

Development of a Polarized Positron Source for CEBAF

Beam dynamics: Design and optimization

Sami Habet

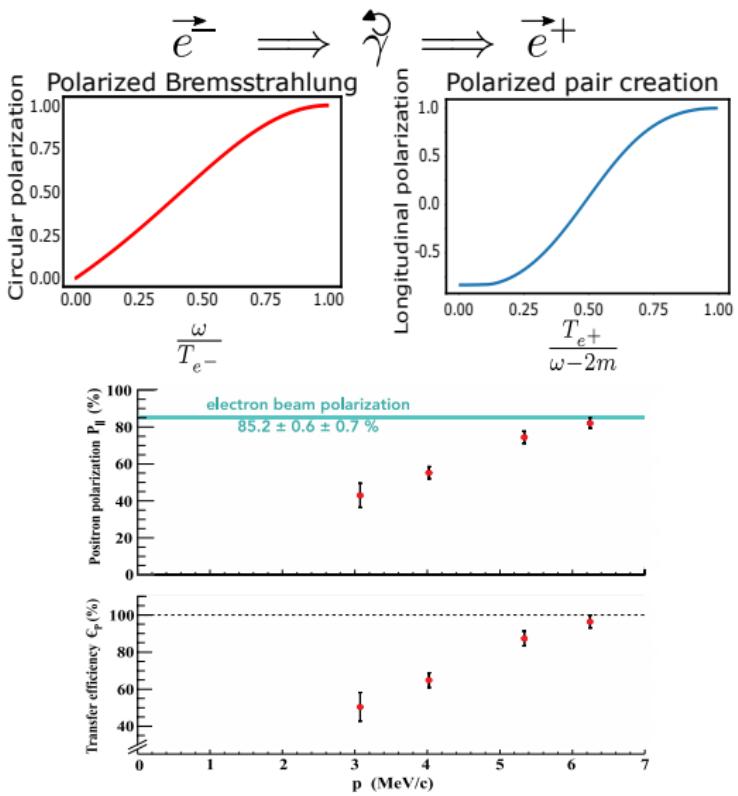
IJCLab & JLab

February 15, 2023



Introduction

J. Grames, E. Voutier et al., JLab Experiment E12-11-105 (2011)



Plan

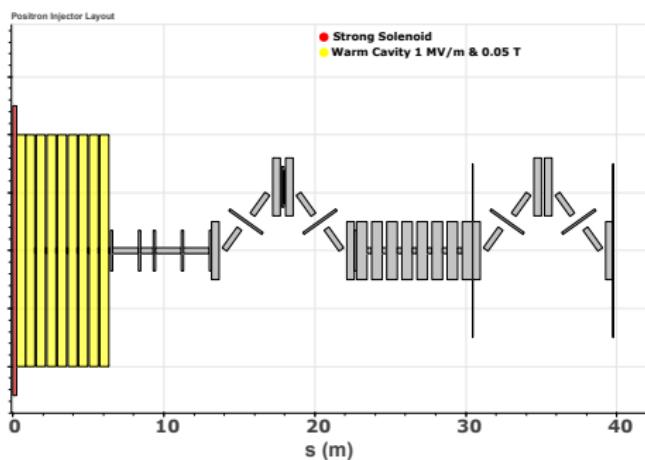
① Target optimization

② Collection system

③ Momentum collimation

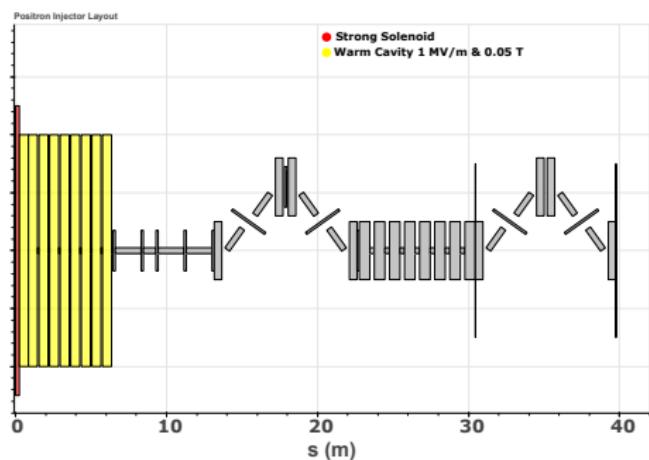
④ Longitudinal optimization

⑤ Conclusion



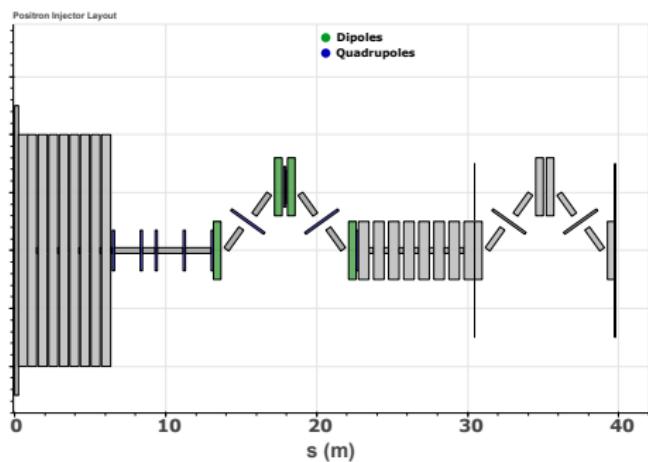
Plan

- ① Target optimization
- ② Collection system
- ③ Momentum collimation
- ④ Longitudinal optimization
- ⑤ Conclusion



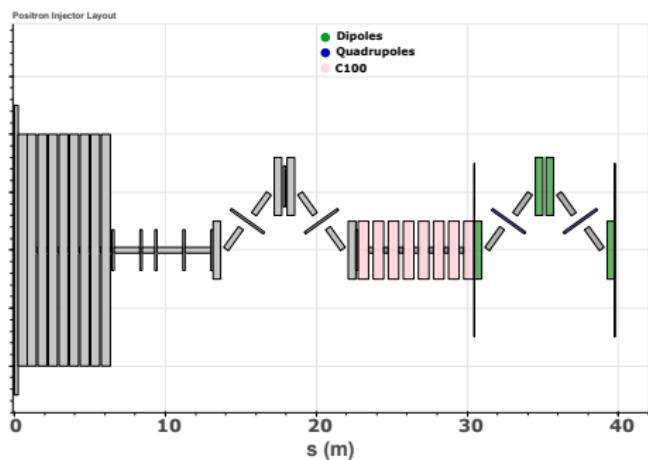
Plan

- ① Target optimization
- ② Collection system
- ③ Momentum collimation
- ④ Longitudinal optimization
- ⑤ Conclusion



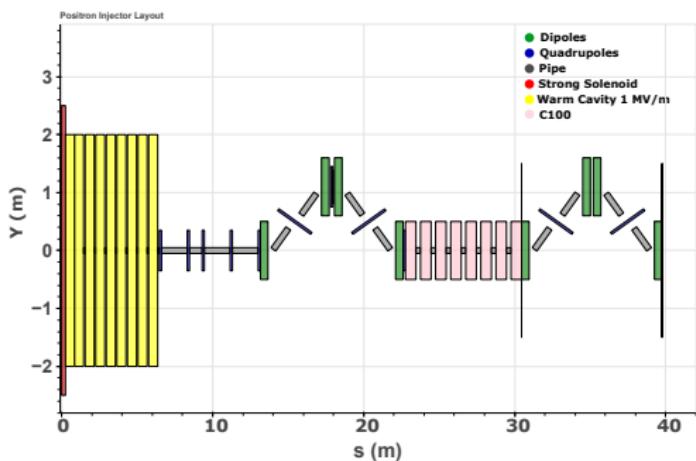
Plan

- ① Target optimization
- ② Collection system
- ③ Momentum collimation
- ④ Longitudinal optimization
- ⑤ Conclusion



Plan

- ① Target optimization
- ② Collection system
- ③ Momentum collimation
- ④ Longitudinal optimization
- ⑤ Conclusion



Outline

- ① Target optimization
- ② Collection system
- ③ Momentum collimation
- ④ Longitudinal optimization
- ⑤ Conclusion
Backup slides

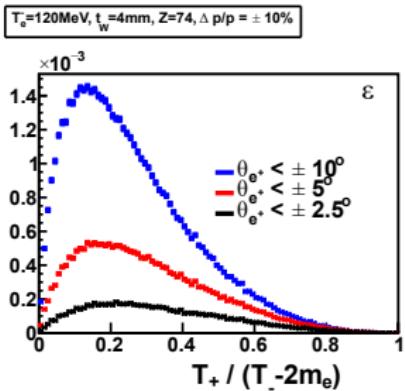
Positron characterization

Unpolarized mode

- Efficiency : $\epsilon = \frac{N_{e^+}}{N_{e^-}}$

Polarized mode

- Figure-of-Merit $FoM = \epsilon P_{e^+}^2$



Positron characterization

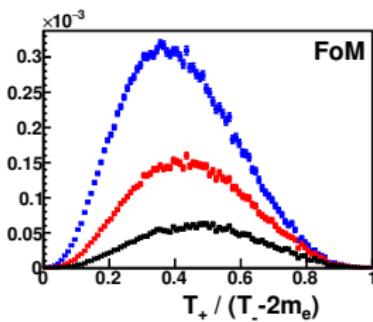
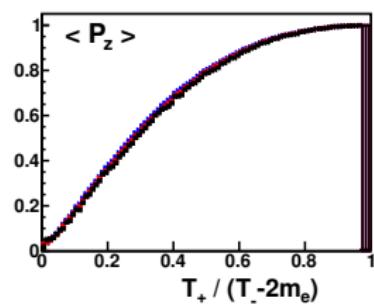
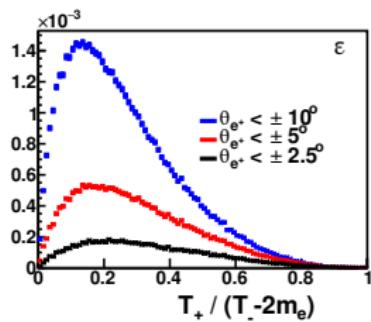
Unpolarized mode

- Efficiency : $\epsilon = \frac{N_{e^+}}{N_{e^-}}$

Polarized mode

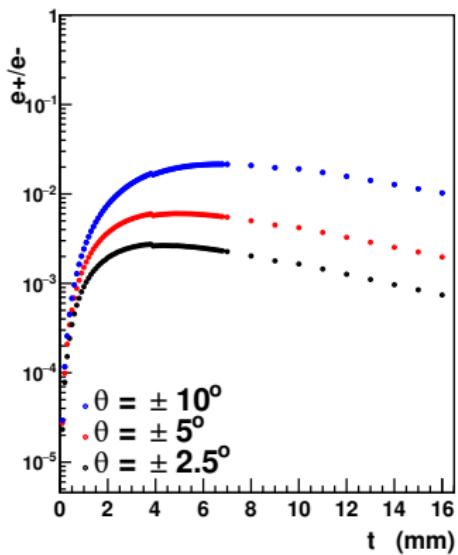
- Figure-of-Merit $FoM = \epsilon P_{e^+}^2$

$T_e=120\text{MeV}$, $t_W=4\text{mm}$, $Z=74$, $\Delta p/p = \pm 10\%$

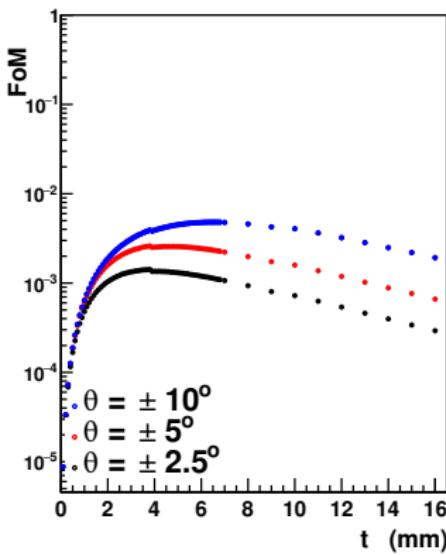


Target thickness optimization

Unpolarized mode

 $T_e = 120\text{ MeV}$, $\Delta P / P = \pm 10\%$, $Z = 74$ 

Polarized mode



Outline

- ① Target optimization
- ② Collection system
- ③ Momentum collimation
- ④ Longitudinal optimization
- ⑤ Conclusion
Backup slides

Quarter Wave Transformer

- Reduce the angular transverse spread

$$x_p = \frac{p_x}{p_z} \text{ and } y_p = \frac{p_y}{p_z}.$$

- Rotate the transverse phase space (x, x_p) and (y, y_p) at the exit of the QWT.
- Use a QWT as an energy filter.
- QWT acceptance :

$$\Delta x_p = \frac{\Delta p_x}{p_z}$$

$$\Delta y_p = \frac{\Delta p_y}{p_z}$$

$$\Delta x = \frac{\Delta p_x}{p_z}$$

$$\Delta y = \frac{\Delta p_y}{p_z}$$

Quarter Wave Transformer

- Reduce the angular transverse spread
 $x_p = \frac{p_x}{p_z}$ and $y_p = \frac{p_y}{p_z}$.
- Rotate the transverse phase space (x, x_p) and (y, y_p) at the exit of the QWT.
- Use a QWT as an energy filter.
- QWT acceptance :

• Radial acceptance

$$\text{QWT} = \frac{\theta}{\theta_0} R$$

• Transverse acceptance

$$\text{QWT} = \frac{\phi}{\phi_0} R$$

$$\text{QWT} = \frac{\psi}{\psi_0} R$$

Quarter Wave Transformer

- Reduce the angular transverse spread
 $x_p = \frac{p_x}{p_z}$ and $y_p = \frac{p_y}{p_z}$.
- Rotate the transverse phase space (x, x_p) and (y, y_p) at the exit of the QWT.
- Use a QWT as an energy filter.
- QWT acceptance :

• Radial acceptance

$$\text{QWT} = \frac{\theta}{\theta_0} R$$

• Transverse acceptance

$$\text{QWT} = \frac{\phi}{\phi_0} R$$

$$\text{QWT} = \frac{\psi}{\psi_0} R$$

Quarter Wave Transformer

- Reduce the angular transverse spread
- Rotate the transverse phase space (x, x_p) and (y, y_p) at the exit of the QWT.
- Use a QWT as an energy filter.
- QWT acceptance :

- Radial acceptance

$$r_0^{QWT} = \frac{B_2}{B_1} R$$

- Transverse acceptance

$$p_t^{QWT} = \frac{eB_1R}{2}$$

Quarter Wave Transformer

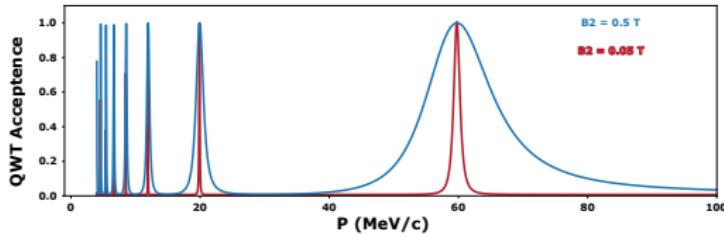
- Reduce the angular transverse spread
 $x_p = \frac{p_x}{p_z}$ and $y_p = \frac{p_y}{p_z}$.
- Rotate the transverse phase space (x, x_p) and (y, y_p) at the exit of the QWT.
- Use a QWT as an energy filter.
- QWT acceptance :

- Radial acceptance

$$r_0^{QWT} = \frac{B_2}{B_1} R$$

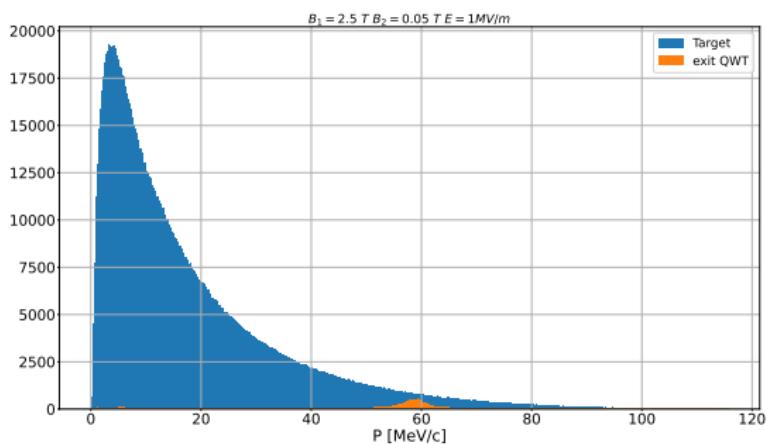
- Transverse acceptance

$$p_t^{QWT} = \frac{eB_1R}{2}$$



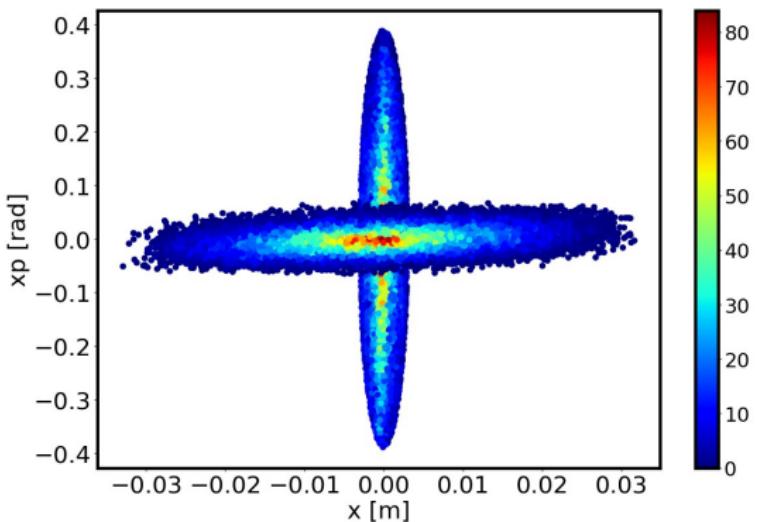
Quarter Wave Transformer

- Reduce the angular transverse spread
 $x_p = \frac{p_x}{p_z}$ and $y_p = \frac{p_y}{p_z}$.
- Rotate the transverse phase space (x, x_p) and (y, y_p) at the exit of the QWT.
- Use a QWT as an energy filter.
- QWT acceptance :
 - Radial acceptance
 $r_0^{QWT} = \frac{B_2}{B_1} R$
 - Transverse acceptance
 $p_t^{QWT} = \frac{eB_1R}{2}$



Quarter Wave Transformer

- Reduce the angular transverse spread
 $x_p = \frac{p_x}{p_z}$ and $y_p = \frac{p_y}{p_z}$.
- Rotate the transverse phase space (x, x_p) and (y, y_p) at the exit of the QWT.
- Use a QWT as an energy filter.
- QWT acceptance :
 - Radial acceptance
 $r_0^{QWT} = \frac{B_2}{B_1} R$
 - Transverse acceptance
 $p_t^{QWT} = \frac{eB_1R}{2}$



Accelerating warm section

Goal

- Reduce the energy spread of the accepted e^+ @ $p = 60 \text{ MeV}/c$
- $f = 1497 \text{ Mhz}$
- $E = 1 \text{ MV}/m$
- $L_{cell} = 0.2 \text{ cm}$
- $r_{cell} = 3 \text{ cm}$

Accelerating warm section

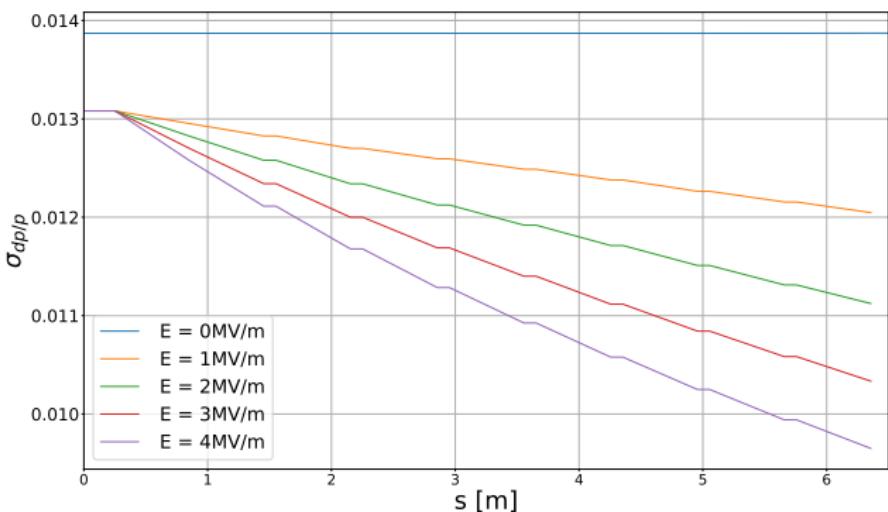
Goal

- Reduce the energy spread of the accepted e^+ @ $p = 60 \text{ MeV}/c$
- $f = 1497 \text{ Mhz}$
- $E = 1 \text{ MV}/m$
- $L_{cell} = 0.2 \text{ cm}$
- $r_{cell} = 3 \text{ cm}$

Accelerating warm section

Goal

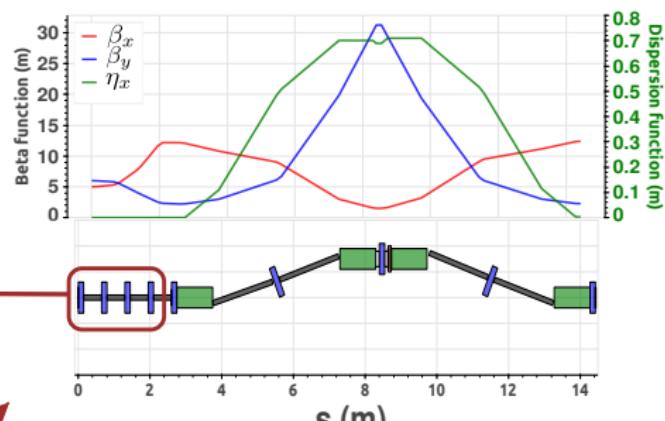
- Reduce the energy spread of the accepted e^+ @ $p = 60 \text{ MeV}/c$
- $f = 1497 \text{ MHz}$
- $E = 1 \text{ MV/m}$
- $L_{cell} = 0.2 \text{ cm}$
- $r_{cell} = 3 \text{ cm}$



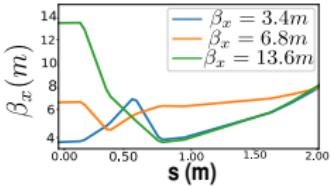
Outline

- ① Target optimization
- ② Collection system
- ③ Momentum collimation
- ④ Longitudinal optimization
- ⑤ Conclusion
Backup slides

Beam size optimization



Matching section



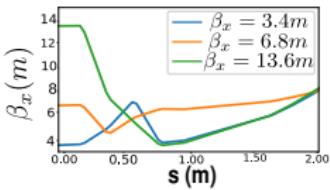
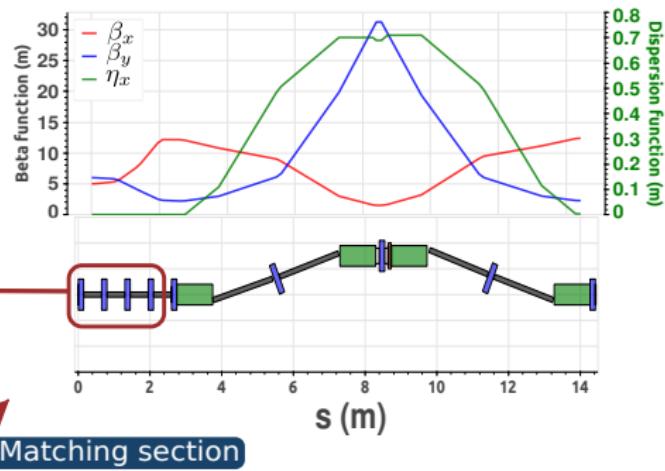
● Periodic Twiss in FODO:

$$\beta_{x,y_{in}} = \beta_{x,y_{out}}$$

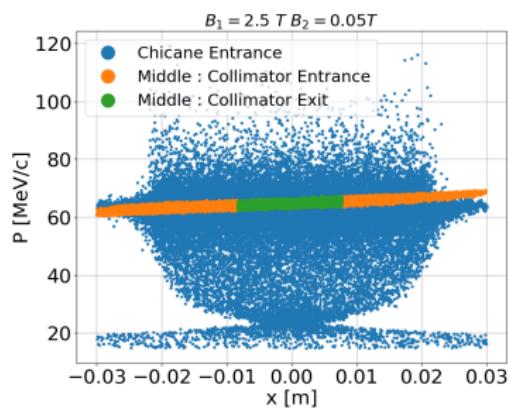
● Minimum beam size condition:

$$\beta_x = \beta_{x,MIN} \longrightarrow \alpha_x = 0$$

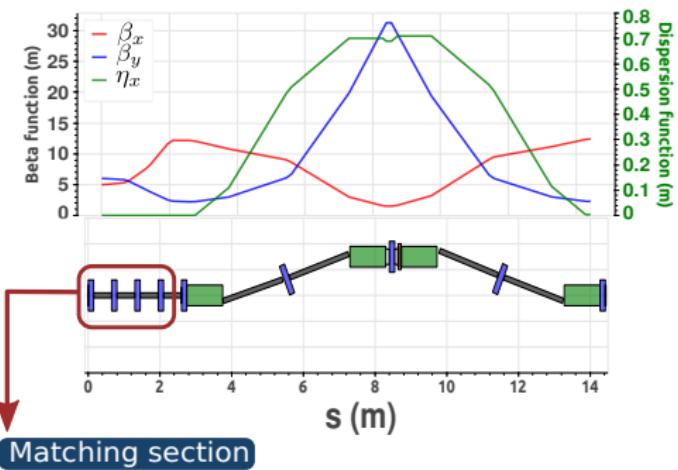
Beam size optimization



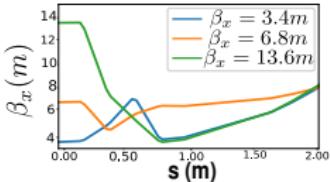
- **Periodic Twiss in FODO:**
 $\beta_{x,y_{in}} = \beta_{x,y_{out}}$
- **Minimum beam size condition:**
 $\beta_x = \beta_{x,MIN} \longrightarrow \alpha_x = 0$



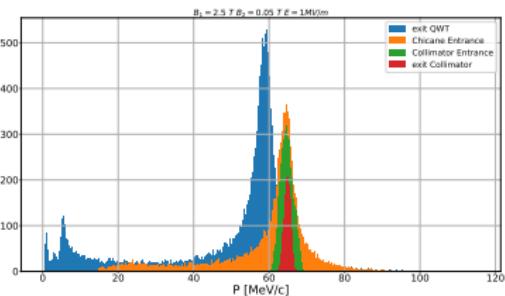
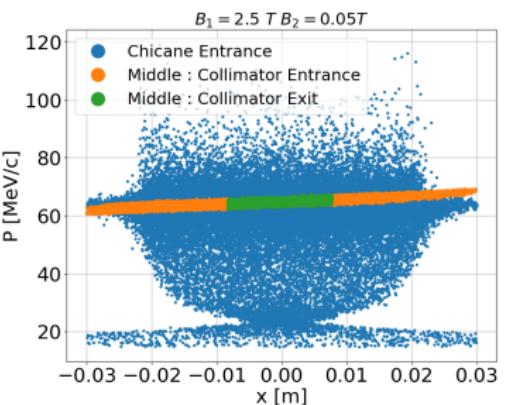
Beam size optimization



Matching section



- **Periodic Twiss in FODO:**
 $\beta_{x,y_{in}} = \beta_{x,y_{out}}$
- **Minimum beam size condition:**
 $\beta_x = \beta_{xMIN} \longrightarrow \alpha_x = 0$



Outline

- ① Target optimization
- ② Collection system
- ③ Momentum collimation
- ④ Longitudinal optimization
- ⑤ Conclusion
Backup slides

Longitudinal optimization: Energy spread and bunch length

- **Compression factor =**

$$\frac{\text{Bunch length}_{\text{Entrance}}}{\text{Bunch length}_{\text{Exit}}}$$

- $C = \frac{1}{1 + [R_{56} \times \kappa]}$
- $\kappa = \frac{d\delta_p}{dz} = \frac{-keV_0}{E_0 + eV_0 \cos \phi} \sin \phi$
- Where:

- R_{56} : Longitudinal chicane element.
- $k = 2\pi \frac{f}{c} [m^{-1}]$
- f is the cavity frequency
- eV_0 Cavity acceleration [MeV]
- E_0 Central energy [MeV]
- ϕ Cavity phase advance.

Longitudinal optimization: Energy spread and bunch length

- **Compression factor =**

$$\frac{\text{Bunch length}_{\text{Entrance}}}{\text{Bunch length}_{\text{Exit}}}$$

- $C = \frac{1}{1 + [R_{56} \times \kappa]}$
- $\kappa = \frac{d\delta_p}{dz} = \frac{-keV_0}{E_0 + eV_0 \cos \phi} \sin \phi$
- Where:
 - R_{56} : Longitudinal chicane element.
 - $k = 2\pi \frac{f}{c} [m^{-1}]$
 - f is the cavity frequency
 - eV_0 Cavity acceleration [MeV]
 - E_0 Central energy [MeV]
 - ϕ Cavity phase advance.

Longitudinal optimization: Energy spread and bunch length

- **Compression factor =**

$$\frac{\text{Bunch length}_{\text{Entrance}}}{\text{Bunch length}_{\text{Exit}}}$$

- $C = \frac{1}{1 + [R_{56} \times \kappa]}$

- $\kappa = \frac{d\delta_p}{dz} = \frac{-keV_0}{E_0 + eV_0 \cos \phi} \sin \phi$

- Where:

- R_{56} : Longitudinal chicane element.
- $k = 2\pi \frac{f}{c} [m^{-1}]$
- f is the cavity frequency
- eV_0 Cavity acceleration [MeV]
- E_0 Central energy [MeV]
- ϕ Cavity phase advance.

Longitudinal optimization: Energy spread and bunch length

- **Compression factor =**

$$\frac{\text{Bunch length}_{\text{Entrance}}}{\text{Bunch length}_{\text{Exit}}}$$

- $C = \frac{1}{1 + [R_{56} \times \kappa]}$
- $\kappa = \frac{d\delta_p}{dz} = \frac{-keV_0}{E_0 + eV_0 \cos \phi} \sin \phi$
- Where:

- R_{56} : Longitudinal chicane element.
- $k = 2\pi \frac{f}{c} [m^{-1}]$
- f is the cavity frequency
- eV_0 Cavity acceleration [MeV]
- E_0 Central energy [MeV]
- ϕ Cavity phase advance.

Longitudinal optimization: Energy spread and bunch length

- **Compression factor =**

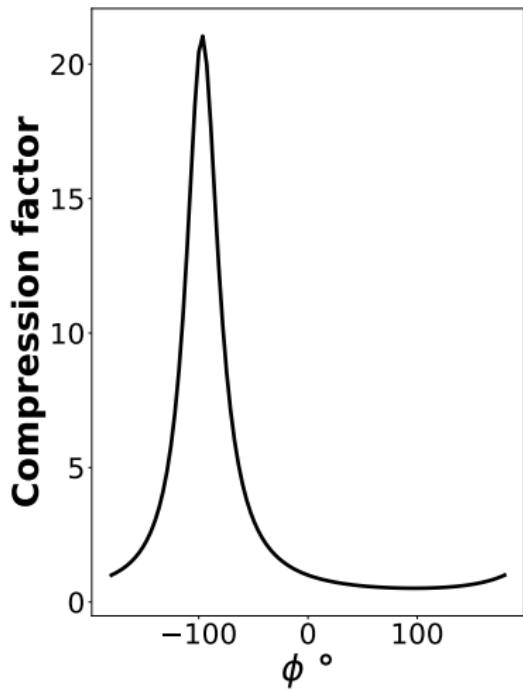
$$\frac{\text{Bunch length}_{\text{Entrance}}}{\text{Bunch length}_{\text{Exit}}}$$

$$\bullet C = \frac{1}{1 + [R_{56} \times \kappa]}$$

$$\bullet \kappa = \frac{d\delta_p}{dz} = \frac{-keV_0}{E_0 + eV_0 \cos \phi} \sin \phi$$

- Where:

- R_{56} : Longitudinal chicane element.
- $k = 2\pi \frac{f}{c} [m^{-1}]$
- f is the cavity frequency
- eV_0 Cavity acceleration [MeV]
- E_0 Central energy [MeV]
- ϕ Cavity phase advance.



Longitudinal optimization: Energy spread and bunch length

- **Compression factor =**

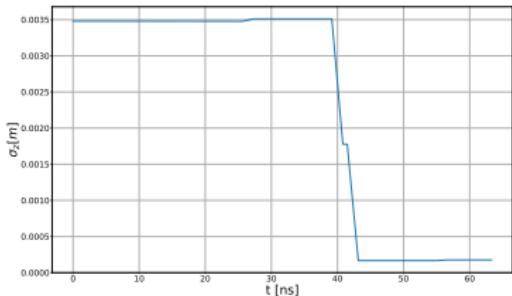
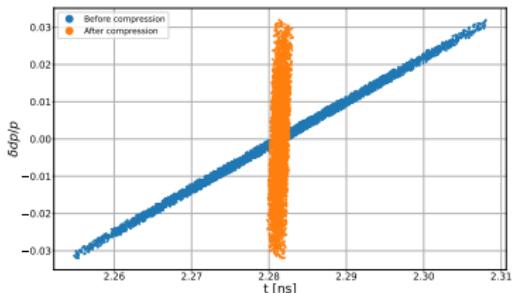
$$\frac{\text{Bunch length}_{\text{Entrance}}}{\text{Bunch length}_{\text{Exit}}}$$

$$\bullet C = \frac{1}{1 + [R_{56} \times \kappa]}$$

$$\bullet \kappa = \frac{d\delta_p}{dz} = \frac{-keV_0}{E_0 + eV_0 \cos \phi} \sin \phi$$

- Where:

- R_{56} : Longitudinal chicane element.
- $k = 2\pi \frac{f}{c} [m^{-1}]$
- f is the cavity frequency
- eV_0 Cavity acceleration [MeV]
- E_0 Central energy [MeV]
- ϕ Cavity phase advance.



Longitudinal optimization: Energy spread and bunch length

- **Compression factor =**

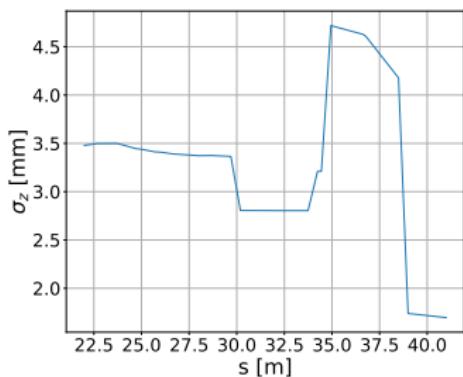
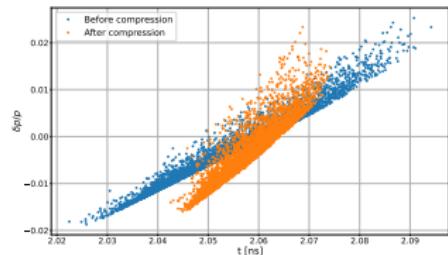
$$\frac{\text{Bunch length}_{\text{Entrance}}}{\text{Bunch length}_{\text{Exit}}}$$

- $C = \frac{1}{1 + [R_{56} \times \kappa]}$

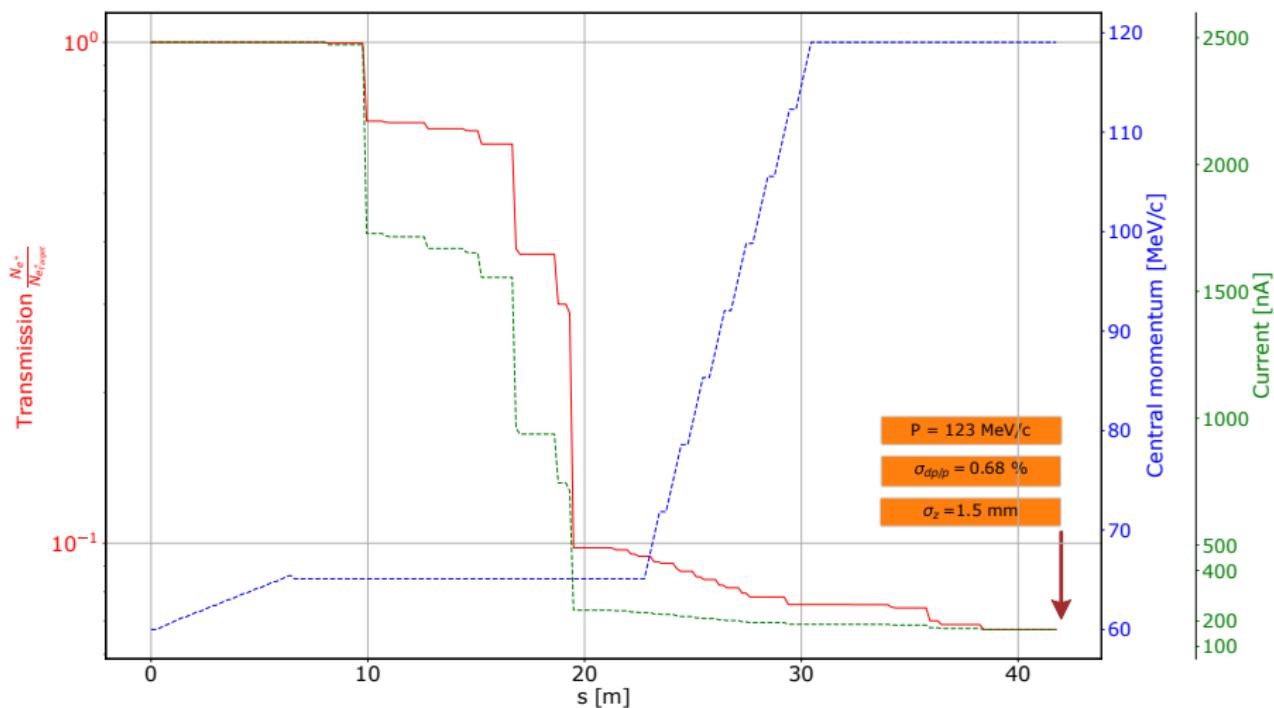
- $\kappa = \frac{d\delta_p}{dz} = \frac{-keV_0}{E_0 + eV_0 \cos \phi} \sin \phi$

- Where:

- R_{56} : Longitudinal chicane element.
- $k = 2\pi \frac{f}{c} [m^{-1}]$
- f is the cavity frequency
- eV_0 Cavity acceleration [MeV]
- E_0 Central energy [MeV]
- ϕ Cavity phase advance.



Transmission and Current



Summary

Params	e^+ injection	CEBAF Acceptance
$\sigma_{dp/p}$ [%]	0.68	$\pm 1\%$
σ_z [ps]	5	≤ 4
σ_x [mm]	8	≤ 3
$N \epsilon_n$ [mm mrad]	14	≤ 40
Mean Momentum [MeV/c]	123	123
e^+ current	170 nA	100 nA

Outline

- ① Target optimization
 - ② Collection system
 - ③ Momentum collimation
 - ④ Longitudinal optimization
 - ⑤ Conclusion

Conclusion

- The performance of the positron system is heavily influenced by the central momentum. For a high yield of positrons, the central momentum should be set to 15 MeV/c, while a high polarization requires a central momentum of 60 MeV/c.
- The QWT helps the selection of the desired momentum and reduces the spread of transverse angles.
- The accelerating section exerts significant influence on the longitudinal plane, thereby reducing the energy spread to meet the CEBAF requirement of $\sigma_{dp/p} = \pm 1\%$.
- For improved compression, the energy spread at the exit of the C100 must be at least five times smaller.
- Expecting higher current for the unpolarized mode P=15 MeV/c.

Conclusion

- The performance of the positron system is heavily influenced by the central momentum. For a high yield of positrons, the central momentum should be set to 15 MeV/c, while a high polarization requires a central momentum of 60 MeV/c.
- The QWT helps the selection of the desired momentum and reduces the spread of transverse angles.
- The accelerating section exerts significant influence on the longitudinal plane, thereby reducing the energy spread to meet the CEBAF requirement of $\sigma_{dp/p} = \pm 1\%$.
- For improved compression, the energy spread at the exit of the C100 must be at least five times smaller.
- Expecting higher current for the unpolarized mode P=15 MeV/c.

Conclusion

- The performance of the positron system is heavily influenced by the central momentum. For a high yield of positrons, the central momentum should be set to 15 MeV/c, while a high polarization requires a central momentum of 60 MeV/c.
- The QWT helps the selection of the desired momentum and reduces the spread of transverse angles.
- The accelerating section exerts significant influence on the longitudinal plane, thereby reducing the energy spread to meet the CEBAF requirement of $\sigma_{dp/p} = \pm 1\%$.
- For improved compression, the energy spread at the exit of the C100 must be at least five times smaller.
- Expecting higher current for the unpolarized mode P=15 MeV/c.

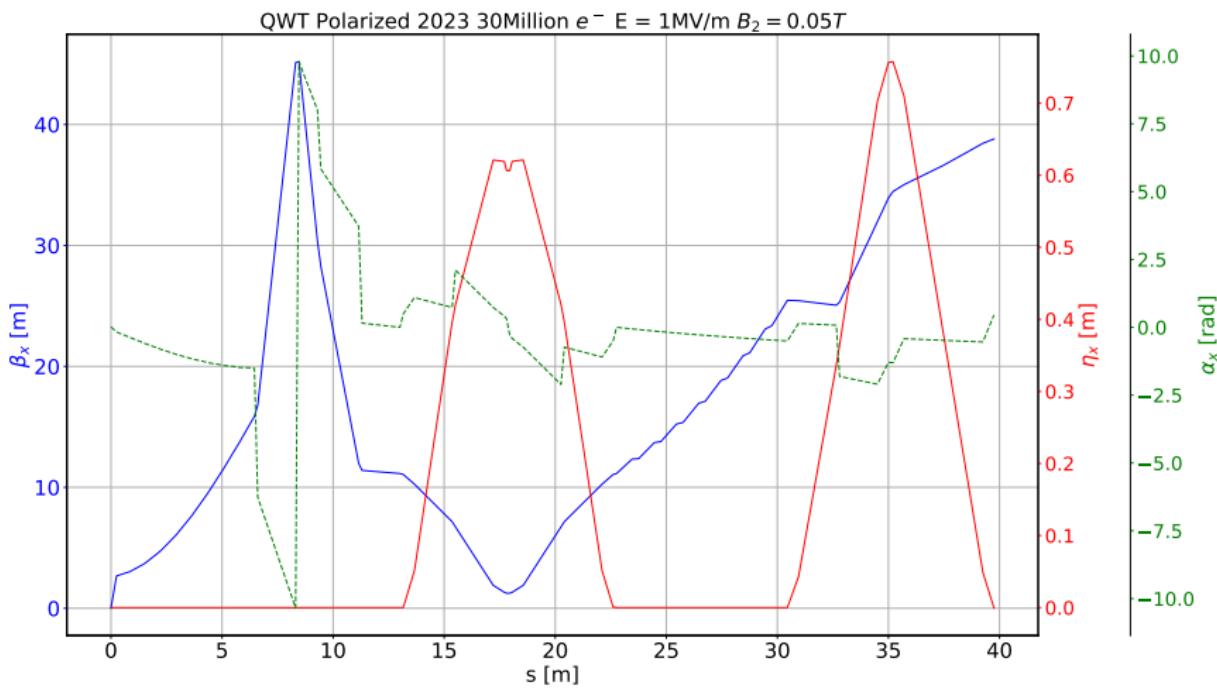
Conclusion

- The performance of the positron system is heavily influenced by the central momentum. For a high yield of positrons, the central momentum should be set to 15 MeV/c, while a high polarization requires a central momentum of 60 MeV/c.
- The QWT helps the selection of the desired momentum and reduces the spread of transverse angles.
- The accelerating section exerts significant influence on the longitudinal plane, thereby reducing the energy spread to meet the CEBAF requirement of $\sigma_{dp/p} = \pm 1\%$.
- For improved compression, the energy spread at the exit of the C100 must be at least five times smaller.
- Expecting higher current for the unpolarized mode P=15 MeV/c.

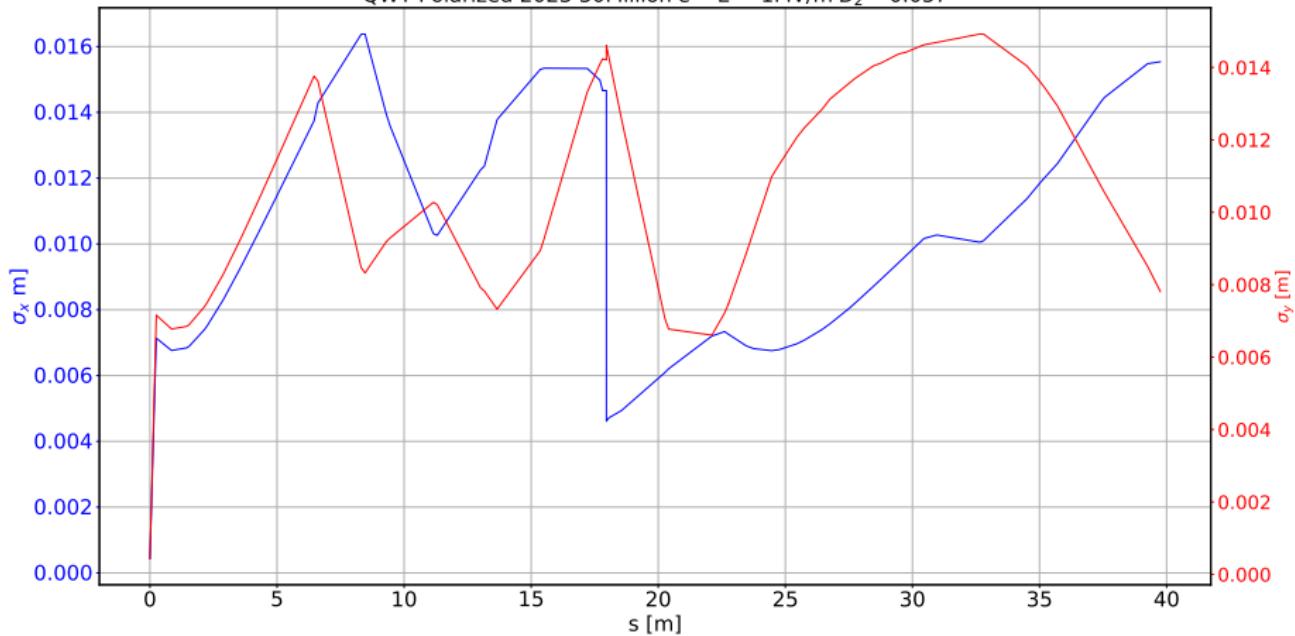
Conclusion

- The performance of the positron system is heavily influenced by the central momentum. For a high yield of positrons, the central momentum should be set to 15 MeV/c, while a high polarization requires a central momentum of 60 MeV/c.
- The QWT helps the selection of the desired momentum and reduces the spread of transverse angles.
- The accelerating section exerts significant influence on the longitudinal plane, thereby reducing the energy spread to meet the CEBAF requirement of $\sigma_{dp/p} = \pm 1\%$.
- For improved compression, the energy spread at the exit of the C100 must be at least five times smaller.
- Expecting higher current for the unpolarized mode P=15 MeV/c.

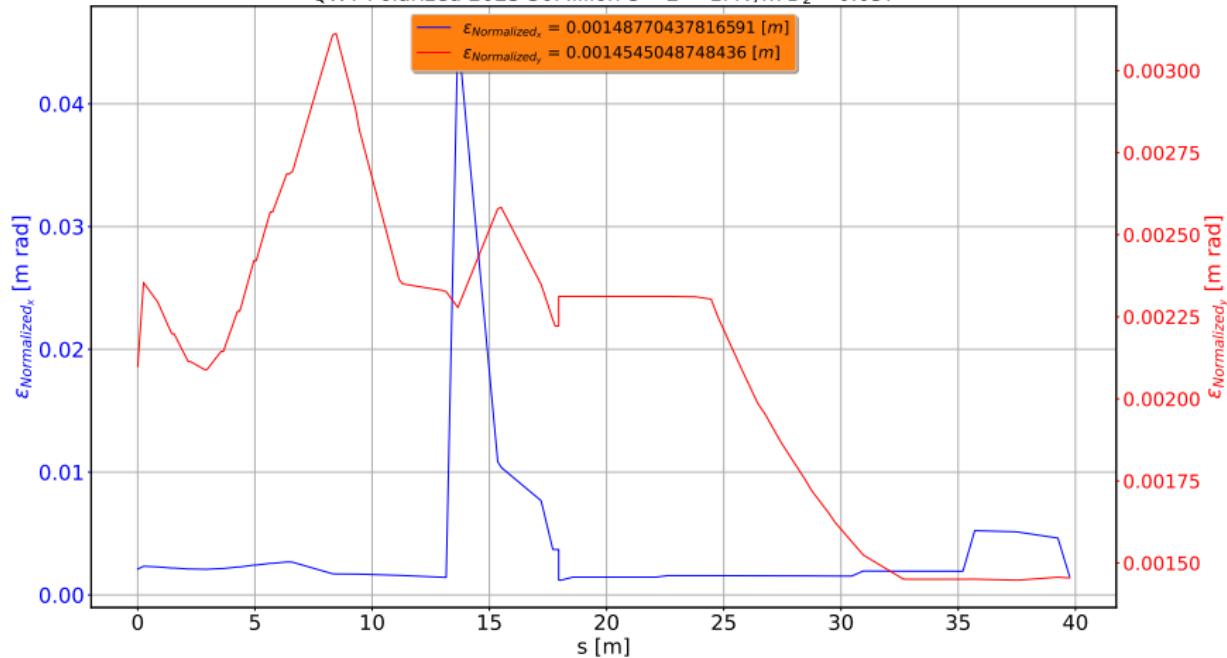
Twiss functions



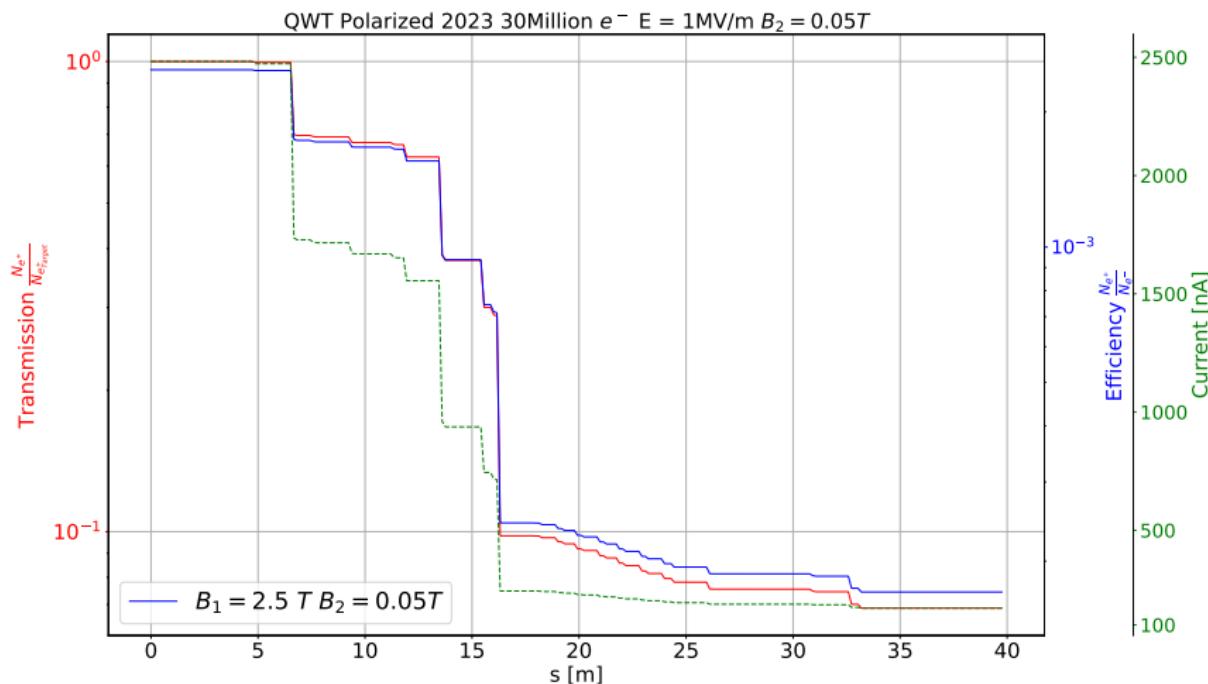
Beam size

QWT Polarized 2023 30Million e^- $E = 1\text{MV/m}$ $B_2 = 0.05T$ 

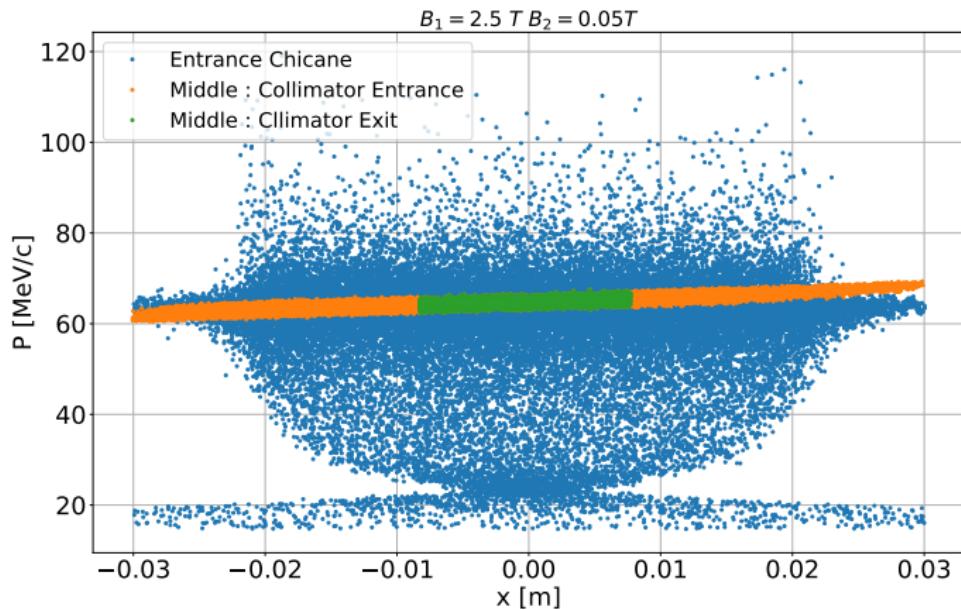
Normalized emittance

QWT Polarized 2023 30Million e⁻ E = 1MV/m B₂ = 0.05T

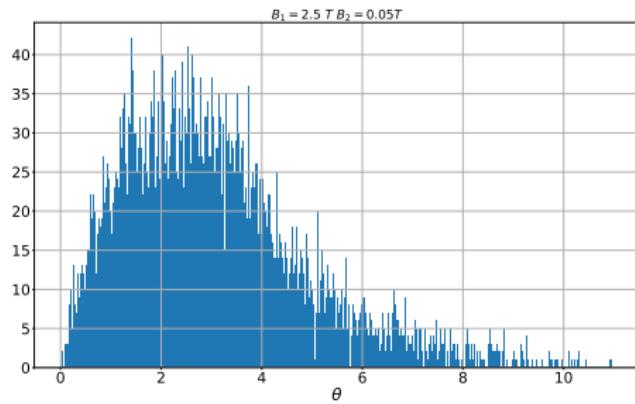
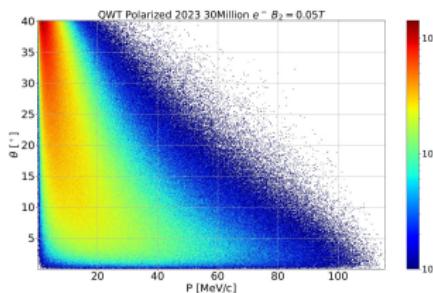
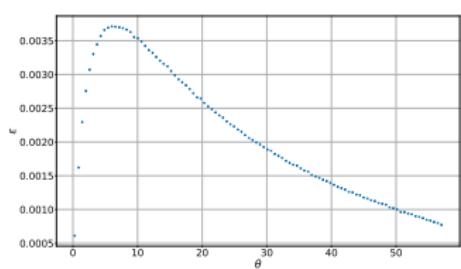
Transmission and current



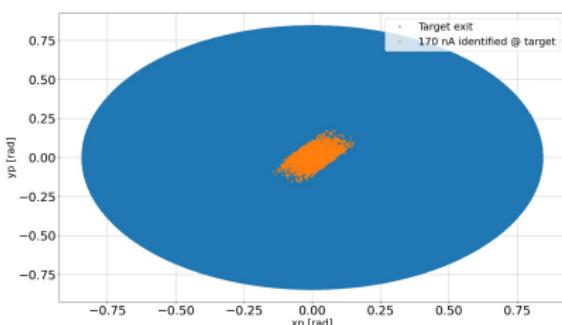
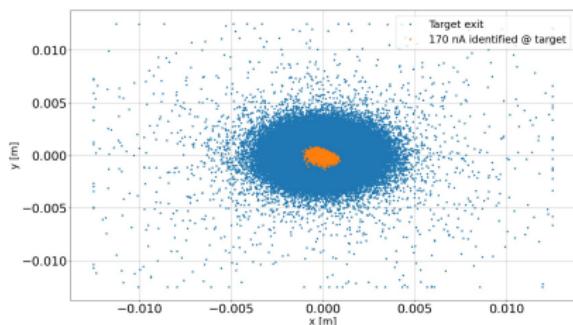
Momentum collimation



Angular distribution



Transverse space



- The transmitted positrons are within the acceptance of the QWT
- $p_t^{QWT} = \frac{eB_1R}{2} . = 10.31^\circ$
- $r_0^{QWT} = \frac{B_2}{B_1} R = 0.6 \text{ mm}$