

RF DIPOLE DEFLECTING/CRABBING CAVITIES

Subashini De Silva

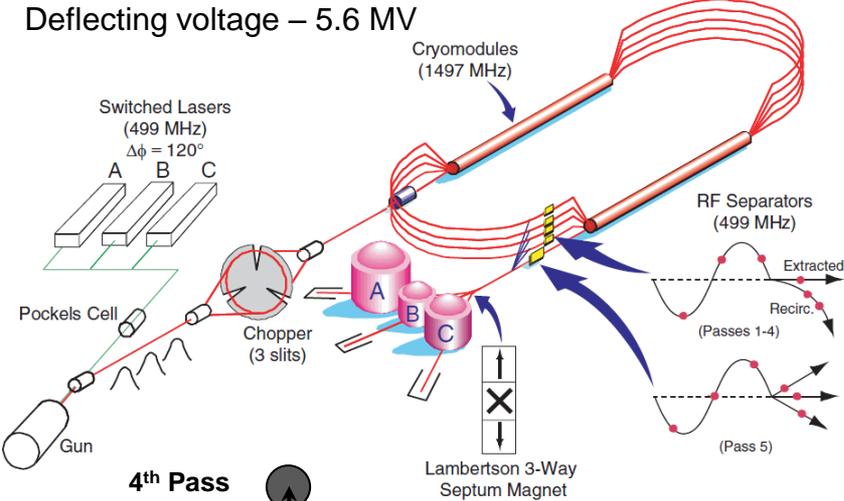
**Center for Accelerator Science
Department of Physics, Old Dominion University
and
Thomas Jefferson National Accelerator Facility**

Compact Deflecting/Crabbing Designs

- Operate in TE-like or TEM-like modes
 - 4-Rod Cavity (University of Lancaster / Jefferson Lab)
 - Parallel-Bar / RF-Dipole Cavity (ODU / SLAC)
 - Quarter Wave Cavity (BNL)
- RF Dipole design has
 - Low surface fields and high shunt impedance
 - Good balance between peak surface electric and magnetic field
 - No LOMs
 - Nearest HOM is widely separated (~ 1.5 fundamental mode)
 - Good uniformity of deflecting field due to high degree symmetry

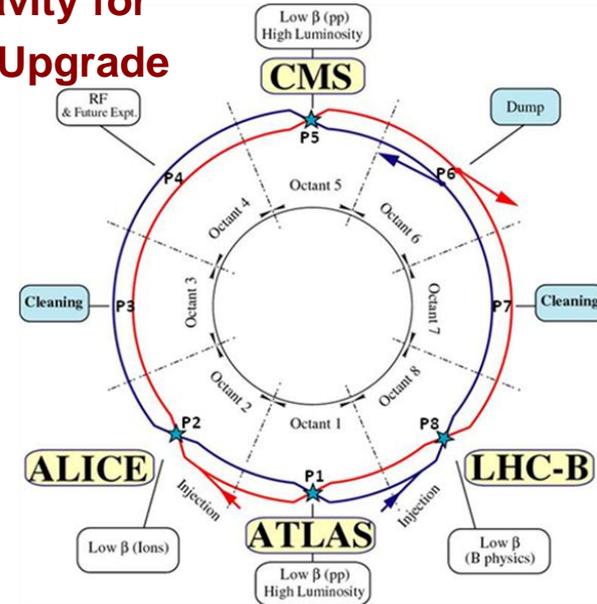
Current Applications of RF Dipole Cavity

499 MHz Deflecting Cavity for Jefferson Lab 12 GeV Upgrade

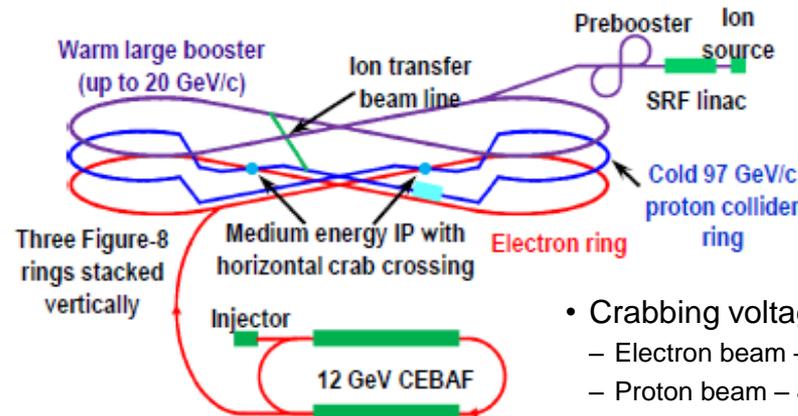


400 MHz Crabbing Cavity for LHC High Luminosity Upgrade

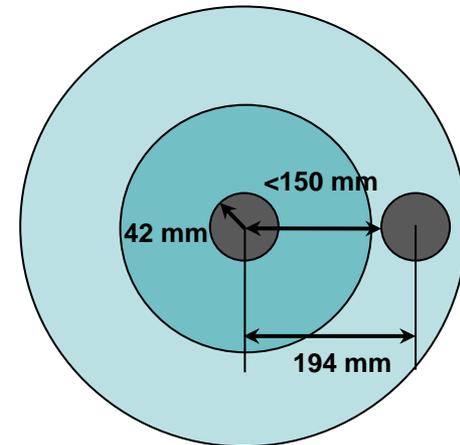
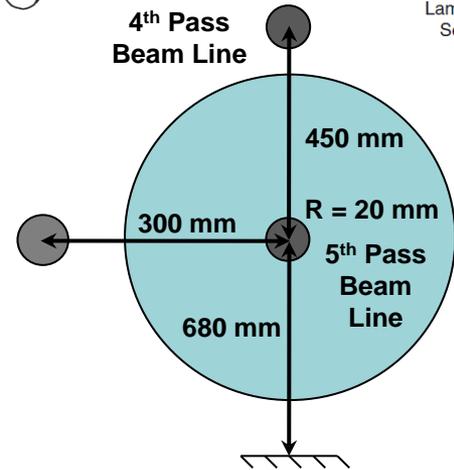
- Crabbing voltage – 10 MV per beam per side
- Requires a crabbing system at two interaction points (IP1 and IP5)
 - Vertical crossing at IP1
 - Horizontal crossing at IP5



750 MHz Crabbing Cavity for MEIC*



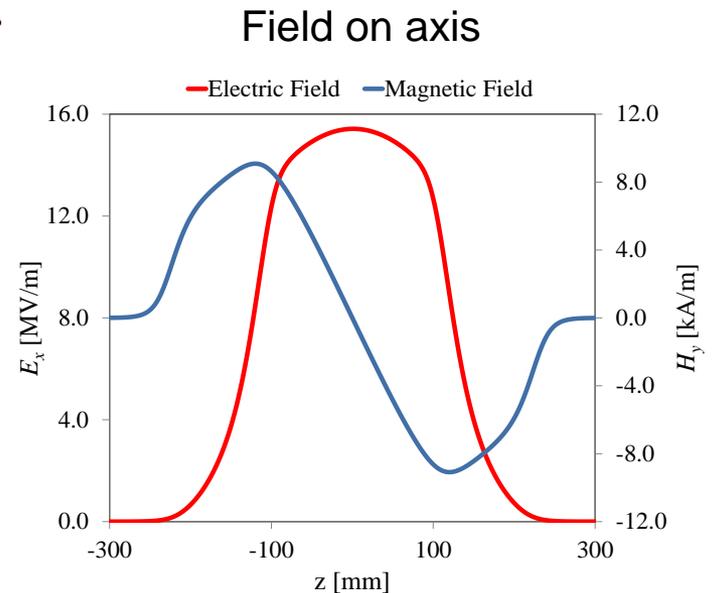
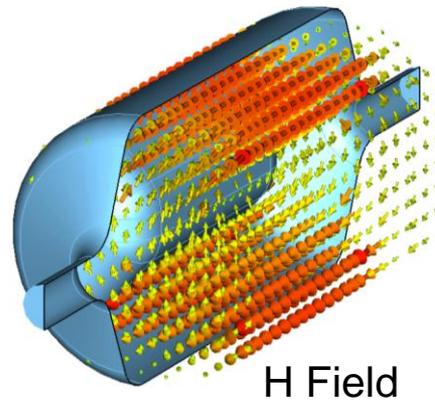
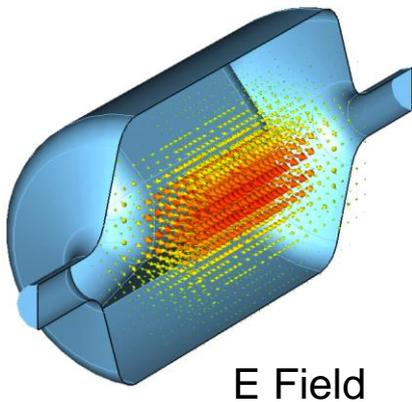
- Crabbing voltage
 - Electron beam – 1.5 MV
 - Proton beam – 8.0 MV



RF Dipole Cavity

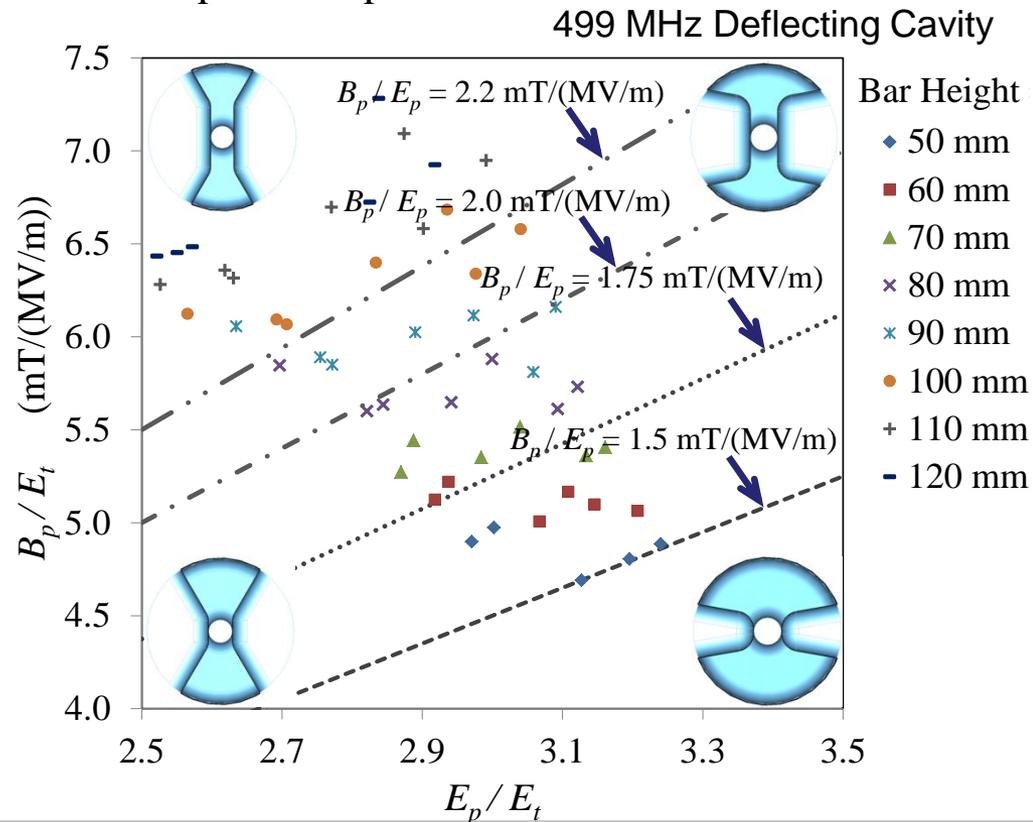
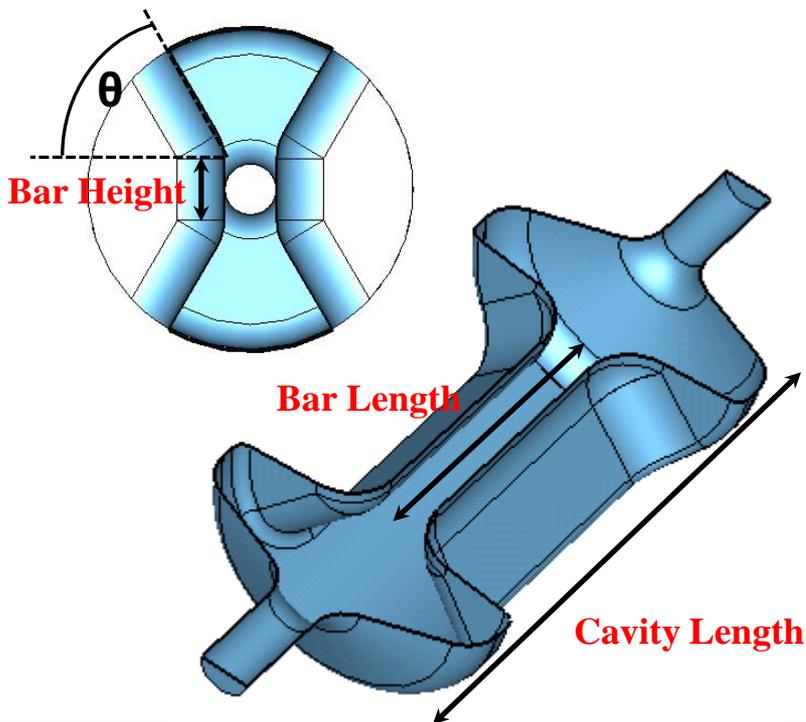
- Operates in a TE-like mode (cannot be a pure TE mode – Panofsky Wenzel Theorem)
- Deflecting/Crabbing mode is the lowest operating mode
- Net deflection is mainly due to the transverse electric field
- Transverse voltage

$$V_t = \int_{-\infty}^{+\infty} \left[E_x(z) \cos\left(\frac{\omega z}{c}\right) + cB_y \sin\left(\frac{\omega z}{c}\right) \right] dz.$$



Characteristics of the RF-Dipole Cavity

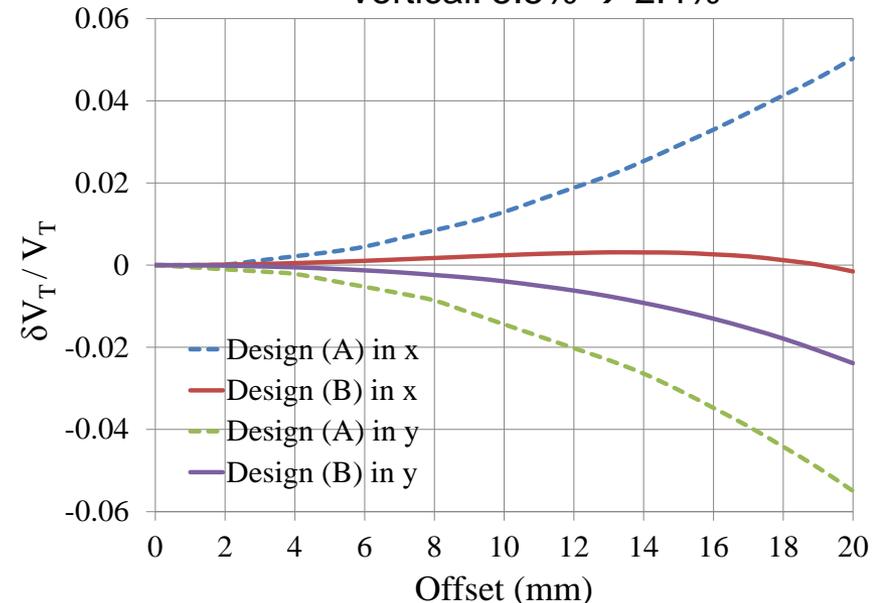
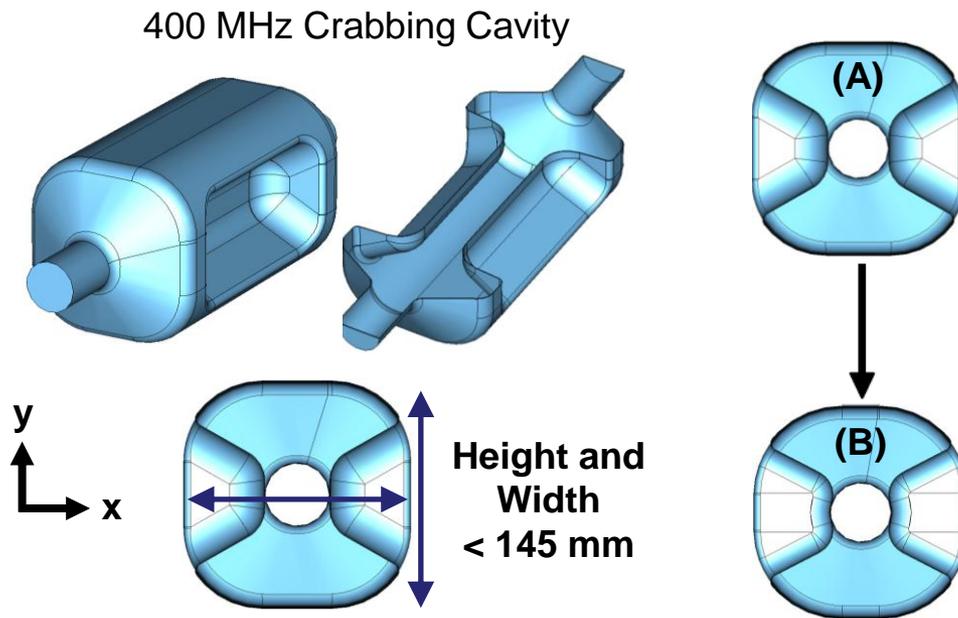
- Properties depend on a few parameters
 - Frequency determined by diameter of the cavity design
 - Bar Length $\sim \lambda/2$
 - Bar height and aperture determine E_p and B_p
 - Angle determines B_p/E_p



RF-Dipole Square Cavity Options

- Square-type rf-dipole cavity to further reduce the transverse dimensions
- Frequency is adjusted by curving radius of the edges
- RF-dipole cavity with modified curved loading elements across the beam aperture to reduce field non-uniformity

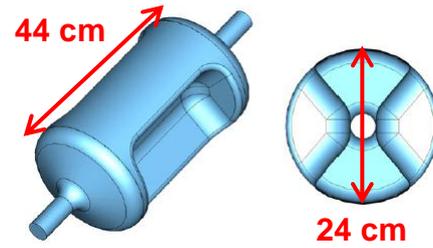
- Voltage deviation at 20 mm
 - Horizontal: 5.0% \rightarrow 0.2%
 - Vertical: 5.5% \rightarrow 2.4%



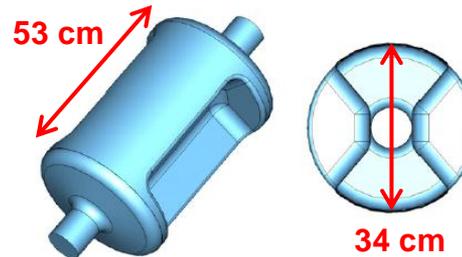
RF-Dipole Cavity Designs

Frequency	499.0	400.0	750.0*	MHz
Aperture Diameter (d)	40.0	84.0	60.0	mm
$d/(\lambda/2)$	0.133	0.224	0.3	
LOM	None	None	None	MHz
Nearest HOM	777.0	589.5	1062.5	MHz
E_p^*	2.86	3.9	4.29	MV/m
B_p^*	4.38	7.13	9.3	mT
B_p^*/E_p^*	1.53	1.83	2.16	mT/(MV/m)
$[R/Q]_T$	982.5	287.2	125.0	Ω
Geometrical Factor (G)	105.9	138.7	136.0	Ω
$R_T R_S$	1.0×10^5	4.0×10^4	1.7×10^4	Ω^2
At $E_T^* = 1 \text{ MV/m}$				

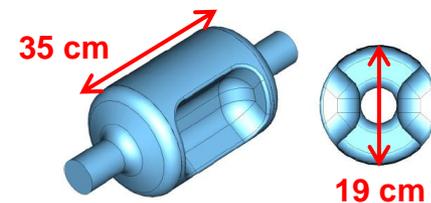
499 MHz Deflecting Cavity for Jefferson Lab 12 GeV Upgrade



400 MHz Crabbing Cavity for LHC High Luminosity Upgrade



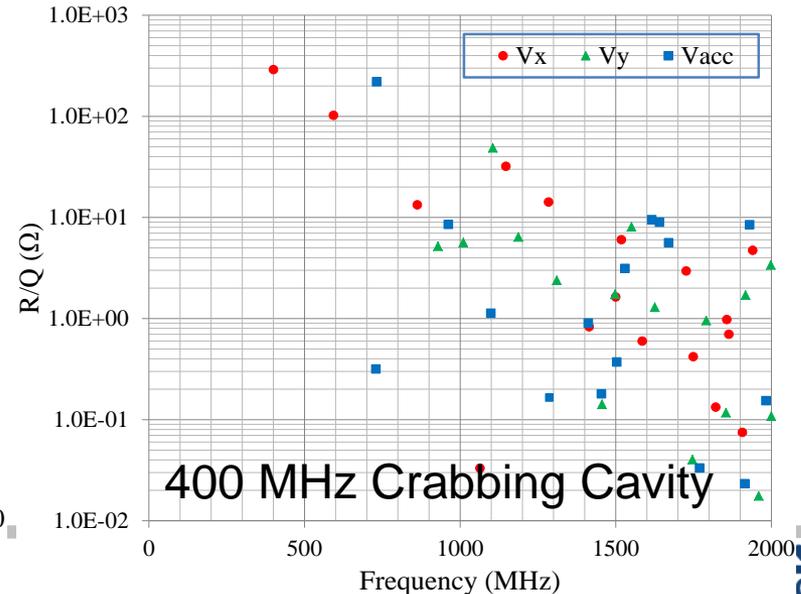
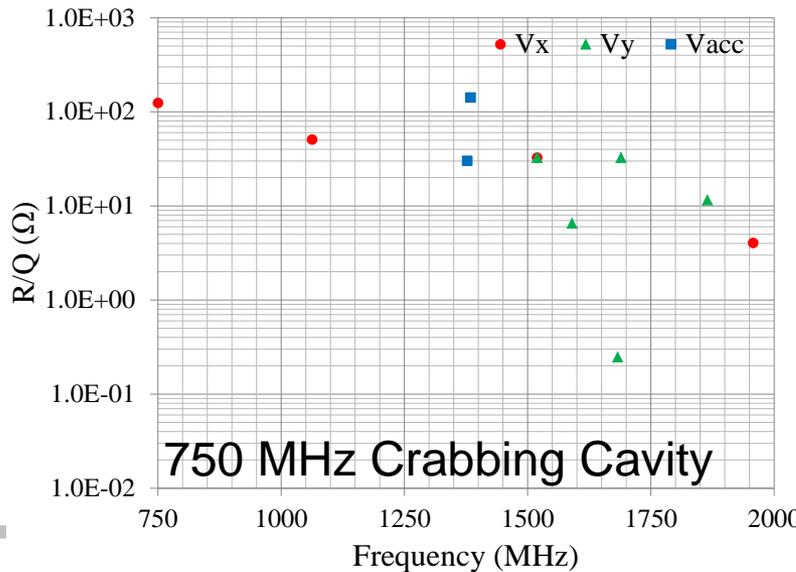
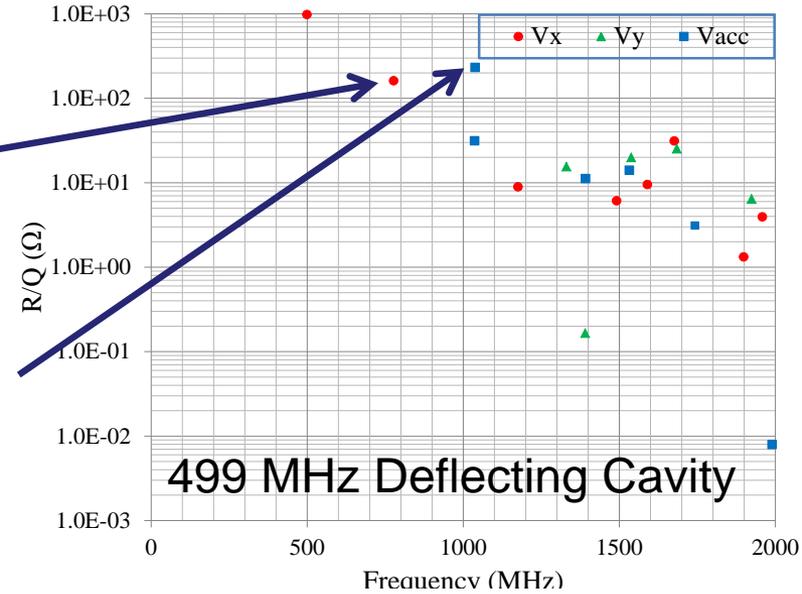
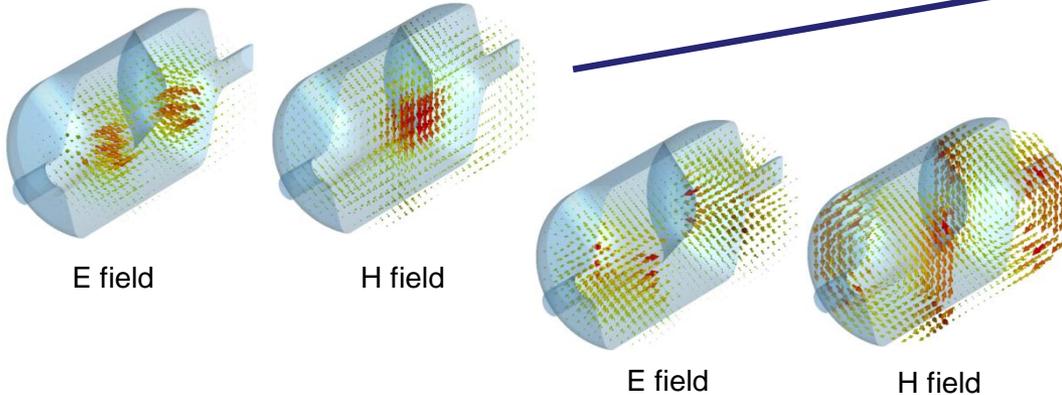
750 MHz Crabbing Cavity for MEIC at Jefferson Lab



* Alex Castilla (ODU)

HOM Properties of the RF-Dipole Cavity

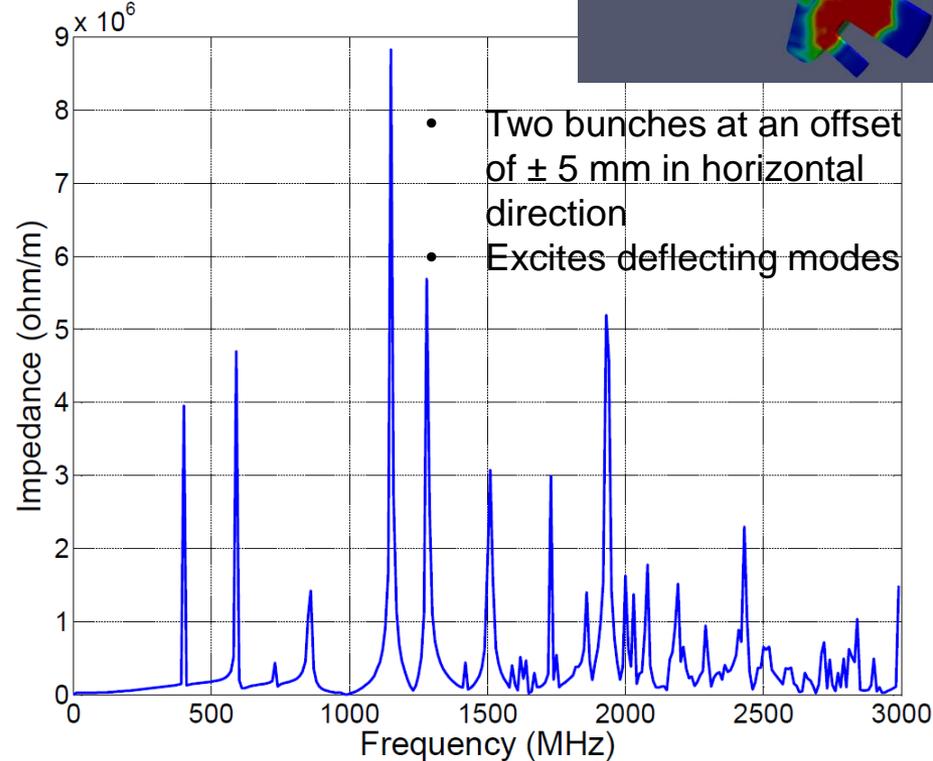
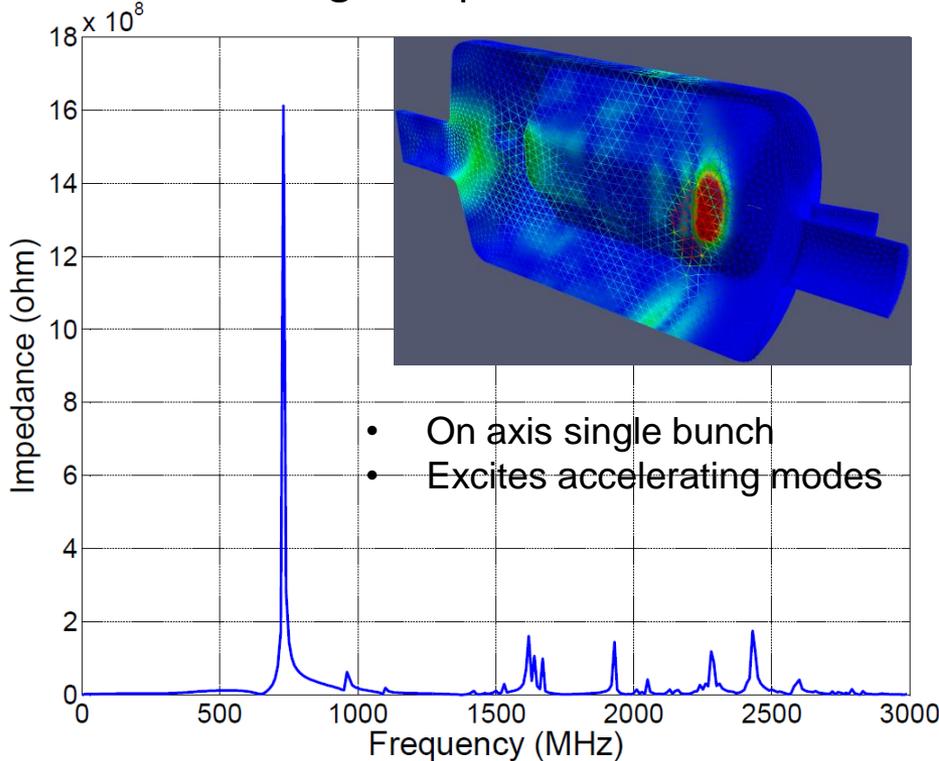
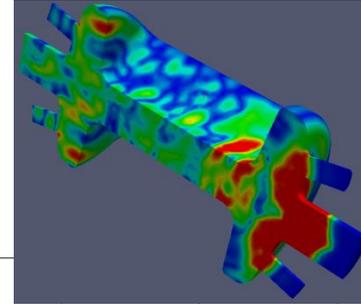
- Widely separated Higher Order Modes
- No Lower Order Modes



Wakefield and Impedance

- T3P – EM Time Domain Solver in the SLAC ACE3P Suite
- For the 400 MHz crabbing cavity
- Bunch Parameters
 - $\sigma = 1.4$ cm
 - charge = 1 pC

$$\lambda(s) = \frac{1}{\sigma\sqrt{2\pi}} \exp\left[-\frac{(s-s_0)^2}{2\sigma^2}\right]$$

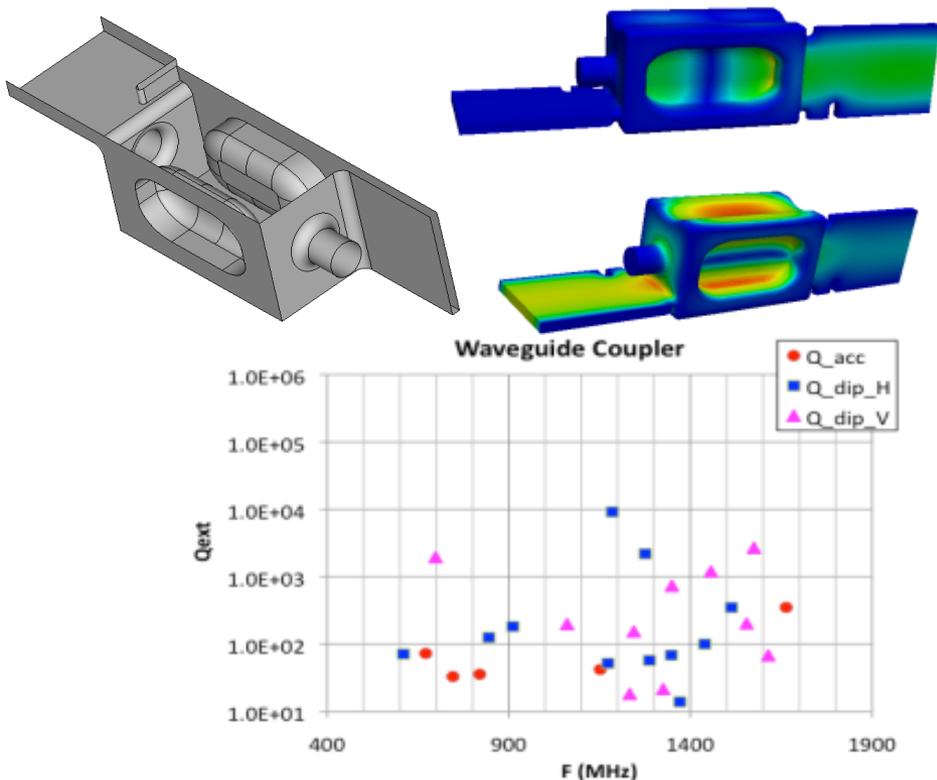


HOM Damping

- Widely separated HOMs from the operating mode allows more options in the design of damping schemes

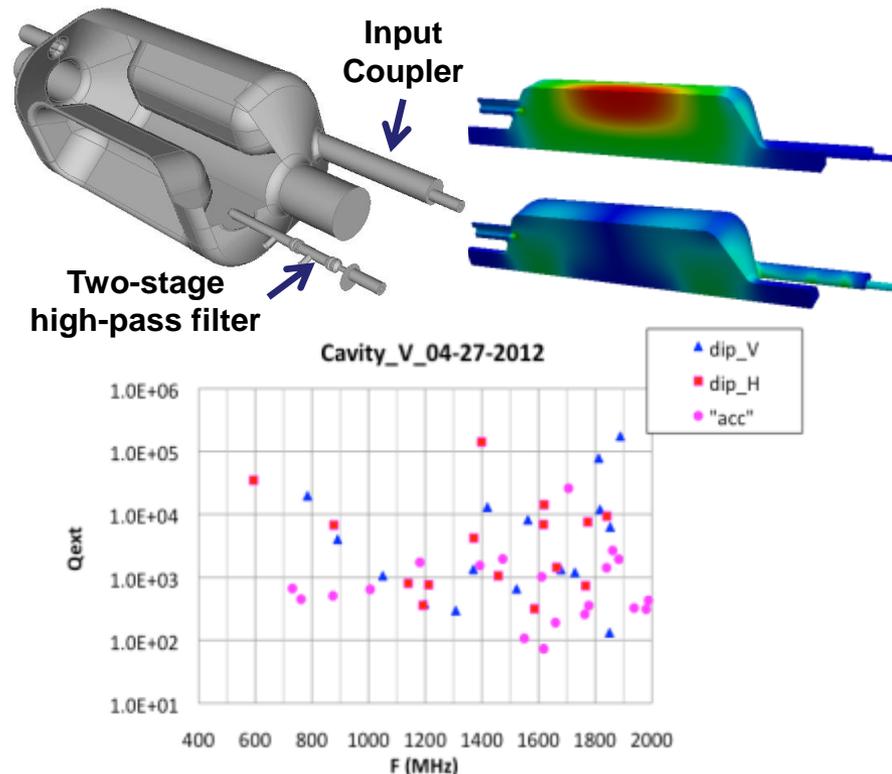
Waveguide Damping

- Strong damping was achieved with waveguide couplers



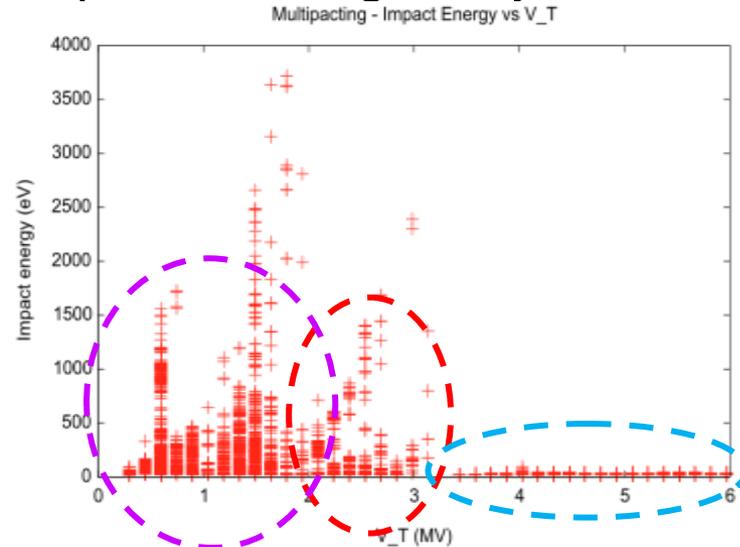
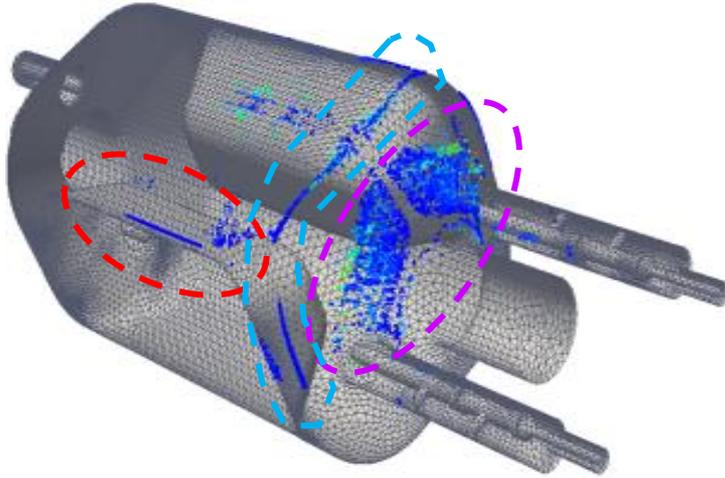
Coaxial Coupling

- A high pass coaxial couplers to exclude the operating mode



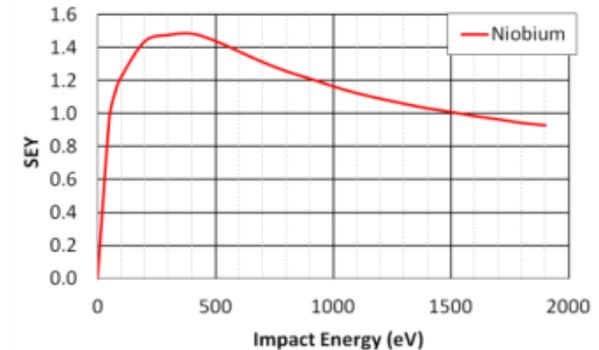
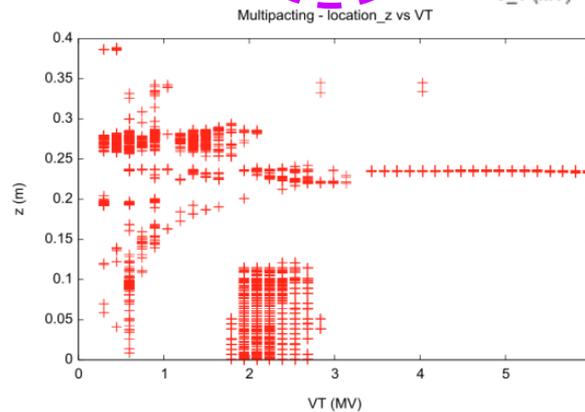
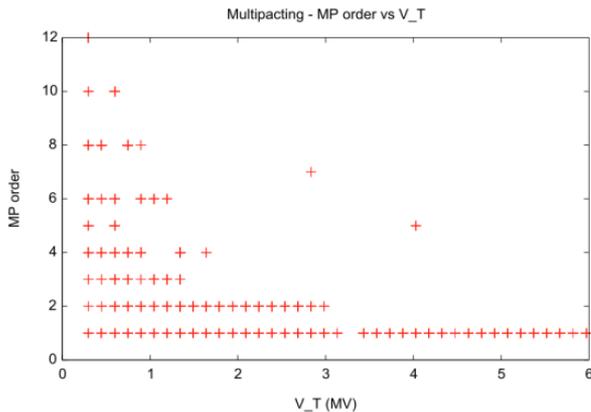
Multipacting Analysis

- Track3P – Particle tracking code in the SLAC ACE3P Suite
- For the 400 MHz square-shaped crabbing cavity



Deflecting Voltage

- 0.5MV to 2.6 MV
- 1.8 MV to 2.8MV
- 3.0 MV to 6.0 MV

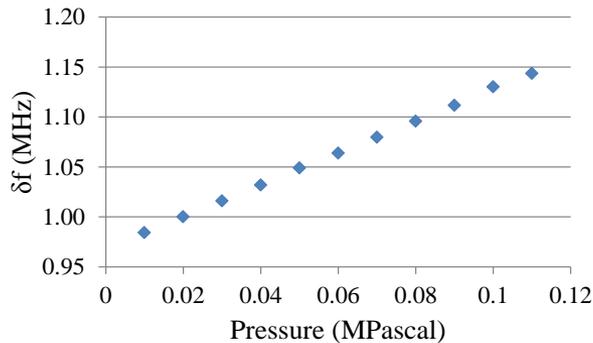


Mechanical Analysis – 499 MHz Cavity

Without any kind of stiffening or pressure sensitivity optimization

Pressure

Pressure sensitivity - 212 Hz/torr



Lorentz Detuning

Room temperature cavity with a uniform 3 mm thickness

- $\Delta f = 6.15 \text{ kHz @ } V_T = 3.0 \text{ MV}$

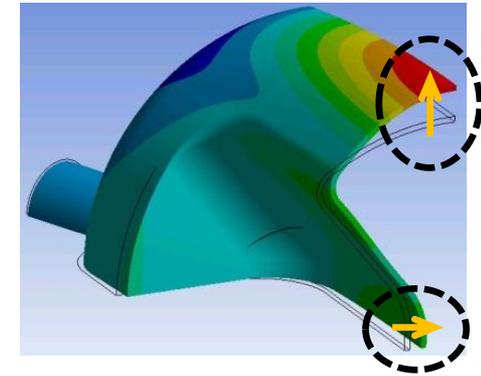
- $k_L = 61.54 \text{ Hz}/(\text{MV}/\text{m})^2$

Fabricated cavity at 4 K

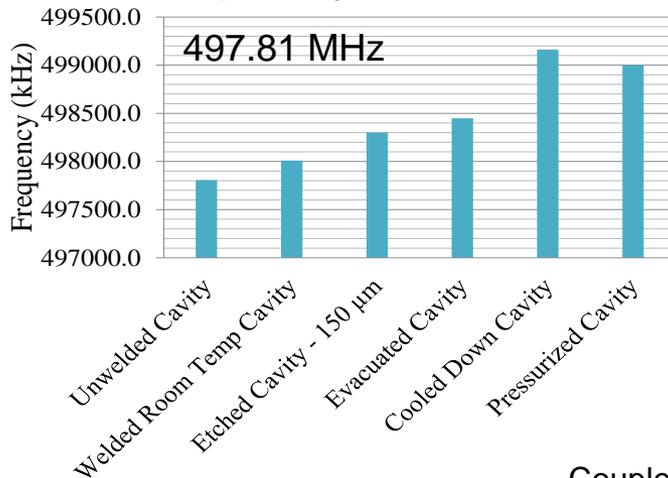
- $\Delta f = 4.93 \text{ kHz @ } V_T = 3.0 \text{ MV}$

- $k_L = 49.27 \text{ Hz}/(\text{MV}/\text{m})^2$

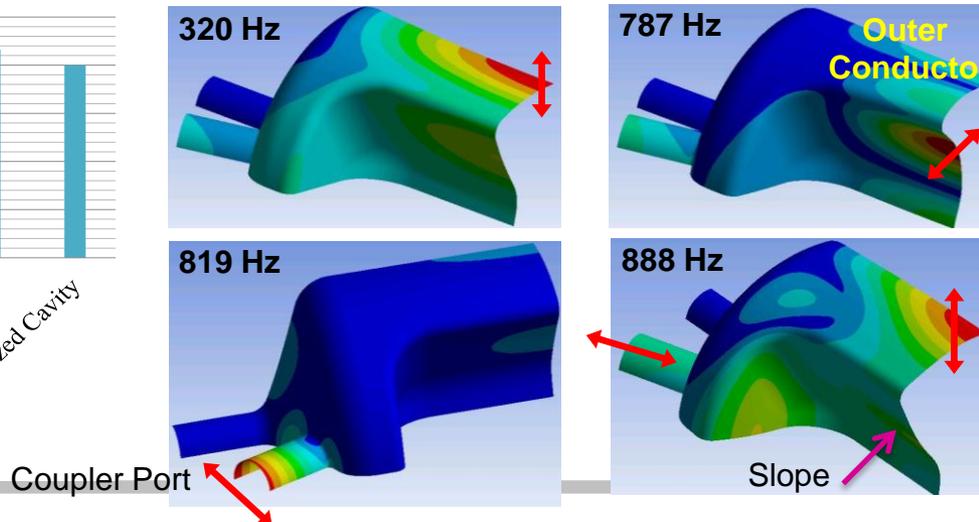
- Deformation = $1.2 \mu\text{m}$



Frequency Variation



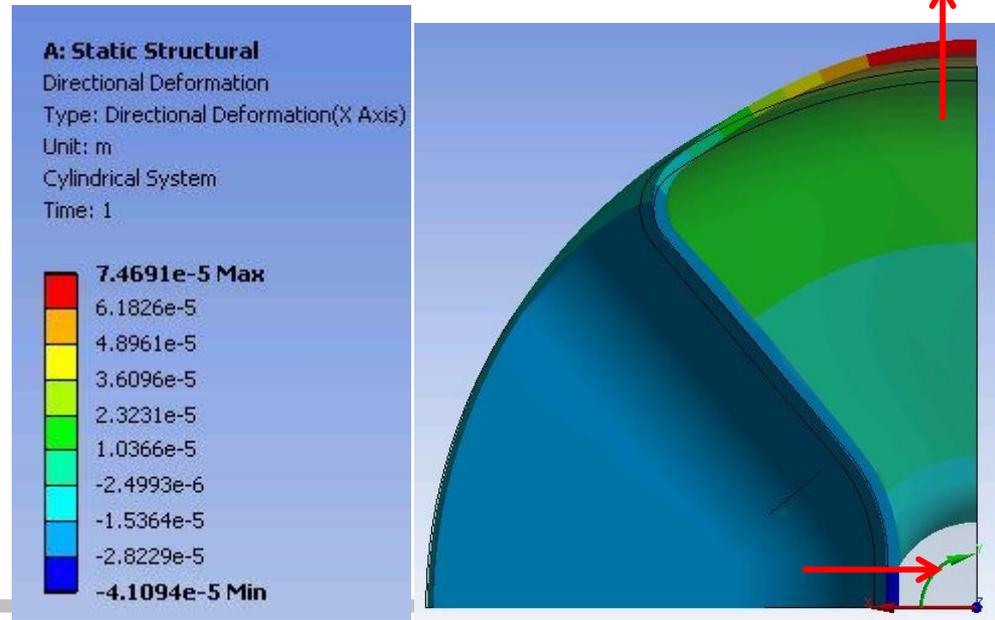
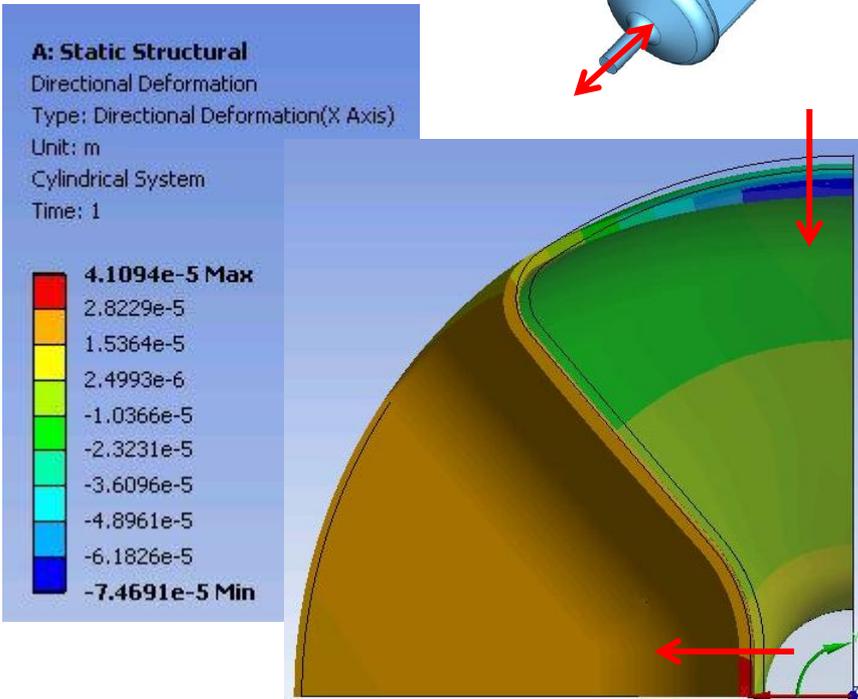
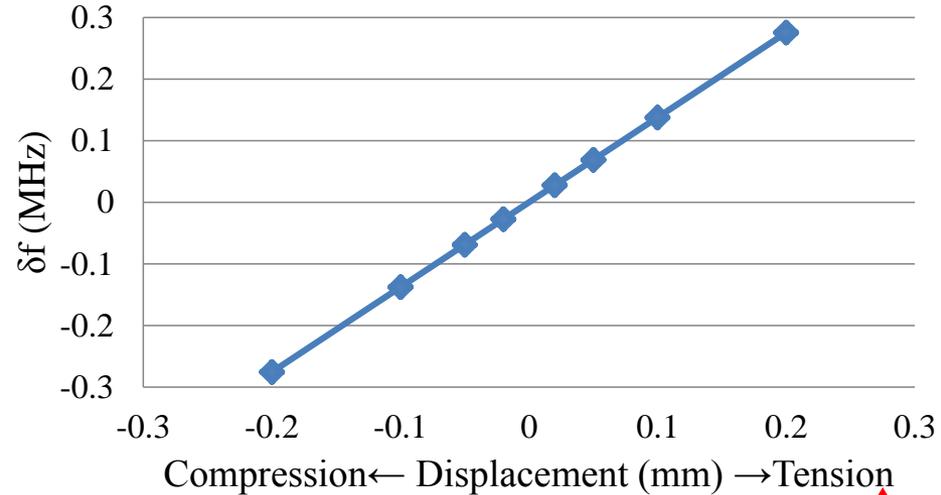
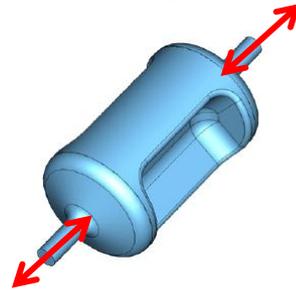
Mechanical Modes



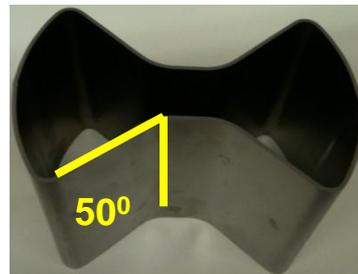
- Cavity with a 3 mm uniform thickness
- At room temperature and under vacuum

Tuning Sensitivity – 499 MHz Cavity

- Cavity as fabricated at 4 K under vacuum
- Tuning sensitivity – 1.4 kHz/ μm

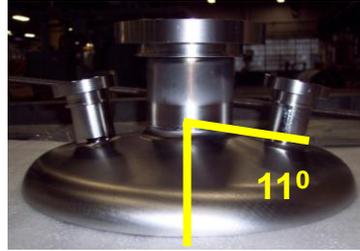


499 MHz RF-Dipole Cavity Fabrication



400 & 750 MHz RF-Dipole Cavity Fabrication

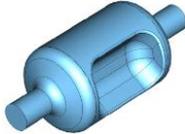
400 MHz Crabbing Cavity



750 MHz Crabbing Cavity



Properties of Cavities Under Development

Parameter					 Alex Castilla (ODU)				Unit
	400.0		499.0		750.0				
Frequency	400.0		499.0		750.0				MHz
Particle	p		e ⁻		e ⁻	p			
Deflecting voltage (V_T^*)	0.375		0.3		0.2				MV
Peak electric field (E_P^*)	3.9		2.86		4.29				MV/m
Peak magnetic field (B_P^*)	7.13		4.38		9.3				mT
Required transverse voltage per beam	10.0		5.6		1.5	8.0			MV
No. of cavities	3		2		1	4			
Transverse voltage per cavity	3.4		3.0		1.5	2.0			MV
Peak magnetic field (B_P)	64.7		43.8		69.8	93.0			mT
Peak electric field (E_P)	35.4		28.6		32.2	42.9			MV
$R_T R_S$	3.7×10^4		3.6×10^4		3.7×10^4				Ω^2
Operating temperature	2.0	4.0	2.0	4.0	2.0	4.0	2.0	4.0	K
Surface Resistance (R_S)**	11.3	70.0	12.0	100.0	14.0	200.0	14.0	200.0	n Ω
Power dissipation per cavity **	3.6	21.9	3.0	25.0	0.9	12.2	1.6	21.7	W
At $E_T^* = 1$ MV/m ** Estimated									

Summary

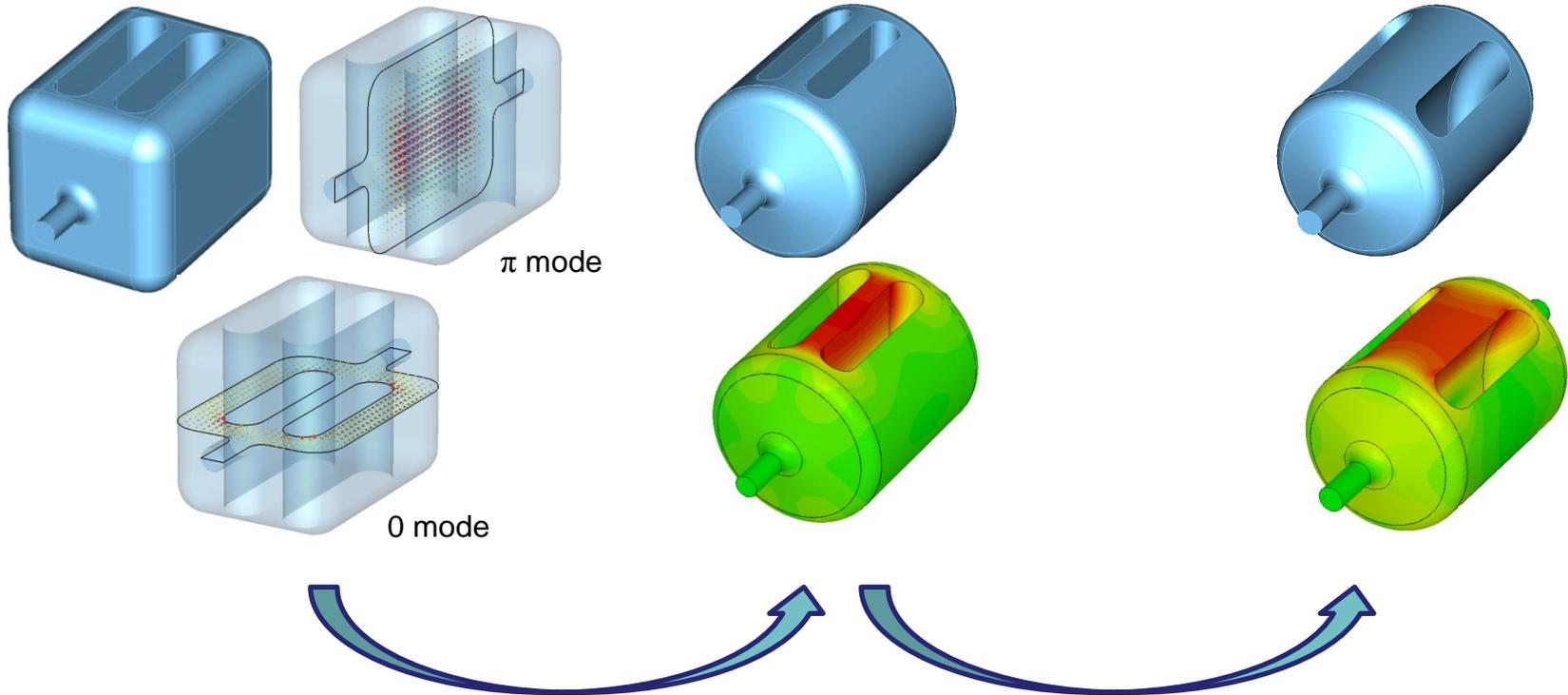
- Development of compact deflecting/crabbing cavities was in response to the strict dimensional requirements in some current applications
- Compact rf-dipole design has
 - Low and balanced surface fields
 - High shunt impedance
 - Has no lower-order-mode with a well-separated fundamental mode
- Work in progress
 - 499 MHz deflecting cavity
 - Fabrication will be completed by Nov-Dec
 - 400 MHz crabbing cavity
 - Preparation for processing
 - Bulk BCP – Fixtures and parts are being fabricated for both cavities (Nov-Dec)
 - 750 MHz crabbing cavity
 - Cavity processed with bulk BCP of 150 μm

Acknowledgements

- Jefferson Lab
 - HyeKyoung Park
- ODU
 - Alejandro Castilla
- SLAC
 - Zenghai Li, Lixin Ge
- Niowave
 - Dmitry Gorelov, Terry Grimm

- The work done at ODU is towards my PhD carried out under the supervision of Dr. Jean Delayen

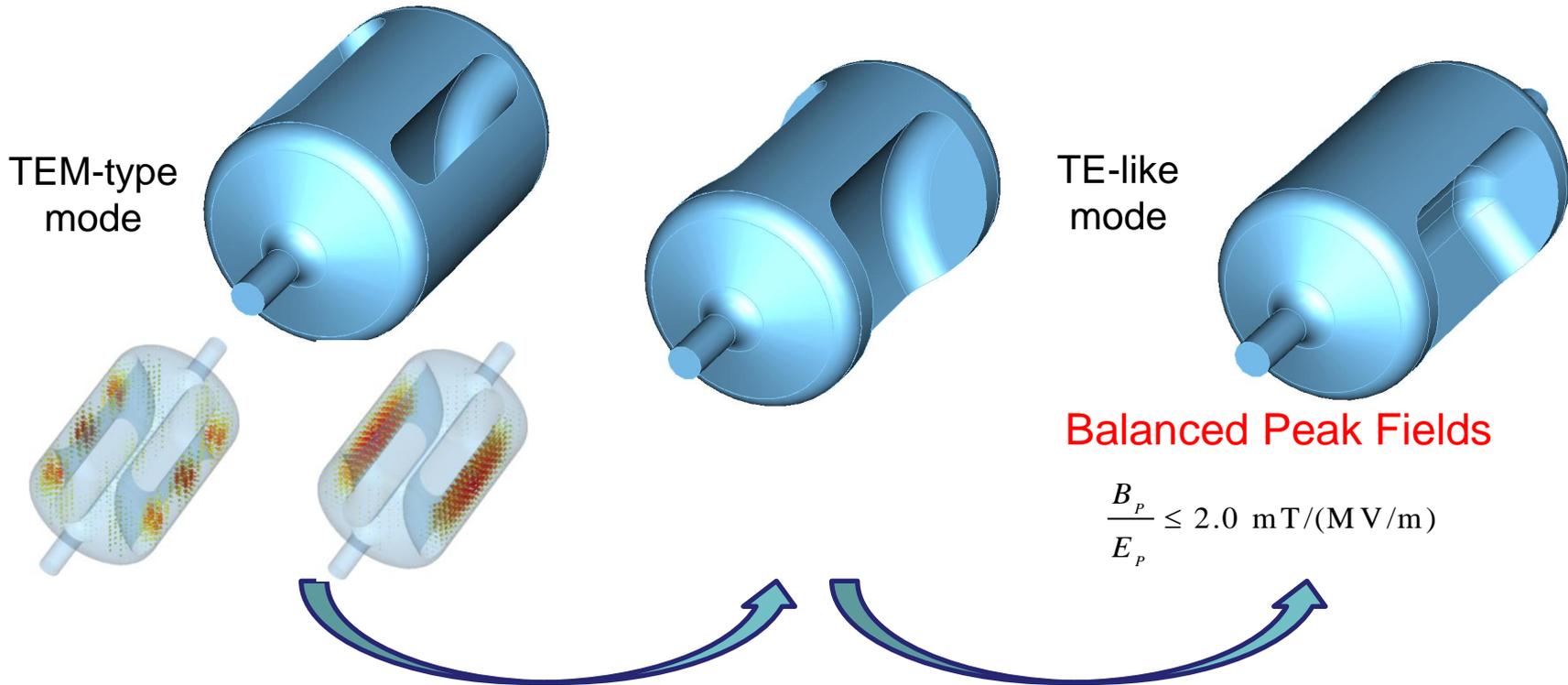
Design Evolution



- To increase mode separation between fundamental modes
- ~18 MHz \rightarrow ~130 MHz
- To improve design rigidity \rightarrow Less susceptible to mechanical vibrations and deformations

- To lower peak magnetic field
- Reduced peak magnetic field by ~20%

Design Evolution



- To remove higher order modes with field distributions between the cavity outer surface and bar outer surface
- Eliminate multipacting conditions

- To lower peak magnetic field
- Reduced peak magnetic field by ~25%
- To achieve balanced peak surface fields
- $B_p/E_p \approx 1.5 \text{ mT}/(\text{MV}/\text{m})$

Stress Analysis – 499 MHz Cavity

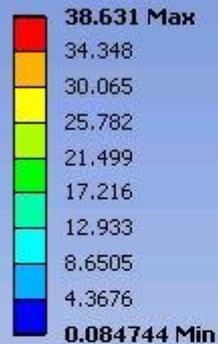
A: VTA Cool down (Room Temp 1.4 atm)

Equivalent Stress

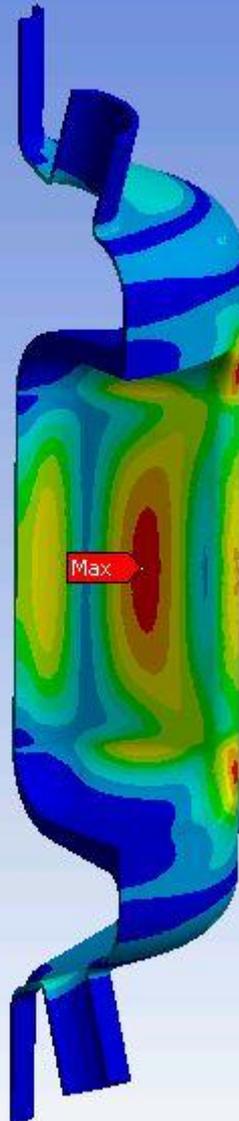
Type: Equivalent (von-Mises) Stress

Unit: MPa

Time: 1



- Fixed support from the top
- Pressure = 0.14186 MPa
- With standard earth gravity



F: VTA Test condition (4K 1 atm)

Equivalent Stress

Type: Equivalent (von-Mises) Stress

Unit: MPa

Time: 1

