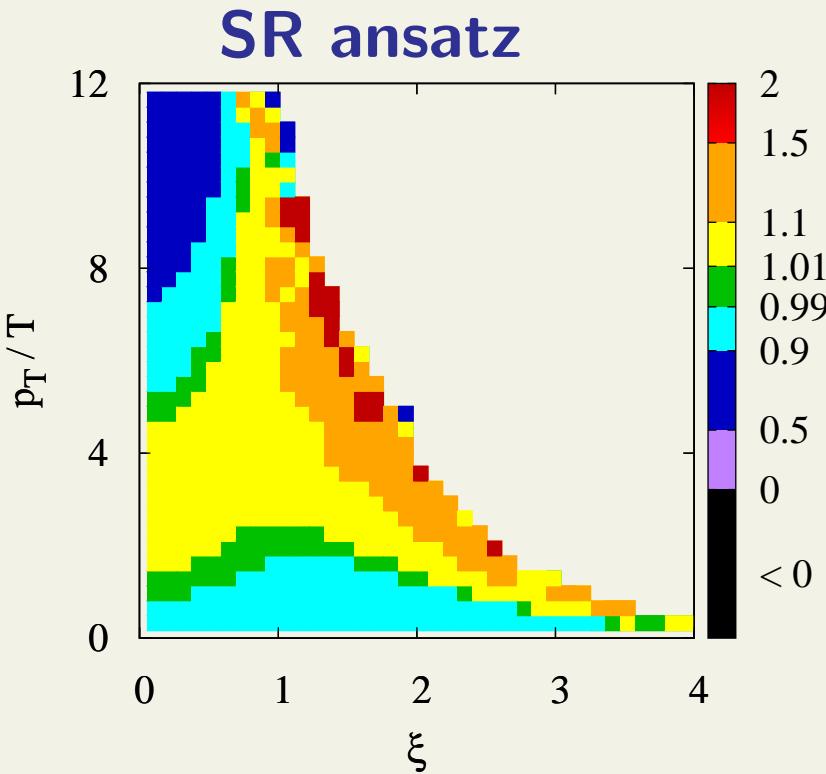
$$\frac{\tau}{\tau_0} = 20$$

$$K = 1 \left(\frac{\tau}{\tau_0} \right)^{2/3}$$

$$\left(\frac{\tau_{REL}}{\tau_{exp}} = 14, \right.$$

$$\left. \frac{\pi_L}{p} = -0.16 \right)$$

$+100\%$
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 $+10\%$
 $\pm 1\%$
 -10%
 -50%
 -100%
 < 0



$$\frac{\eta}{s} \sim 0.1 \quad [K_0 = 2]$$

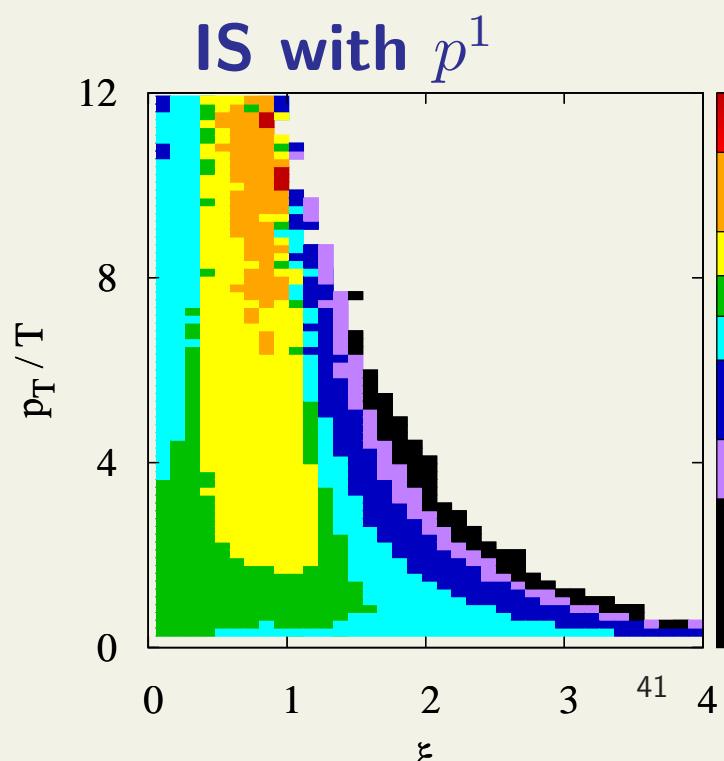
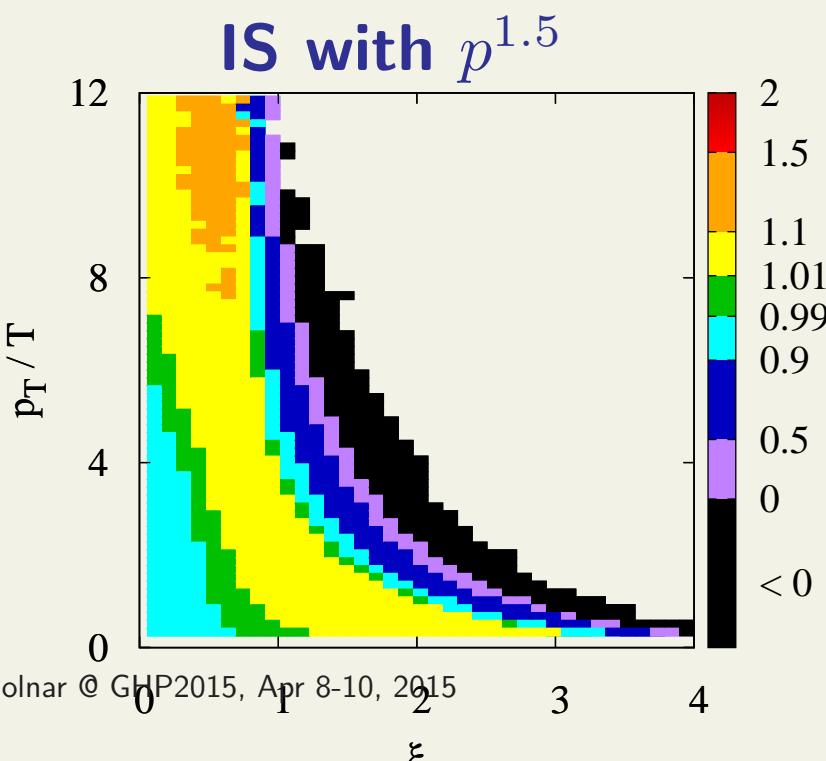
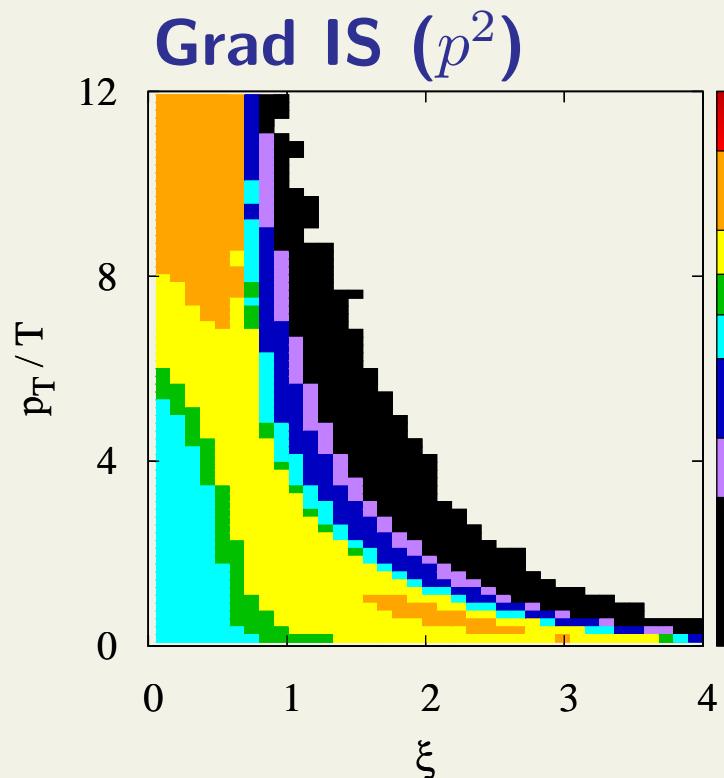
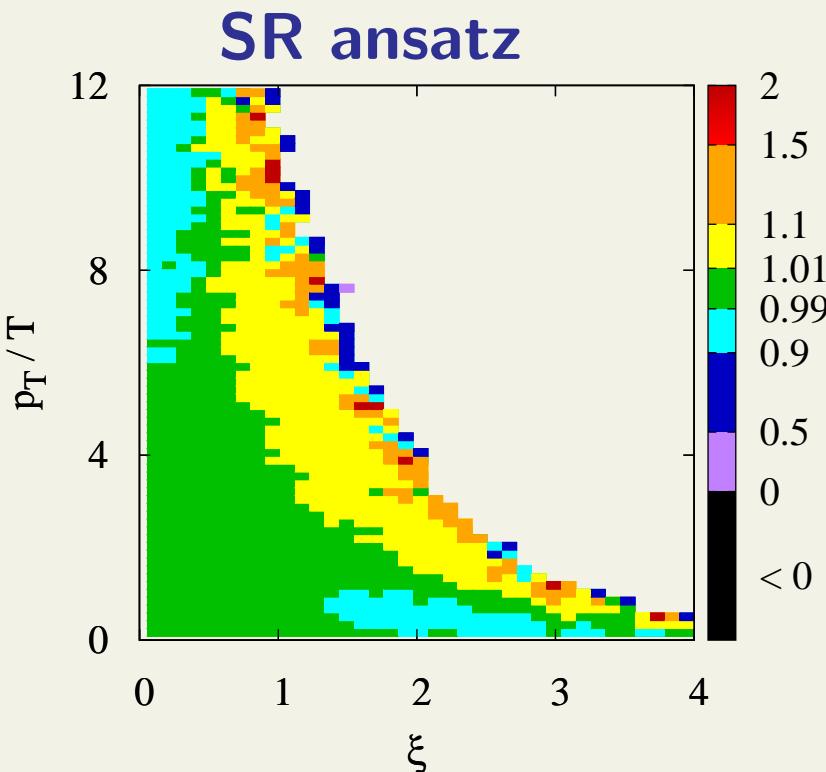
$$\frac{\tau}{\tau_0} = 1.2$$

$$K = 2 \left(\frac{\tau}{\tau_0} \right)^{2/3}$$

$$\left(\frac{\tau_{REL}}{\tau_{exp}} = 0.47, \right.$$

$$\left. \frac{\pi_L}{p} = -0.15 \right)$$

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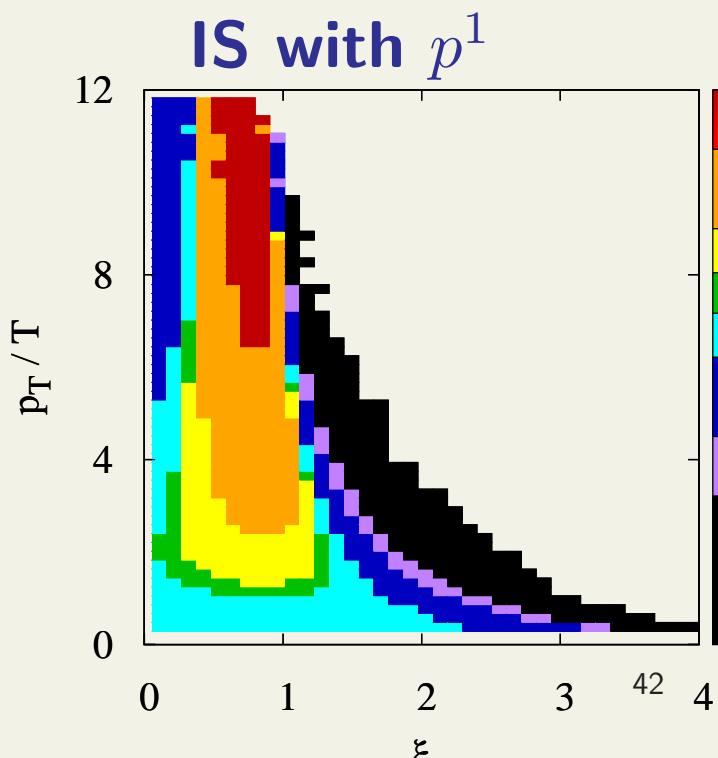
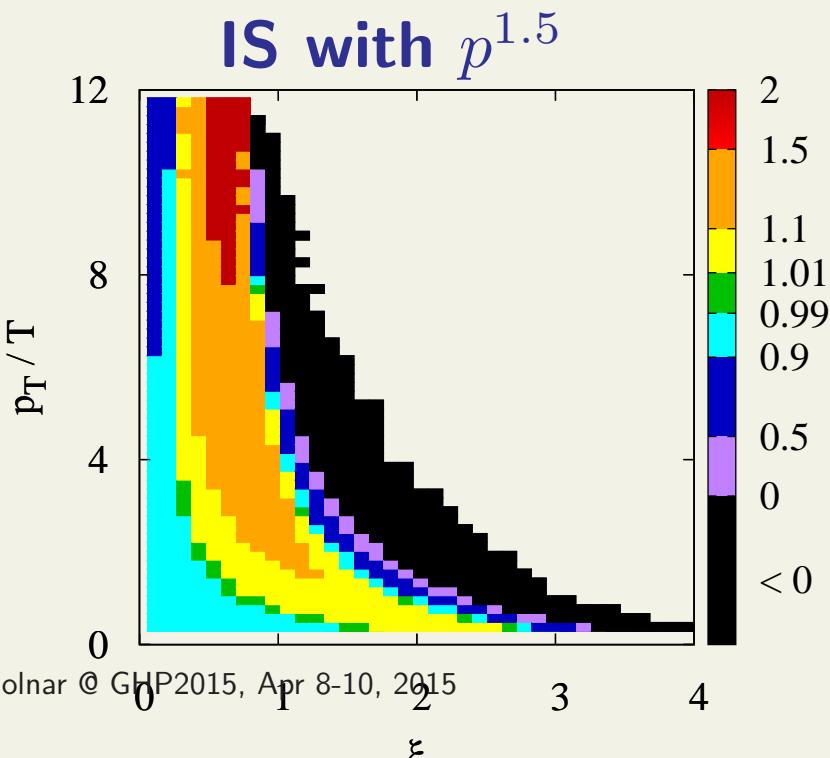
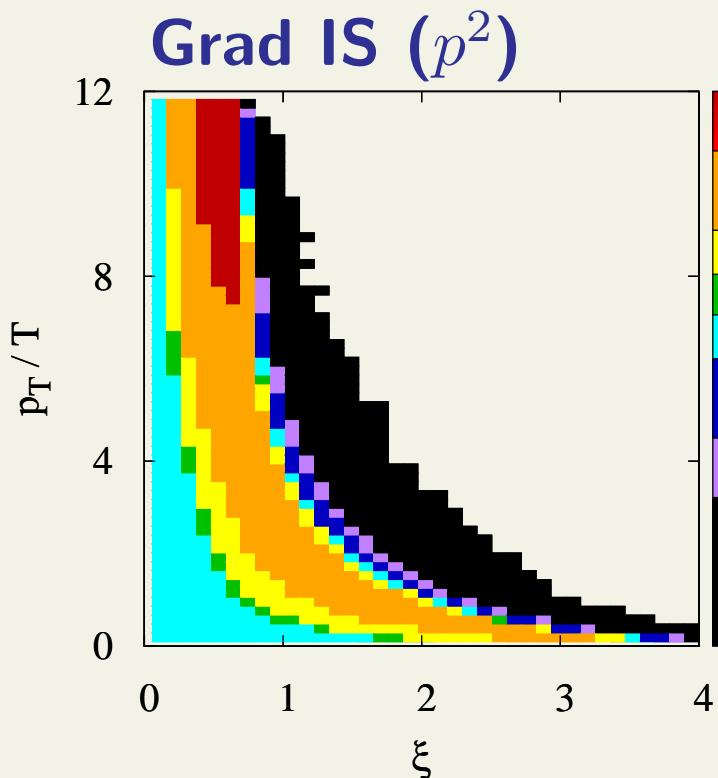
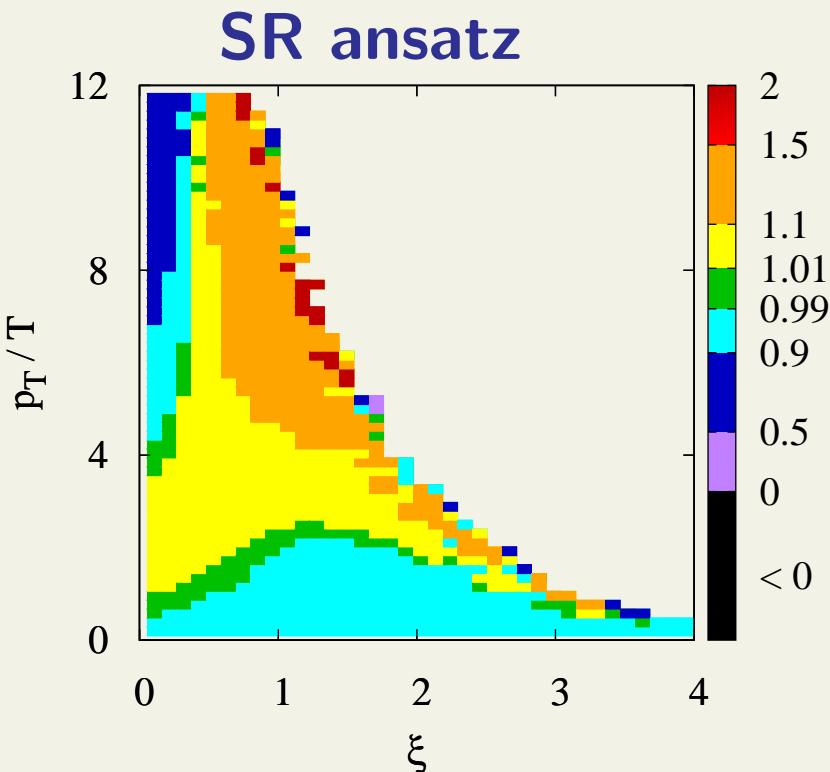
$$\frac{\tau}{\tau_0} = 2$$

$$K = 2 \left(\frac{\tau}{\tau_0} \right)^{2/3}$$

$$\left(\frac{\tau_{REL}}{\tau_{exp}} = 0.33, \right.$$

$$\left. \frac{\pi_L}{p} = -0.29 \right)$$

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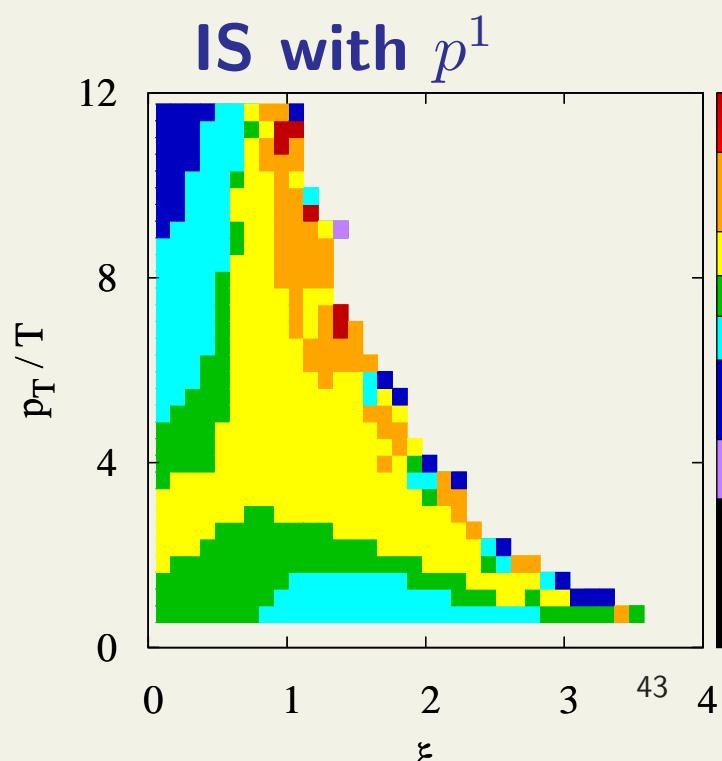
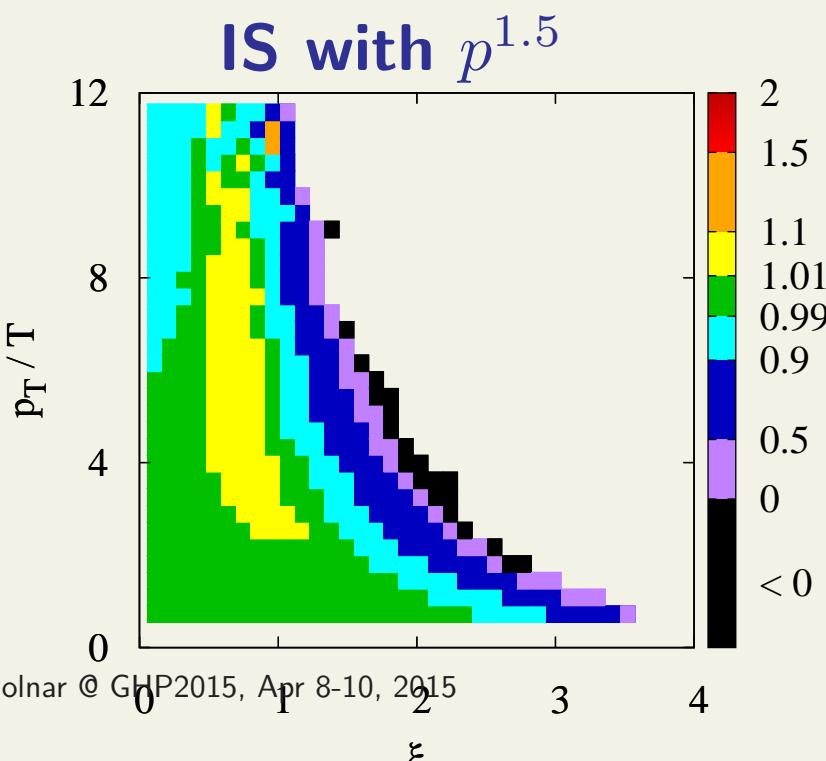
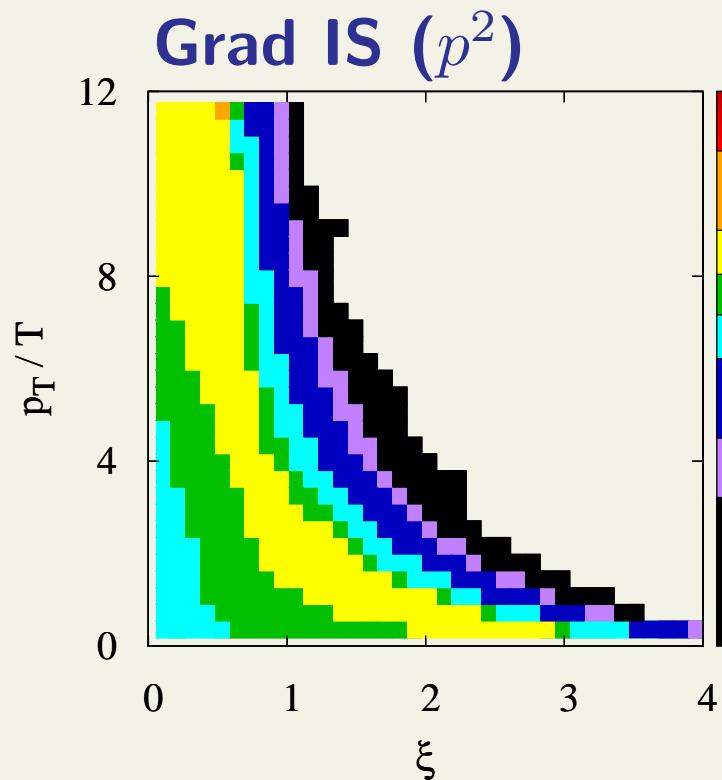
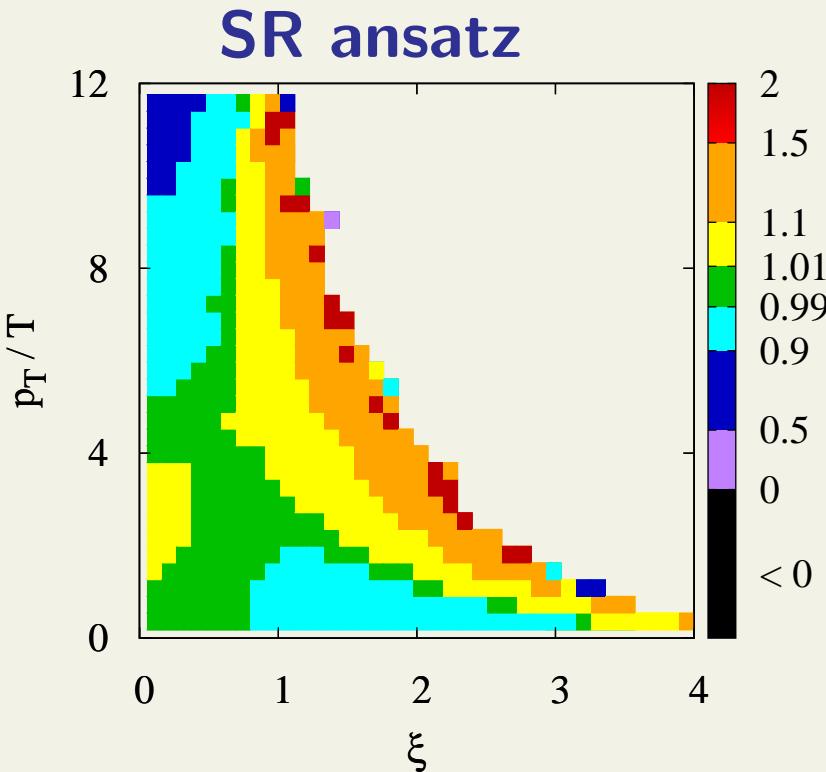
$$\frac{\tau}{\tau_0} = 20$$

$$K = 2 \left(\frac{\tau}{\tau_0} \right)^{2/3}$$

$$\left(\frac{\tau_{REL}}{\tau_{exp}} = 0.07, \right.$$

$$\left. \frac{\pi_L}{p} = -0.08 \right)$$

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$$\frac{\eta}{s} \sim 0.03 \quad [K_0 = 6.49]$$

$$\frac{\tau}{\tau_0} = 1.2$$

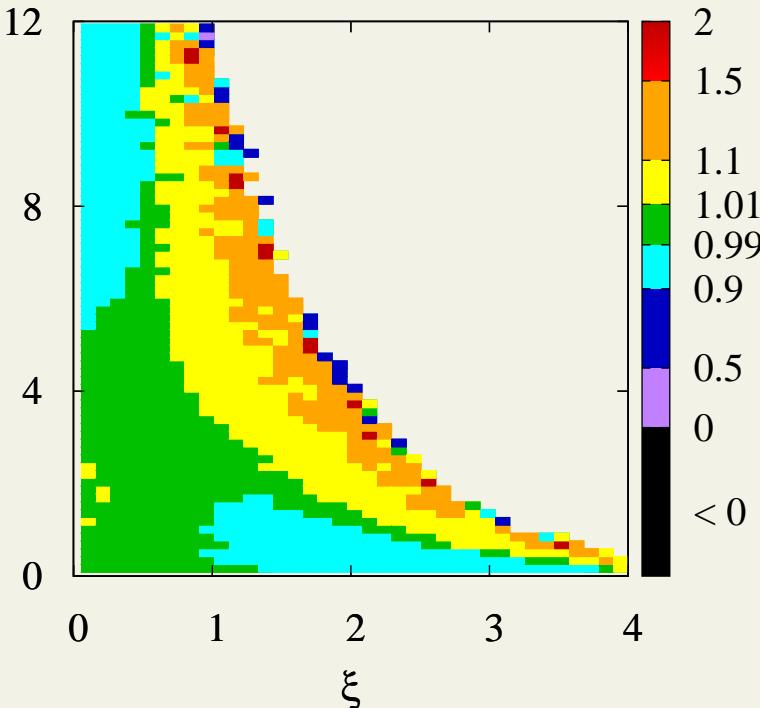
$$K = 6.49 \left(\frac{\tau}{\tau_0} \right)^{2/3}$$

$$\left(\frac{\tau_{REL}}{\tau_{exp}} = 0.14, \right.$$

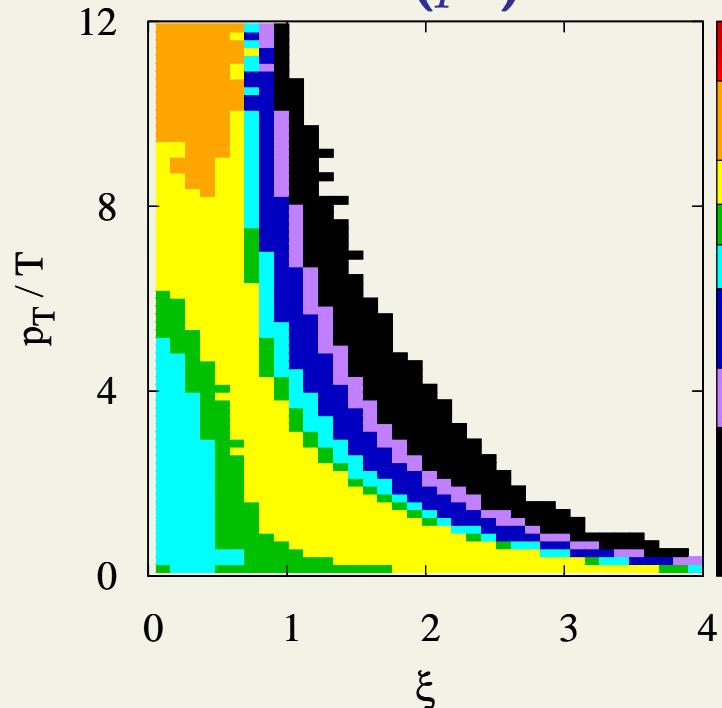
$$\left. \frac{\pi_L}{p} = -0.11 \right)$$

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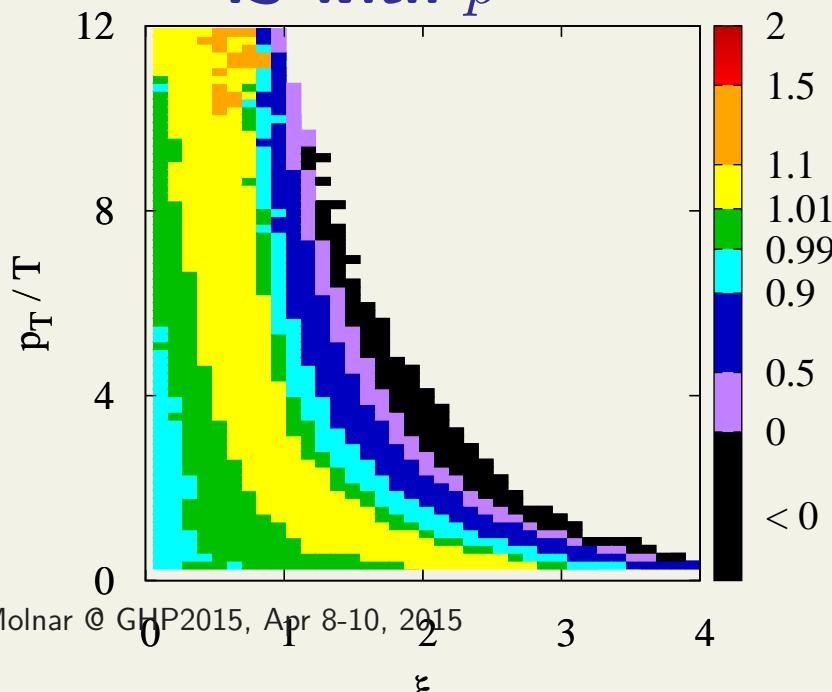
SR ansatz



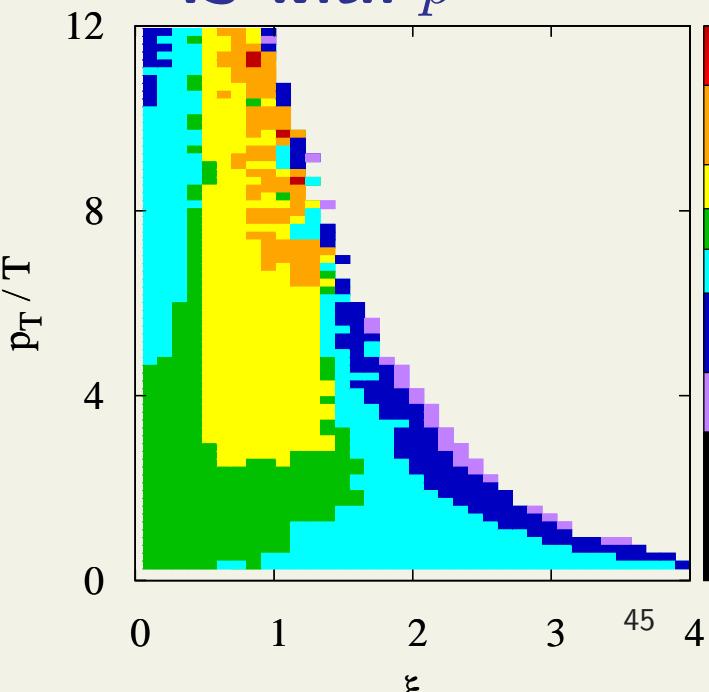
Grad IS (p^2)



IS with $p^{1.5}$



IS with p^1



$$\frac{\tau}{\tau_0} = 1.6$$

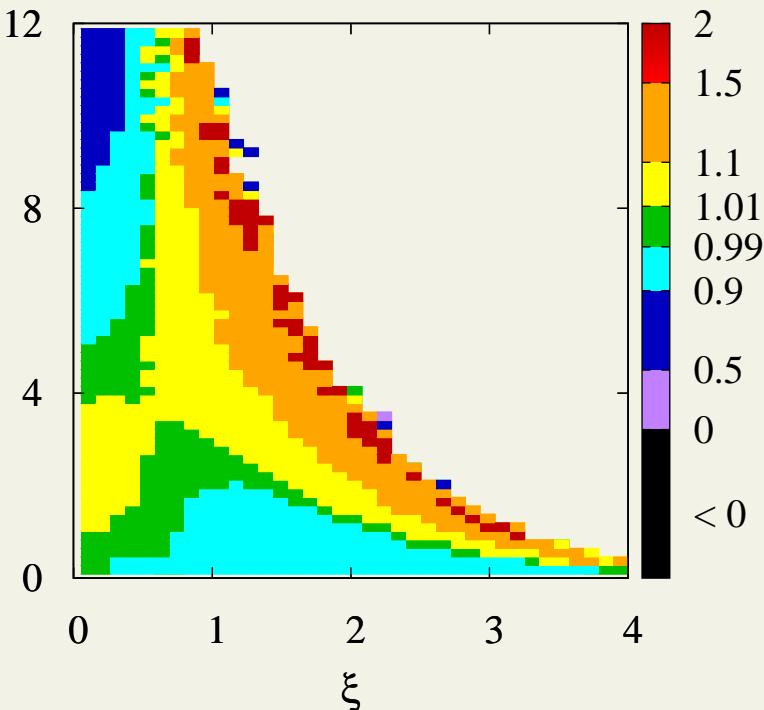
$$K = 6.49 \left(\frac{\tau}{\tau_0} \right)^{2/3}$$

$$\left(\frac{\tau_{REL}}{\tau_{exp}} = 0.12, \right.$$

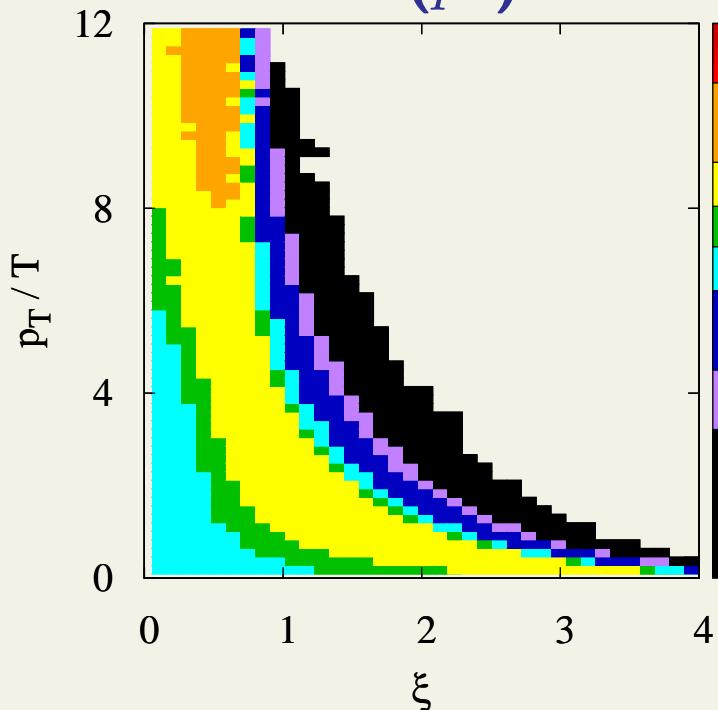
$$\left. \frac{\pi_L}{p} = -0.12 \right)$$

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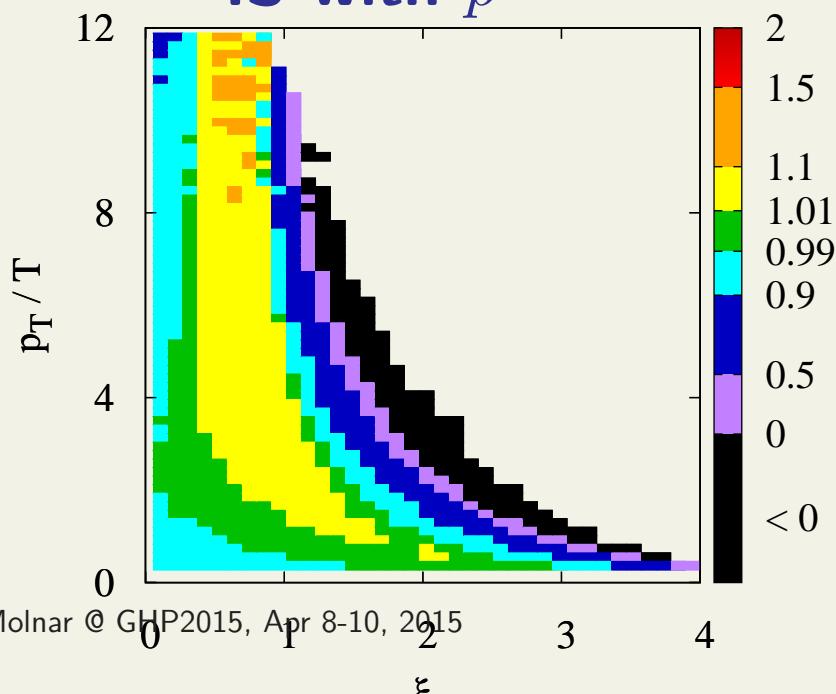
SR ansatz



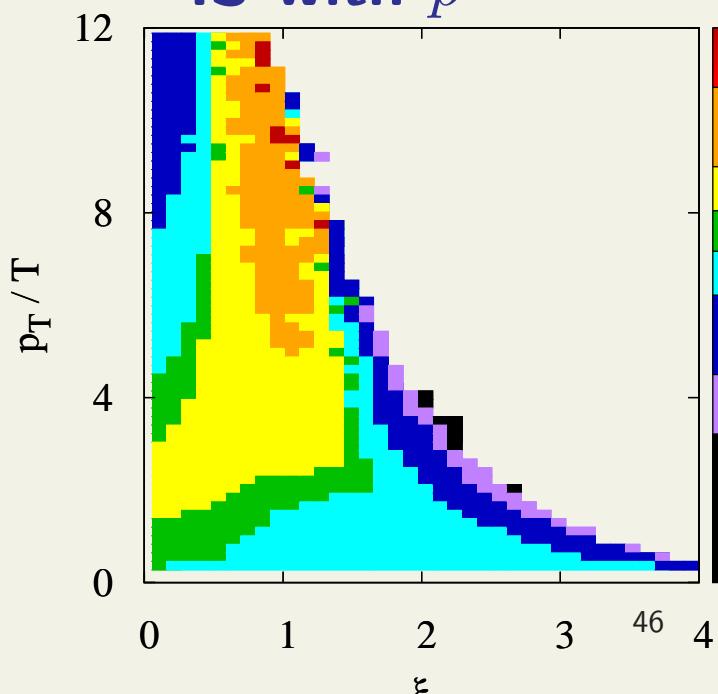
Grad IS (p^2)



IS with $p^{1.5}$



IS with p^1



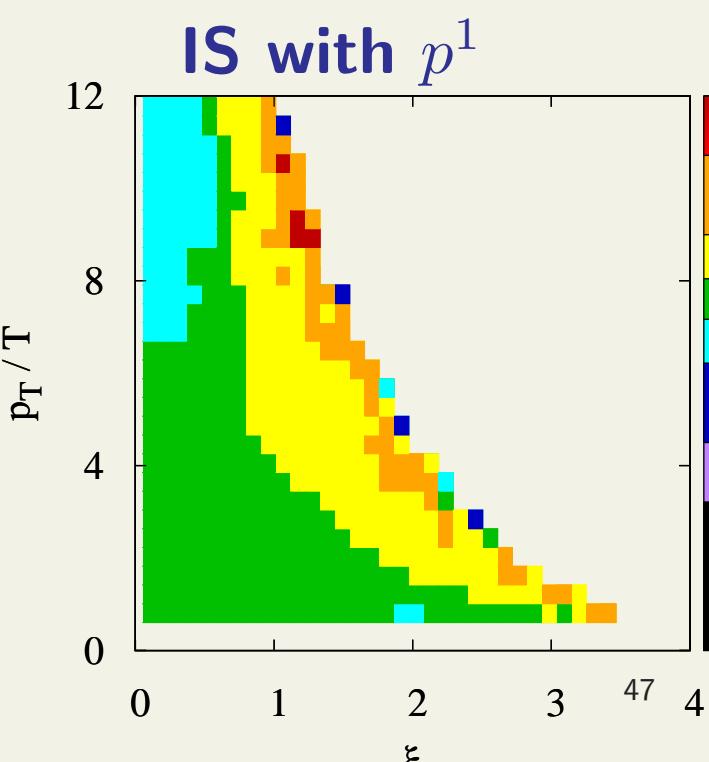
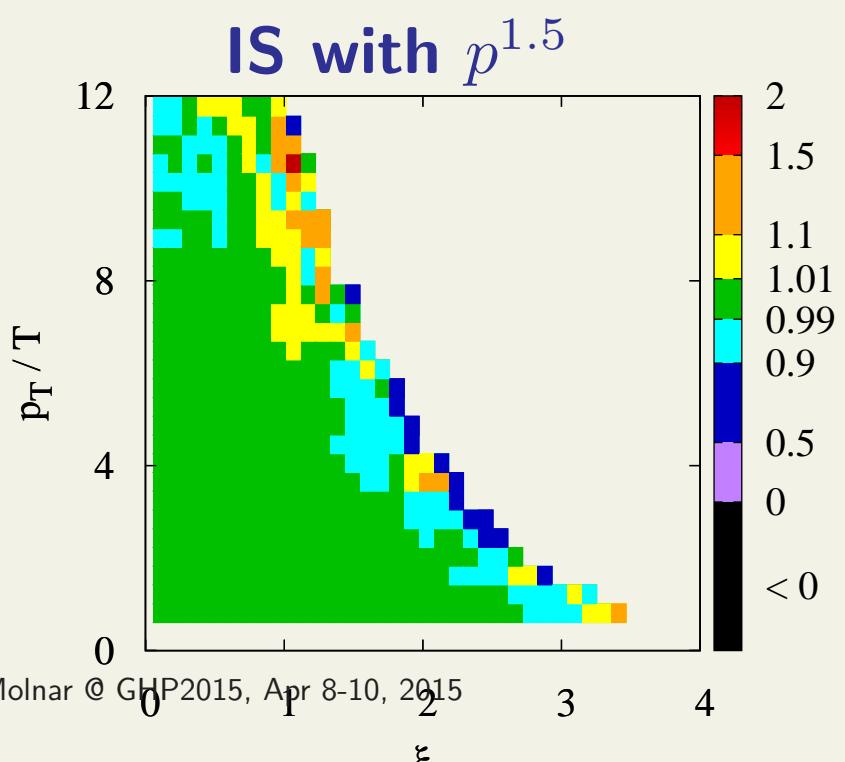
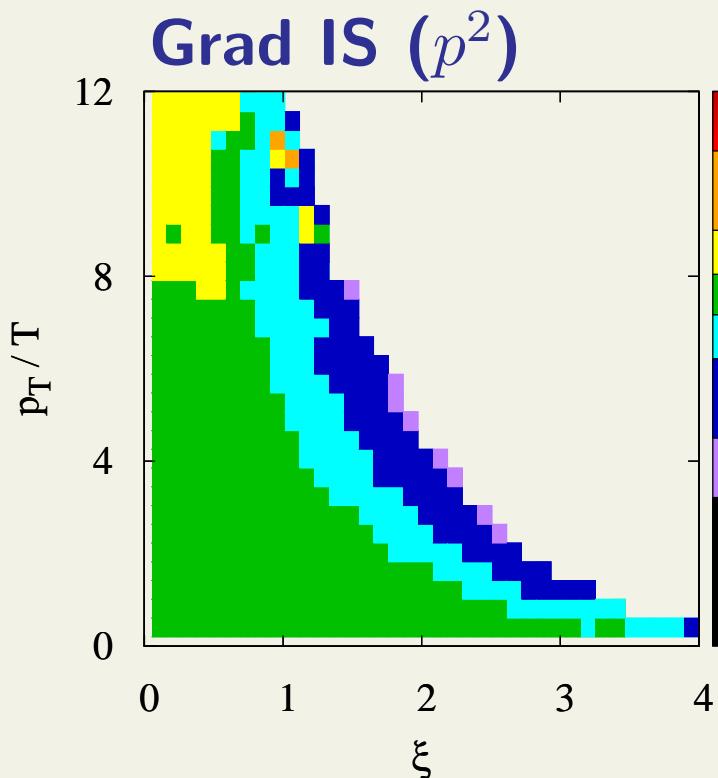
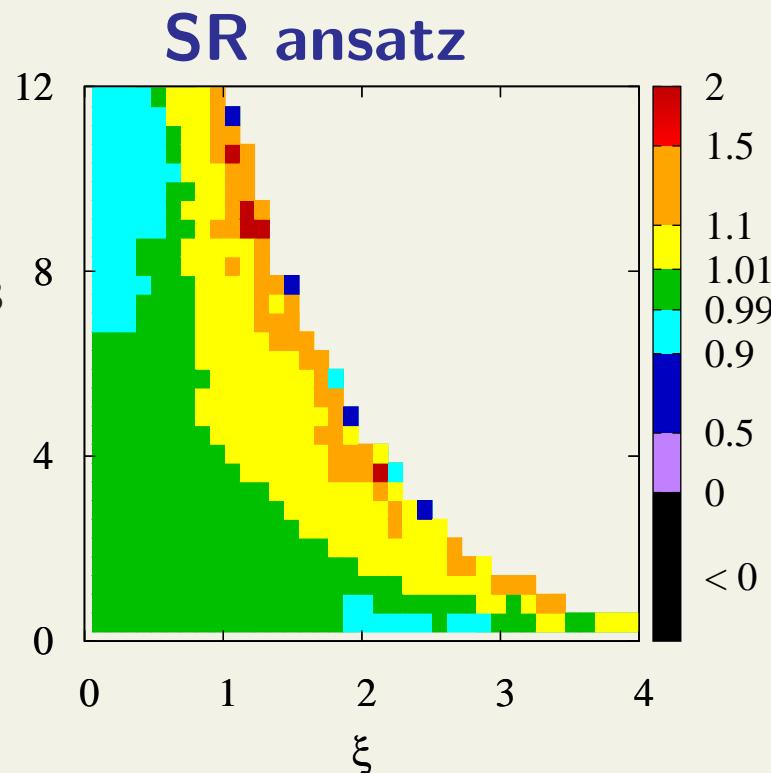
$$\frac{\tau}{\tau_0} = 20$$

$$K = 6.49 \left(\frac{\tau}{\tau_0} \right)^{2/3}$$

$$\left(\frac{\tau_{REL}}{\tau_{exp}} = 0.02, \right.$$

$$\left. \frac{\pi_L}{p} = -0.02 \right)$$

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 -100%
 < 0



\Rightarrow

For high shear viscosity, SR looks more accurate

For small viscosity and late times, IS with $p^{1.5}$ works best

(linear response indeed works when $\tau_{REL} \ll \tau_{exp}$)

SR is generally very similar to IS with linear p^1

Now make 1D projections:

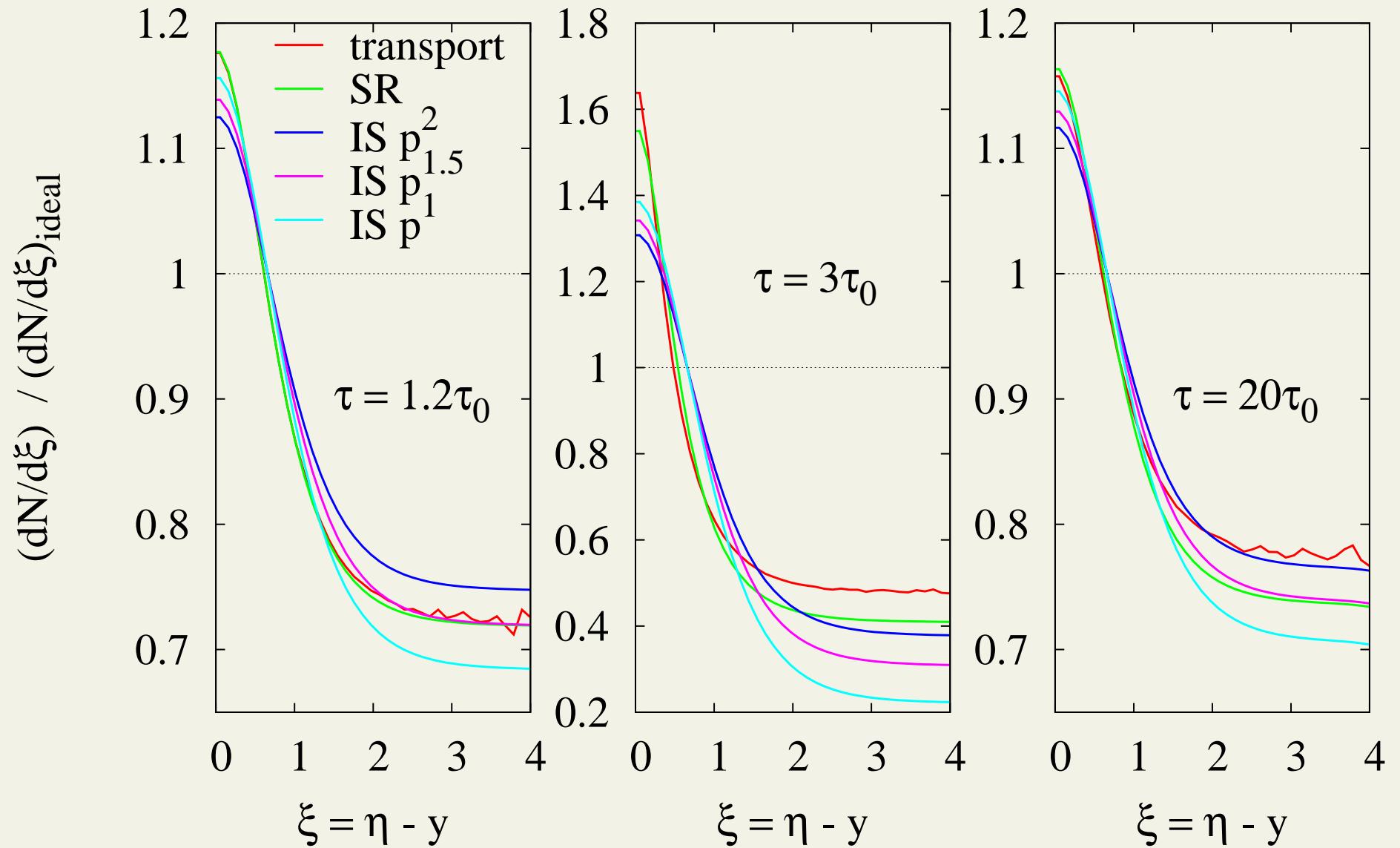
rapidity distribution:
$$\frac{dN}{d\xi}(\tau) = A_T \tau \operatorname{ch}\xi \int d^2 p_T p_T f$$

spectra:
$$\frac{dN}{2\pi p_T dp_T}(\tau) = A_T \tau p_T \int d\xi \operatorname{ch}\xi f$$

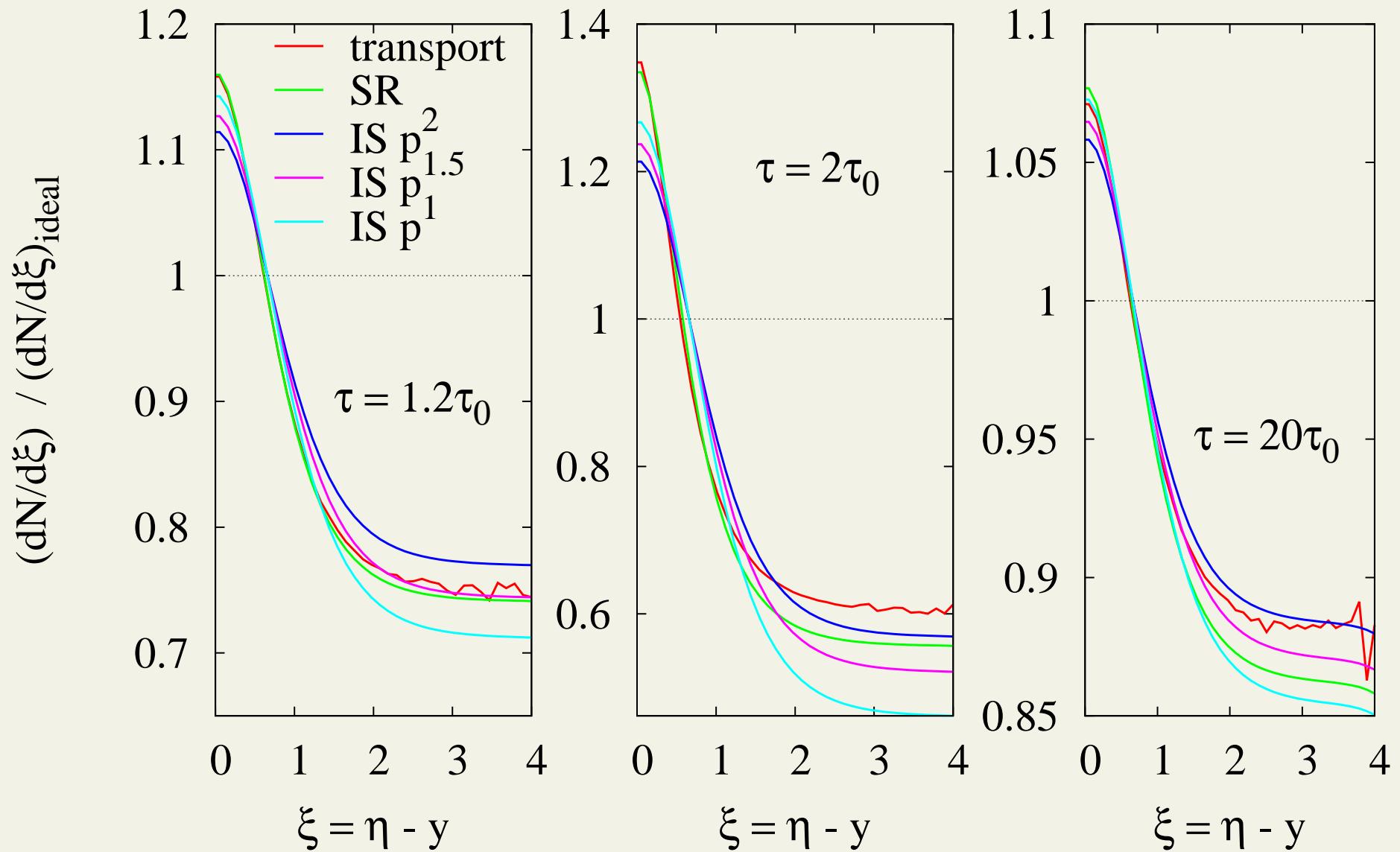
Rapidity distributions

normalize to $\frac{dN}{d\xi}_{thermal} = \frac{1}{2ch^2\xi}$

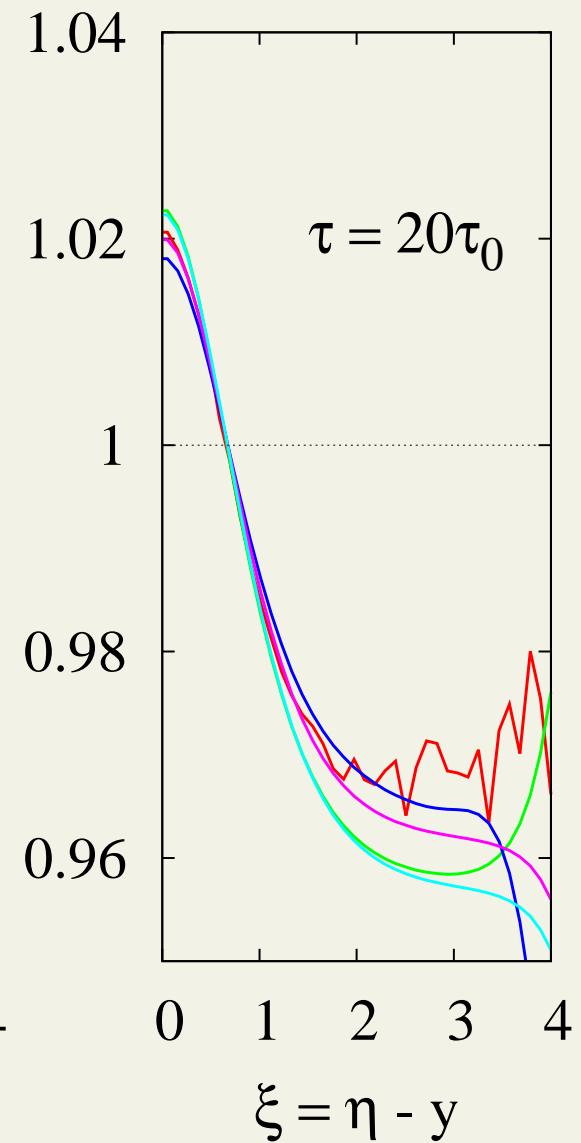
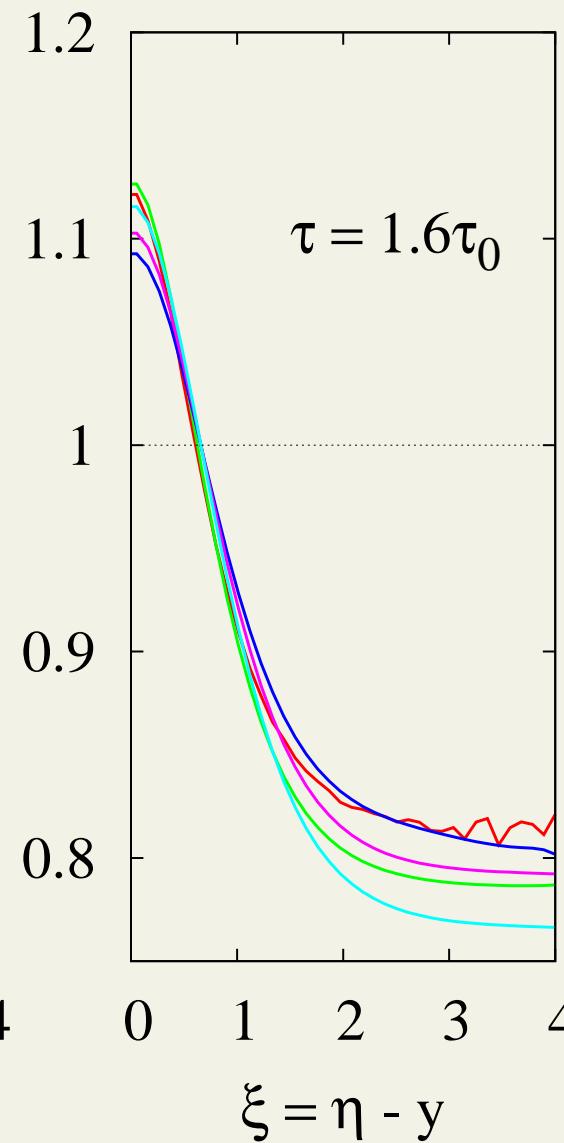
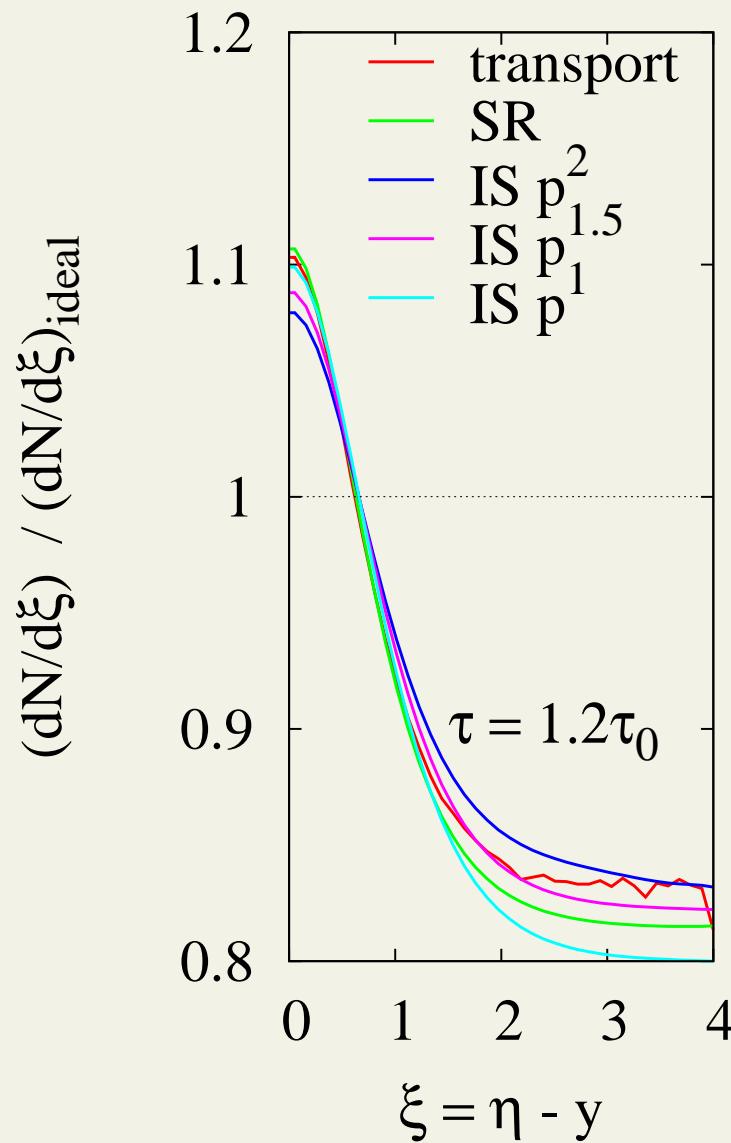
$$K_0 = 1$$



$$K_0 = 2$$



$$K_0 = 6.49$$



\Rightarrow

For low ξ , SR works best.

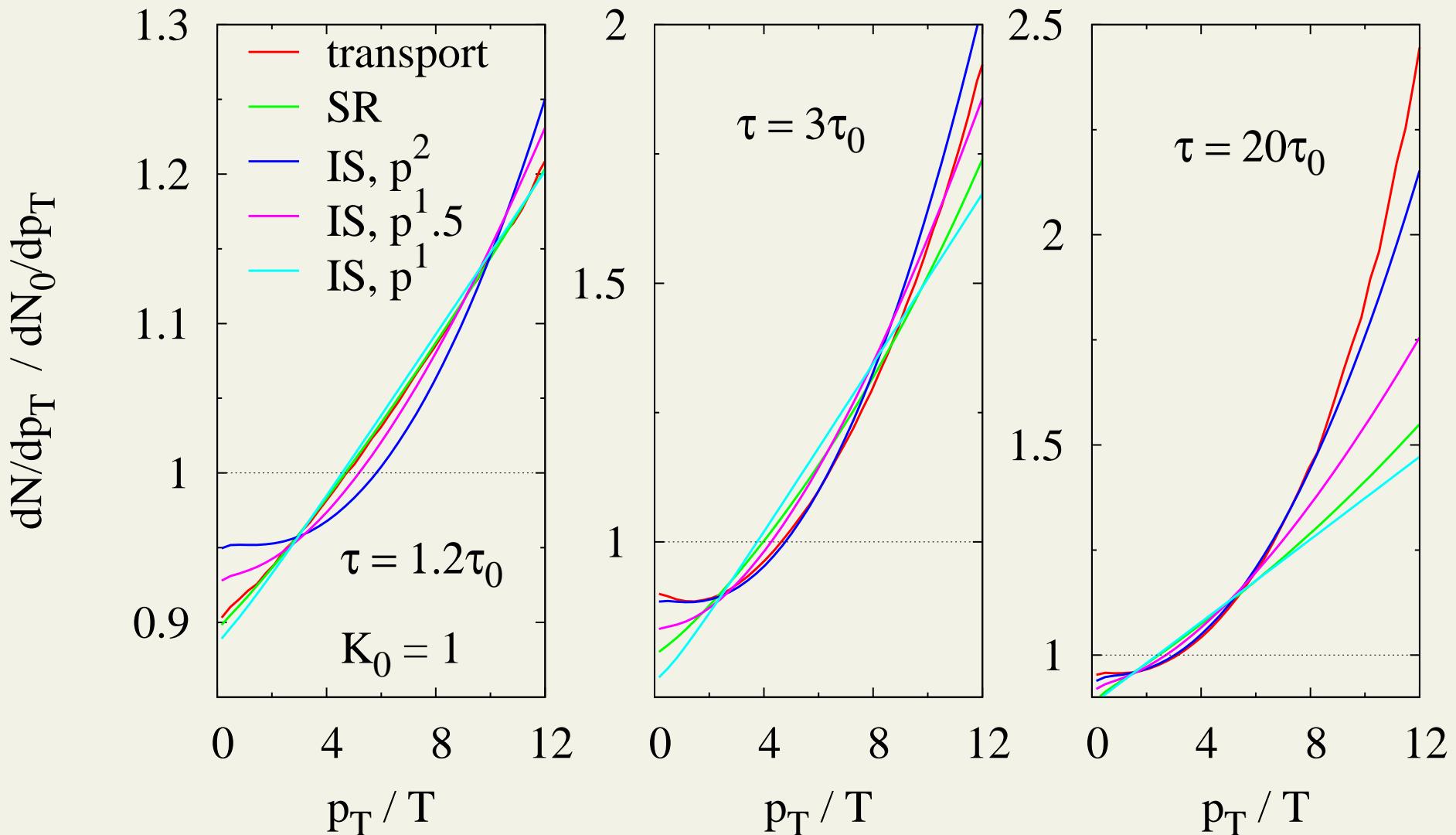
For high ξ :

at early times with higher viscosity, SR is best

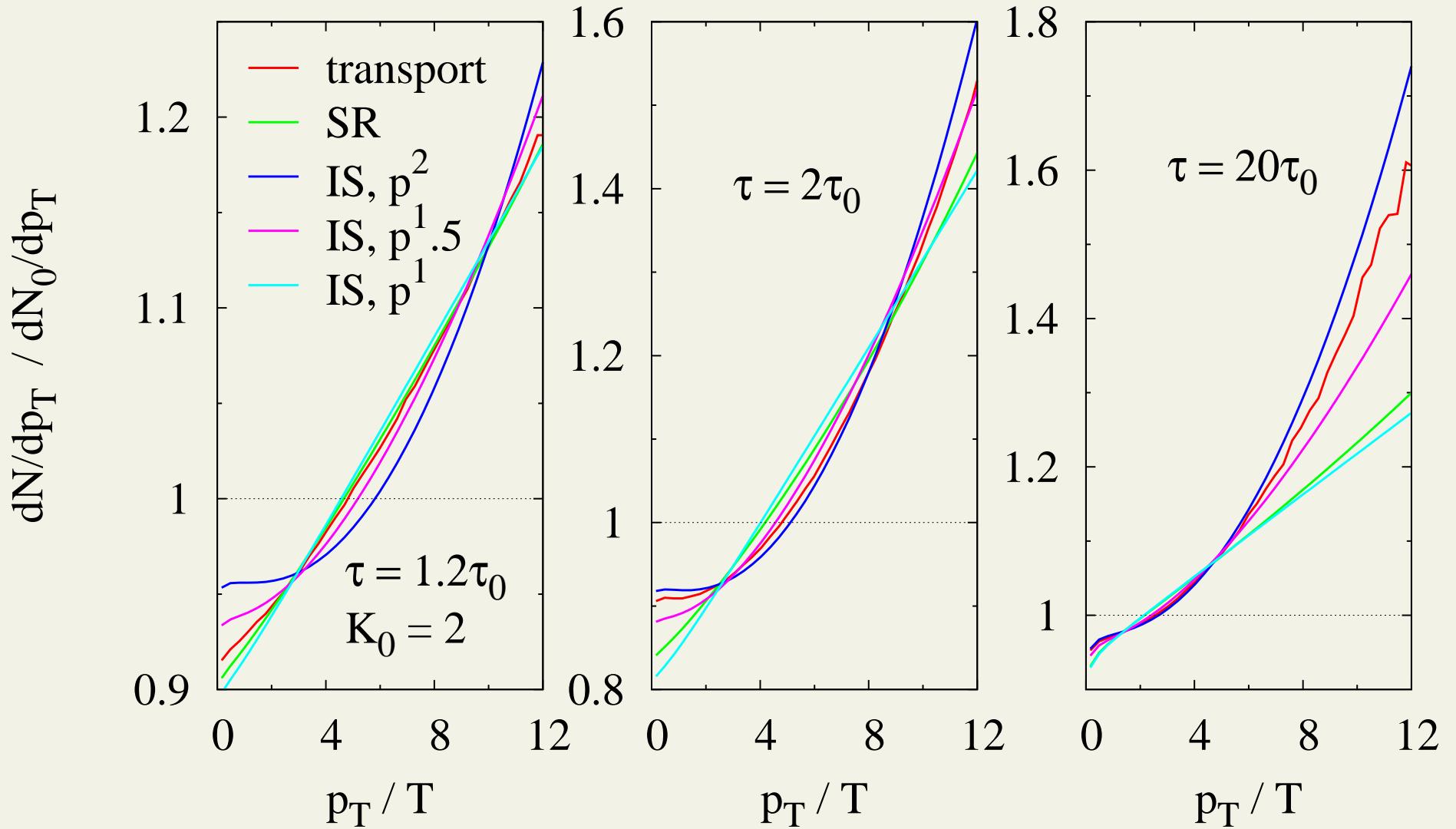
at late times, or with low viscosity, Grad (IS) is best

Now check spectra, normalize to ideal thermal (f_0).

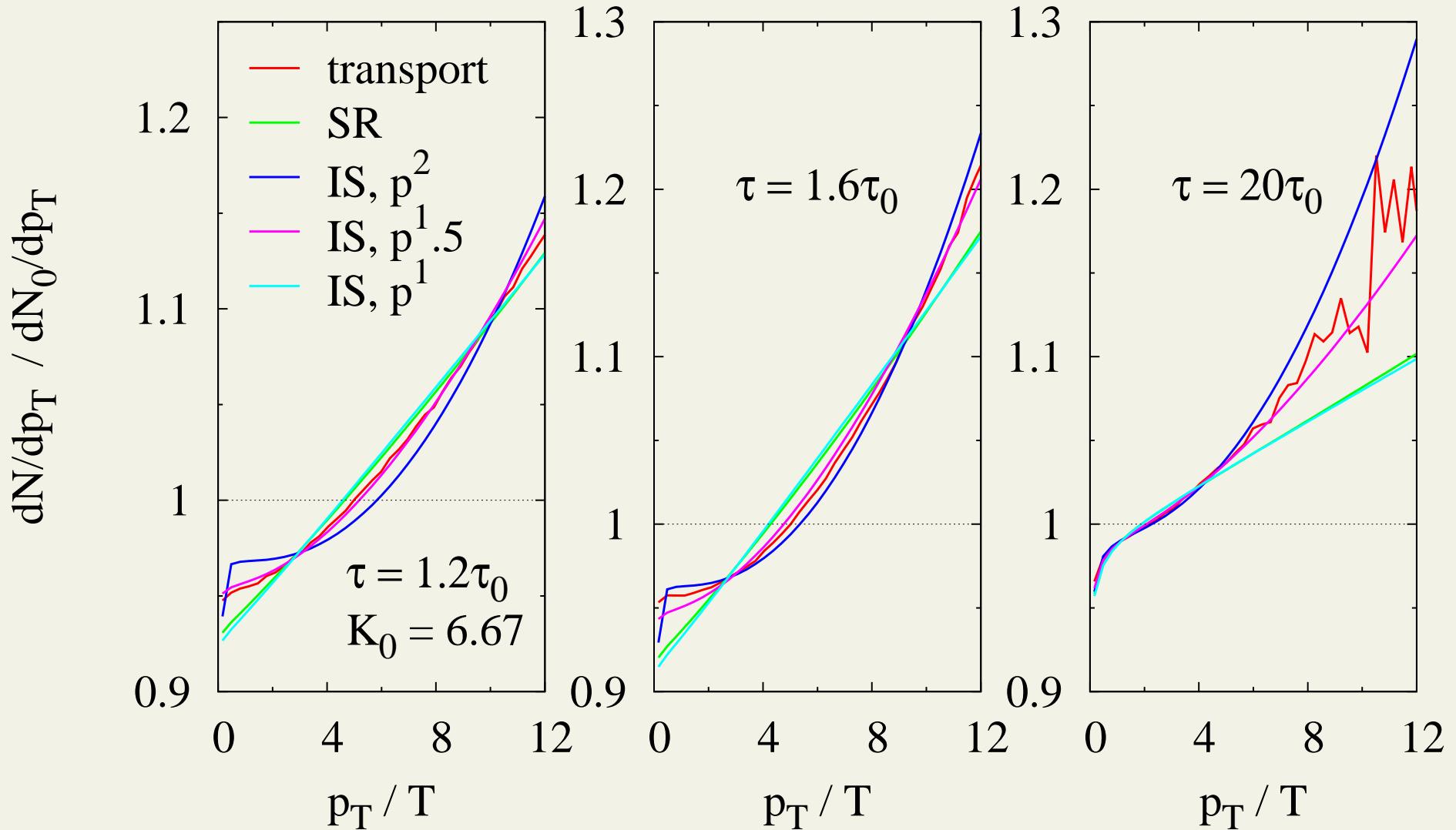
$$K_0 = 1$$



$$K_0 = 2$$



$$K_0 = 6.49$$



\Rightarrow

At early times and for higher viscosity, SR does best.

At late times, for not too low viscosity quadratic(!) does best.

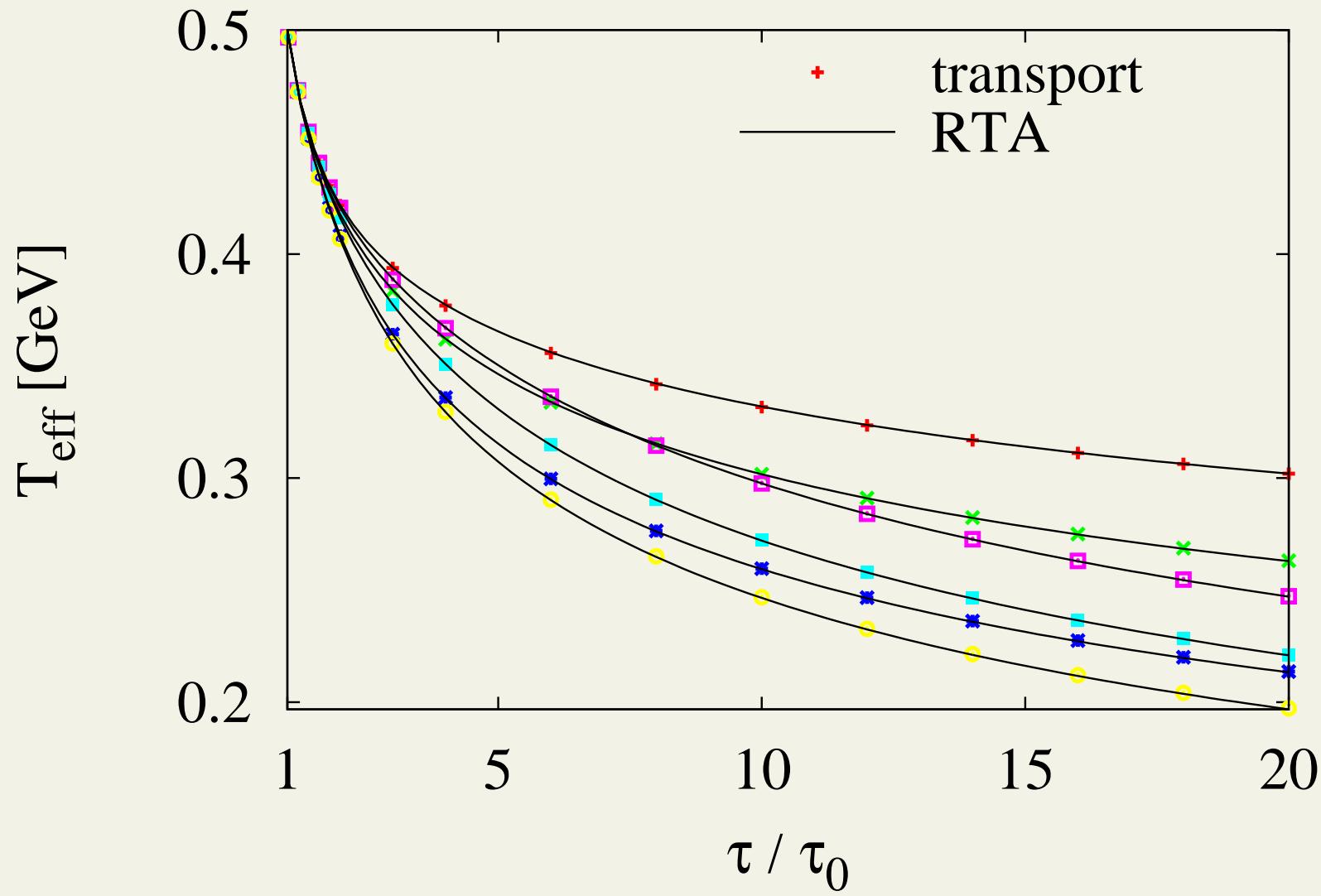
At low viscosity $p^{1.5}$ works best (linear response valid).

Finally, let us look at the RTA more carefully

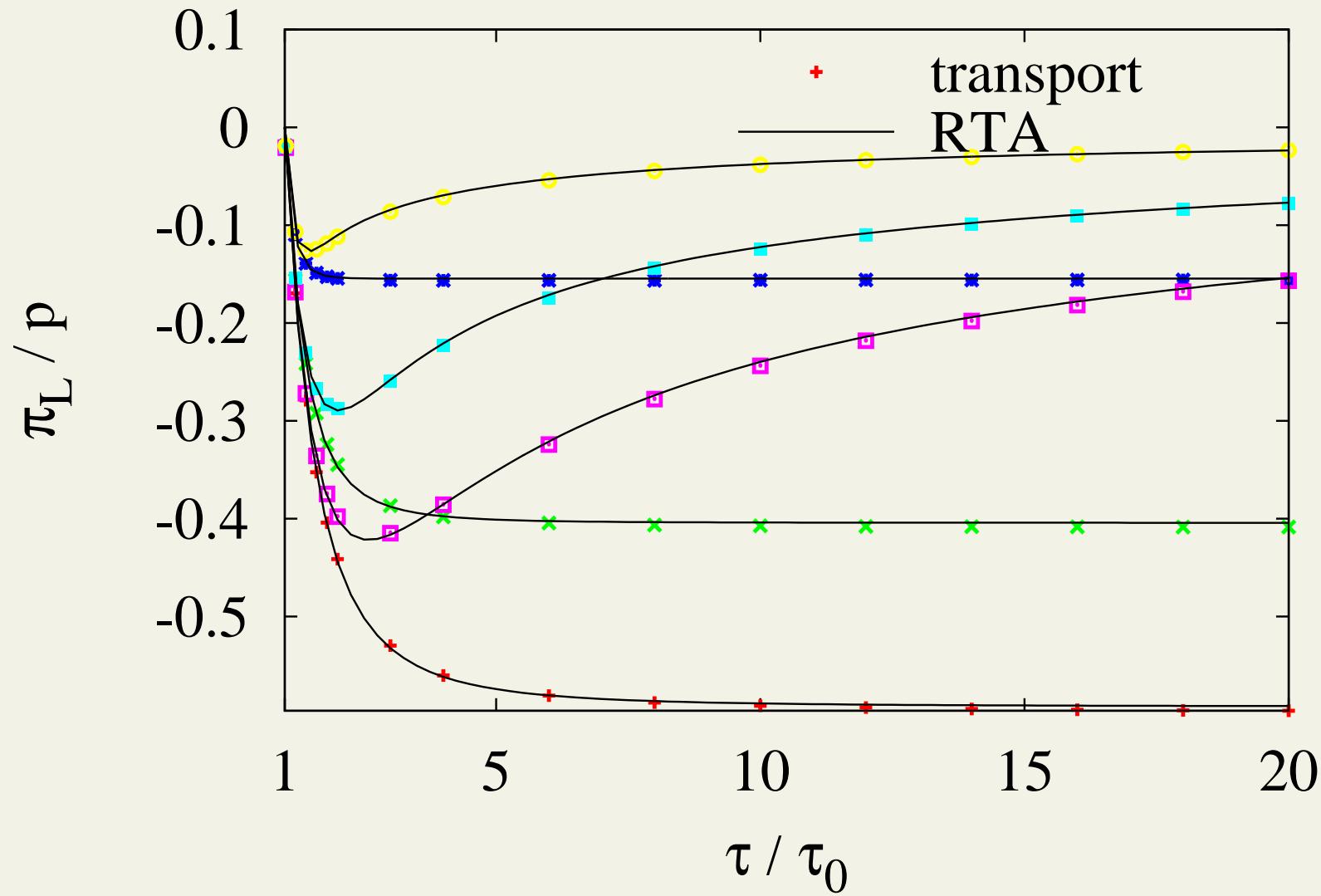
Match to viscosity:

$$\tau_{REL} = \frac{5\eta}{4nT} = 1.05631.. \frac{\tau}{K(\tau)} \quad \sim \quad \tau_{sc}$$

RTA well reproduces cooling - T_{eff} vs τ



and also well reproduces shear stress vs τ



f_{Grad} / f_{RTA}

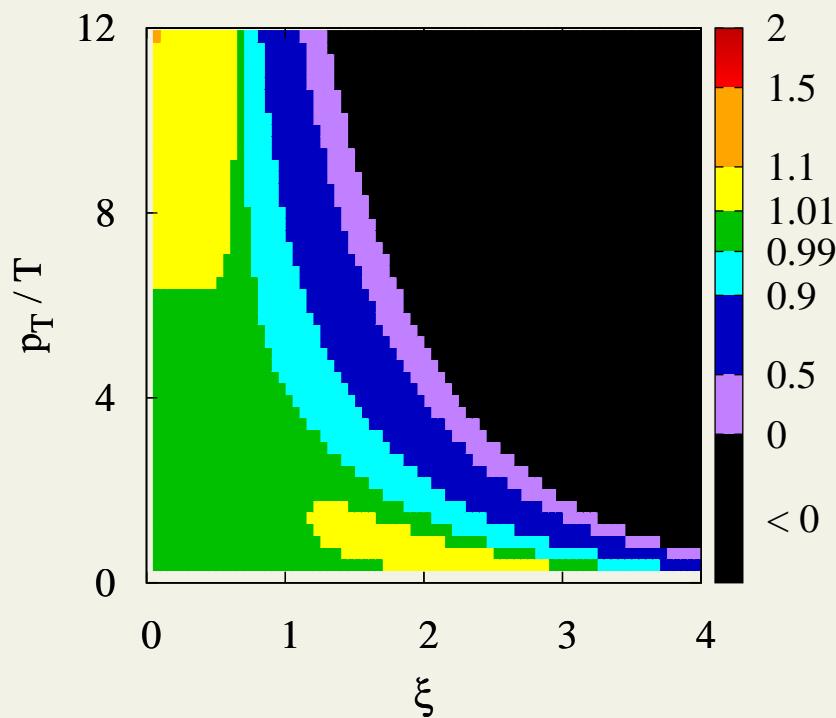
+100%

+50%

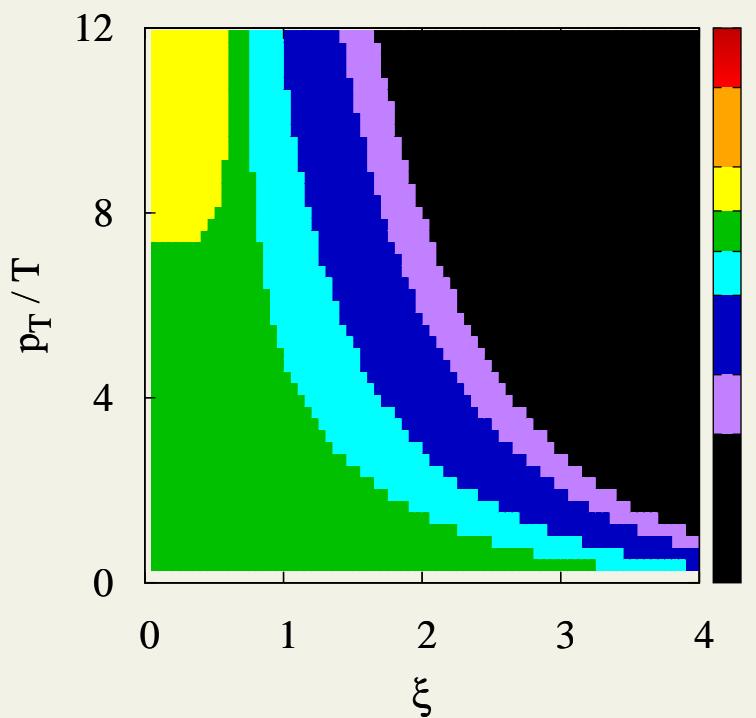
+10%

$\pm 1\%$

-10%



IS with $p^{1.5} / f_{RTA}$

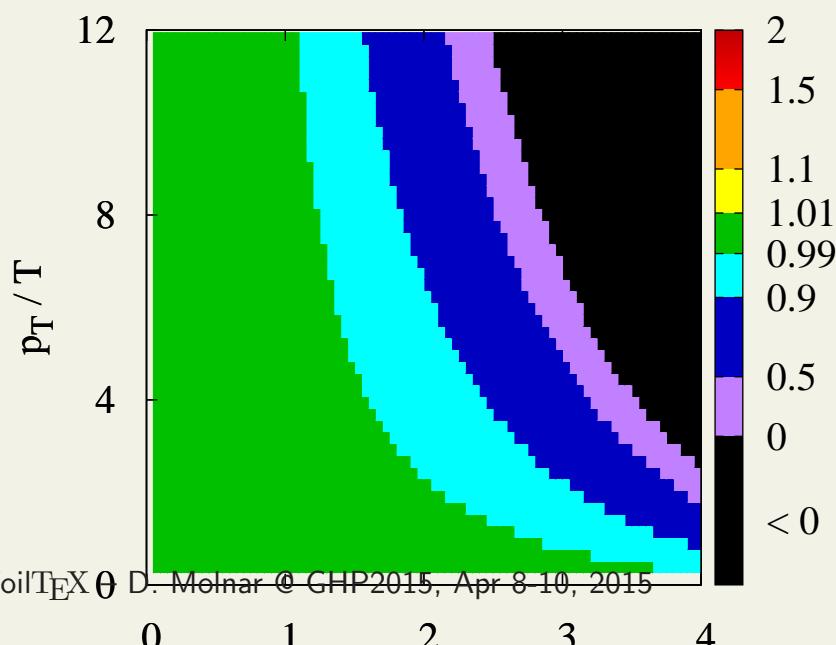


IS with p^1 / f_{RTA}

-50%

-100%

< 0



**despite its linear δf in
linear response regime**
 $(\tau = 20\tau_0, \eta/s \sim 0.03)$

Summary

- If you want particles from dissipative hydro, you must use some model of δf . Several such models have been proposed, and they should be tested, e.g., against full kinetic theory.
- NO FREE LUNCH: we compared Grad ($\sim p^2$), linearized Boltzmann, the Strickland-Romatschke ansatz, and relaxation time equation in the linear response regime in a simple 0+1D Bjorken scenario, and found none of these universally accurate.

We do confirm good applicability of the linearized response approach (which does provide universal answers), but only at late times $\tau/\tau_0 \gtrsim 10$ and for fairly small $\eta/s \lesssim 0.05$.

- At present the choice of δf is a theoretical uncertainty. Perhaps we should look for observables that are less sensitive to it..

Many more comparisons can be done (e.g., 2+1D for elliptic flow, more complex interactions, multicomponent case, ...). Send us your δf 's.

Now... if you only wanted positivity

$$1 + \phi(p) \rightarrow e^{\phi(p)} \rightarrow e^{\tanh \phi(p)} \rightarrow$$

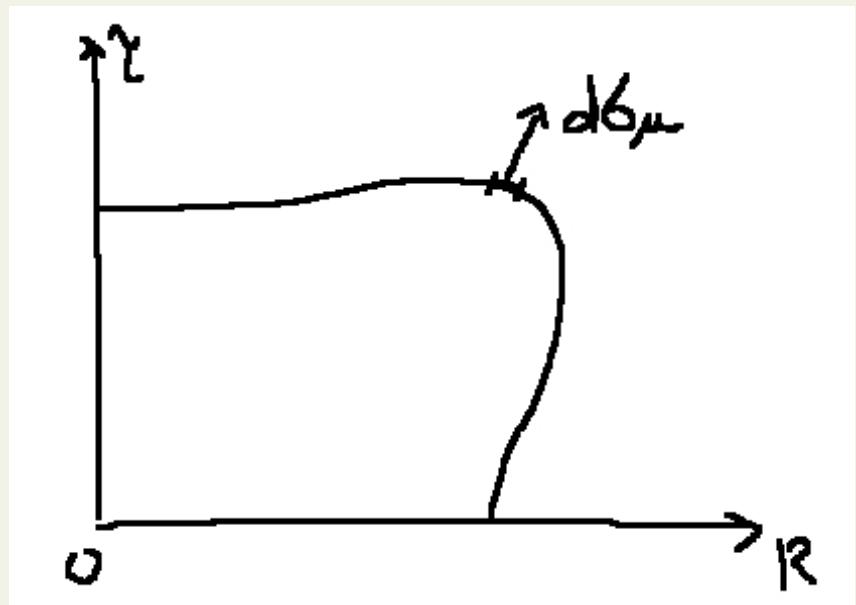
$$\rightarrow e^{\alpha \tanh \frac{\phi(p)}{\alpha}} \rightarrow e^{\alpha(p) \tanh \frac{\phi(p)}{\alpha(p)}} \rightarrow \dots$$

lots of options

Cooper-Frye freezeout

Cooper & Frye, PRD10 ('74)

Assumed sudden transition to a gas on a 3D hypersurface (e.g., $T = \text{const}$)



$$E dN = p^\mu d\sigma_\mu(x) d^3 p f_{\text{gas}}(x, \vec{p})$$

(covariant analog of

$$\frac{dN}{d^3 x d^3 p} = f(\vec{x}, \vec{p}, t_{fo})$$

for a $t = \text{const}$ surface)

conserves energy-momentum and charges locally

BUT: - negative contributions possible $p \cdot d\sigma < 0$
- arbitrariness in choice of HS & self-consistency problem